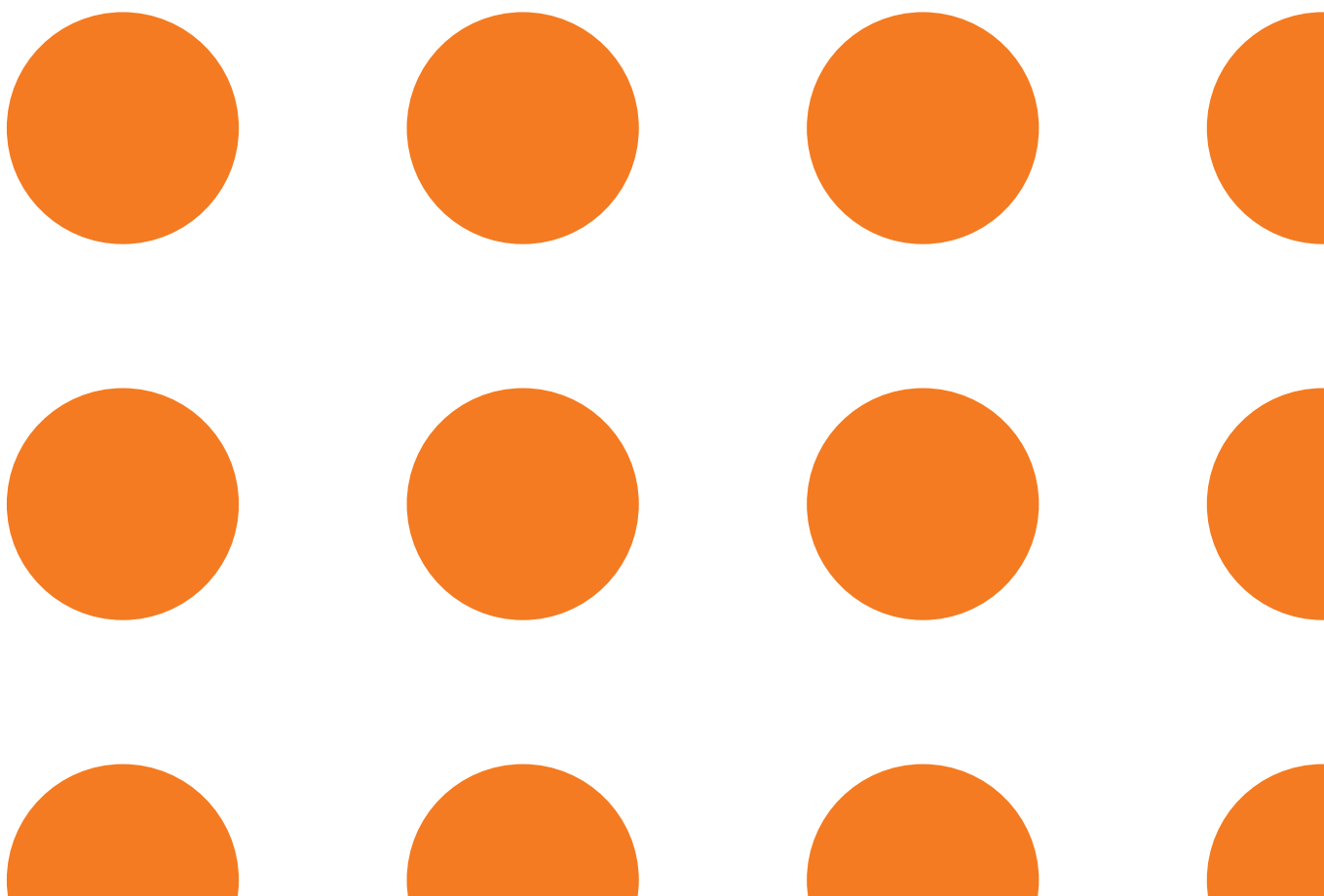


EDÍCIA ODBORNÝCH PRÍRUČIEK

RASTISLAV MENĎAN, MONIKA PAVČEKOVÁ, BORIS VAVROVIČ

COMPLEX THERMAL-TECHNICAL ANALYSIS OF THE DETACHED PANEL APARTMENT HOUSE OF TYPE B 70 IN ORIGINAL STATE (PART 1)



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OF TYPE B 70 IN ORIGINAL STATE
(PART 1)**

SLOVENSKÁ TECHNICKÁ UNIVERZITA V BRATISLAVE

2025

Publikácia bola spracovaná s podporou projektu KEGA 046STU-4/2025 - Aktualizácia a modernizácia vybraných predmetov pozemného staviteľstva so zohľadnením súčasných požiadaviek v oblasti obnovy budov a architektúry.

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ISBN 978-80-227-5565-8

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Vydala Slovenská technická univerzita v Bratislave vo Vydavateľstve SPEKTRUM
STU, Bratislava, Vazovova 5, v roku 2025.

Rozsah 129 strán, 10,034 AH, 10,240 VH, 1. vydanie, edičné číslo 6261,
vydané v elektronickej forme

Schválila Edičná rada Stavebnej fakulty STU v Bratislave.

85 – 243 – 2025

ISBN 978-80-227-5565-8
DOI: 10.61544/CWHE8660

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Used Symbols and Units

A_f	Area of window frame	m^2
A_g	Area of window glazing	m^2
A_w	Area of window	m^2
b	Thermal effusivity of floor.....	$W.s^{1/2}/(m^2.K)$
b_N	Standard value of thermal effusivity of floor	$W.s^{1/2}/(m^2.K)$
b_x	Reduction factor	-
c	Specific thermal capacity	$J/(kg.K)$
d	Thickness	m
f_{Rsi}	Temperature factor	-
i_{LV}	Gap permeability coefficient	$m^3/(m.s.Pa^{0.67})$
l	Length of joints of windows and entry doors	m
l_g	Length of perimeter of glazing	m
M_c	Annual amount of condensed water vapour in a construction	$kg/(m^2.a)$
$M_{c,max}$	Maximum permissible annual amount of condensed water vapour in a construction according to the standard	$kg/(m^2.a)$
M_d	Diffusion flow rate of water vapour	$kg/(m^2.s)$
M_{ev}	Annual amount of evaporated water vapour from a construction	$kg/(m^2.a)$
n	Air change rate	$1/h$
p_{de}	Partial pressure of water vapour of external air	Pa
p_{di}	Partial pressure of water vapour of internal air	Pa
$p_{sat,se}$	Partial pressure of saturated water vapour on external surface of a construction	Pa
$p_{sat,si}$	Partial pressure of saturated water vapour on internal surface of a construction	Pa
R	Thermal resistance	$m^2.K/W$
R_d	Diffusion resistance	m/s
R_N	Standard value of thermal resistance	$m^2.K/W$
R_{se}	Surface resistance of heat transfer on external side of a construction	$m^2.K/W$
R_{si}	Surface resistance of heat transfer on internal side of a construction	$m^2.K/W$
U	Thermal transmittance	$W/(m^2.K)$
U_f	Thermal transmittance of window frame	$W/(m^2.K)$

U_g	Thermal transmittance of window glazing	W/(m ² .K)
U_N	Standard value of thermal transmittance.....	W/(m ² .K)
U_w	Thermal transmittance of window	W/(m ² .K)
$U_{w,N}$	Standard value of thermal transmittance of window	W/(m ² .K)
V_b	Volume of the heated space of building	m ³
ΔM_d	Condensed amount of water vapour	kg/(m ² .s)
$\Delta \theta_{si}$	Safety value of surface temperature.....	K
$\Delta \theta_{10}$	Decrease of contact temperature	°C
θ_{dp}	Dew point temperature	°C
θ_e	Calculating external air temperature.....	°C
θ_i	Calculating internal air temperature.....	°C
θ_{si}	Internal surface temperature.....	°C
$\theta_{si,80}$	Critical surface temperature for growth of moulds	°C
λ	Thermal conductivity coefficient	W/(m.K)
μ	Diffusion resistance factor	-
ρ	Apparent density	kg/m ³
Σ	Sum	-
φ_e	Relative humidity of external air	%
φ_i	Relative humidity of internal air	%
ψ	Linear thermal transmittance	W/(m.K)
ψ_g	Linear thermal transmittance in contact of glazing and frame	W/(m.K)

Introduction

Renovation of panel apartment buildings and related problems are becoming more and more current topic. The emphasis is put not only on a quality of housing but also on decreasing the energy need for heating and minimizing heat losses through envelope constructions of a building. This is possible to reach only by quality thermal protection in form of revovation of envelope constructions of a building, i.e. thermal insulation of external walls, roof and floor and replacement of original windows. An important factor for achieving lower energy need for heating but also the healthy indoor environment without the risk of growth of moulds is a correct solution of thermal bridges.

This publication presents issues of thermal-technical evaluation of envelope constructions and selected details of detached panel apartment house of structural system B 70 in its original state, which was built in the seventies and eighties of the twentieth century. The aim of team of authors was comprehensively calculate and analyse thermal-technical properties of this building. This publication can be used as a tool when renovating buildings built in this type of structural system.

The thermal-technical evaluation of the detached panel apartment house B 70 in its original state is divided into two publications (Part 1 and Part 2). This publication (Part 1) deals with a description of the building (Chapter 1), evaluation of envelope constructions (Chapter 2), windows (Chapter 3), evaluation of 24 selected details of the building from the point of view of hygienic criterion and calculation of linear themal transmittance (Chapter 4).

The second publication (Part 2) presents an evaluation of another details, calculation of ΔU -value and energy need for heating.

The publication is written in a clearly arranged tabular way, in form of professional handbook. It has no ambition to be a textbook, but only a handbook. It is intended not only for students of faculties of civil engineering and faculties of architecture, but also for the professional and general public.

The basic prerequisite for using this handbook is at least a minimum knowledge of building thermal technology and thermal protection of buildings.

Team of authors

1 Evaluated Building

Table 1.1 – Floor plan of detached house of structural system B 70

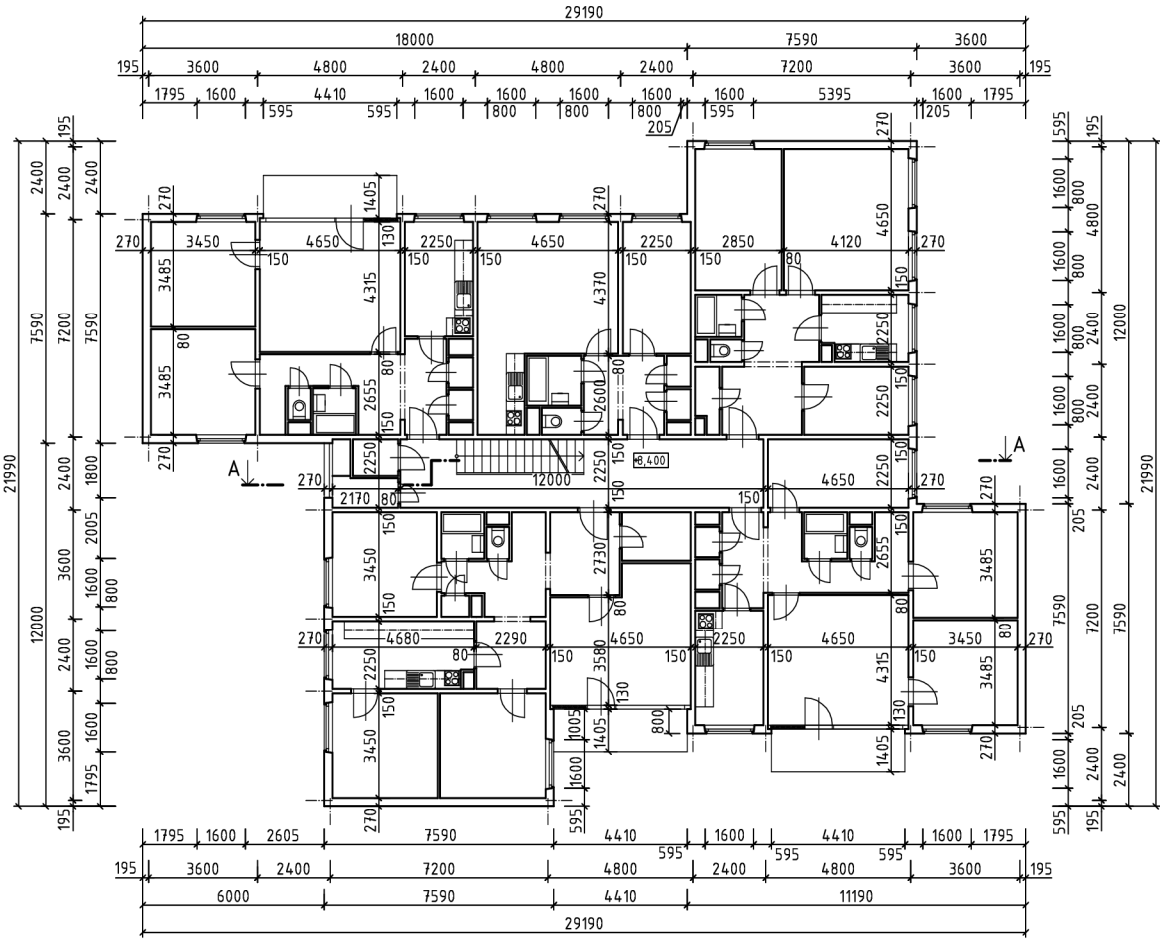
Structural system B 70 - detached house	
Floor plan	
	
Description of the evaluated building	
The evaluated apartment house is built in the structural system B 70. It is a detached house. It has 8 living floors with flats and an entrance floor. The module of load-bearing walls is 2400, 3600 and 4800 mm. The construction height is 2800 mm. The building has a flat roof. External wall panels consist of reinforced concrete load-bearing wall with the thickness of 150 mm, polystyrene foam boards of 60 mm and reinforced concrete membrane of 60 mm. The thickness of internal load-bearing reinforced concrete walls and ceiling panels is 150 mm. The building has wooden windows with double glazing and steel windows.	

Table 1.2 – Front view and cross-section of detached house of structural system B 70



2 Thermal-Technical Properties and Evaluation of Envelope Constructions of a Building

Table 2.1.1 - Thermal-technical properties and evaluation of external wall 1

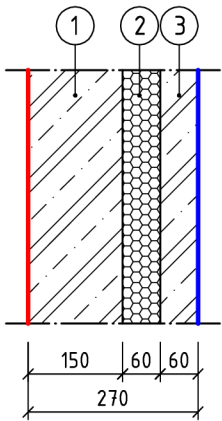
External wall 1								
Boundary conditions for interior $\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$						Boundary conditions for exterior $\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$		
No.	Material	Thickness	Apparent density	Thermal conductivity coefficient	Specific thermal capacity	Diffusion resistance factor	Thermal resistance	Diffusion resistance
	Symbol	d	ρ	λ	c	μ	R_i	$R_{d,j} \times 10^{-9}$
	Unit	m	kg/m ³	W/(m.K)	J/(kg.K)	(-)	m ² .K/W	m/s
1	Reinforced concrete	0.150	2400	1.580	1020	29.0	0.095	23.11
2	Polystyrene foam	0.060	30	0.070*	1270	50.0	0.857	15.94
3	Reinforced concrete	0.060	2400	1.580	1020	29.0	0.038	9.24
NOTE: The value λ W/(m.K) of the second layer is considered with a degradation influence (leaking of cement grout into insulation during a manufacturing of external panels in precast concrete plant)								
Results of calculation of thermal-technical parameters								
Thermal resistance of a construction				$R = 0.990\text{ m}^2\cdot\text{K/W}$				
Diffusion resistance of a construction				$R_d = 48.29 \times 10^9\text{ m/s}$				
Thermal transmittance				$U = 0.862\text{ W/(m}^2\cdot\text{K)}$				
Internal surface temperature				$\theta_{si} = 16.08\text{ }^{\circ}\text{C}$				
Moisture regime				Water vapour condenses inside the construction				
Evaluation of a construction of the fragment								Rating
Thermal resistance		$R = 0.99\text{ m}^2\cdot\text{K/W} < R_N = 4.40\text{ m}^2\cdot\text{K/W}$ - standard value						not meet
Thermal transmittance		$U = 0.86\text{ W/(m}^2\cdot\text{K)} > U_N = 0.22\text{ W/(m}^2\cdot\text{K)}$ - standard value						not meet
Risk of growth of moulds		$\theta_{si} = 16.08\text{ }^{\circ}\text{C} > \theta_{si,80} + \Delta\theta_{si} = 12.82\text{ }^{\circ}\text{C}$						meet
Moisture regime		$M_c = 0.032\text{ kg/(m}^2\cdot\text{a)} < M_{ev} = 1.325\text{ kg/(m}^2\cdot\text{a)}$ - annual balance						meet
		$M_c = 0.032\text{ kg/(m}^2\cdot\text{a)} < M_{c,max} = 0.5\text{ kg/(m}^2\cdot\text{a)}$ - permissible amount						meet

Table 2.1.2 - Distribution of temperature and water vapour pressures in the external wall 1

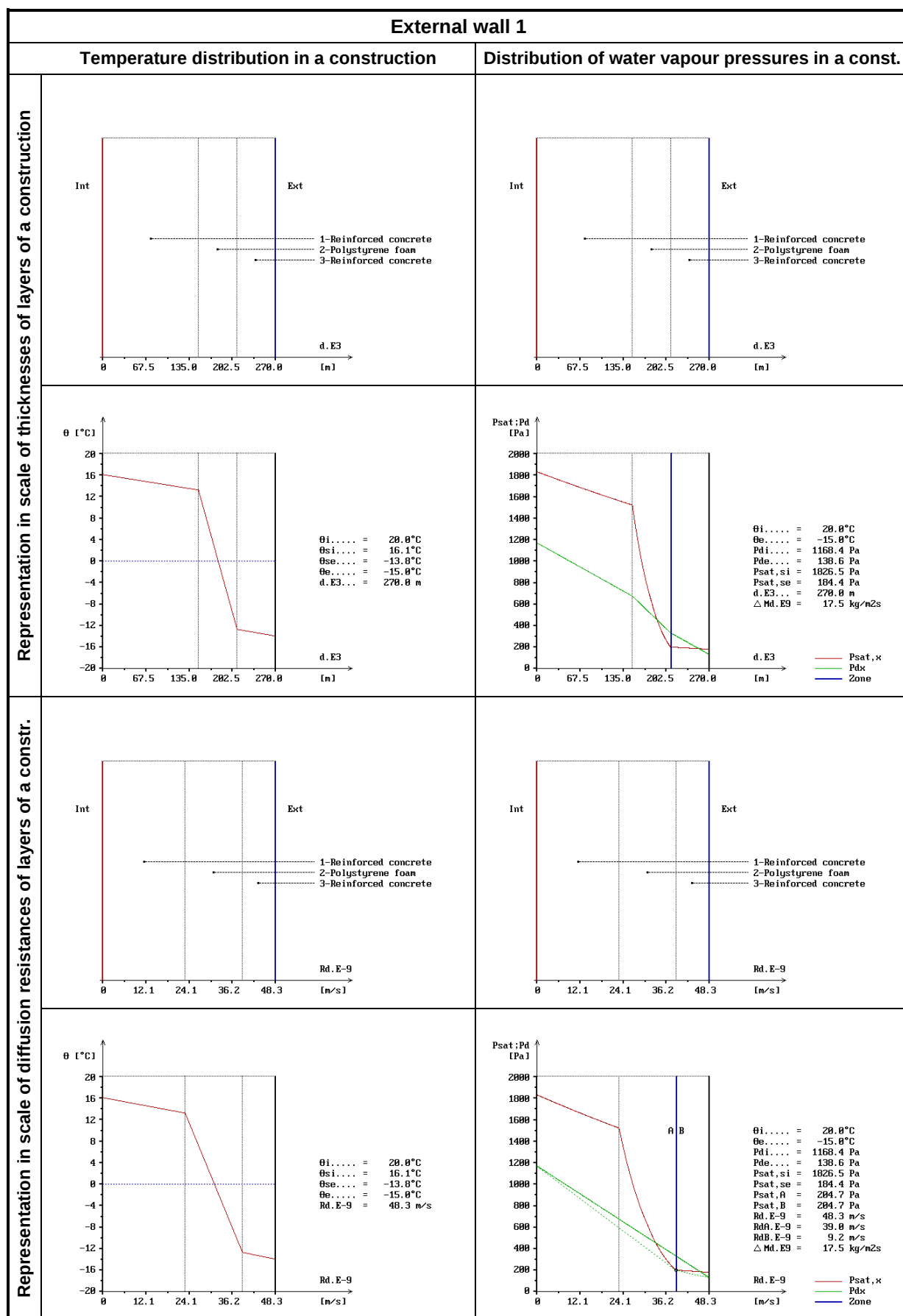


Table 2.2.1 - Thermal-technical properties and evaluation of external wall 2

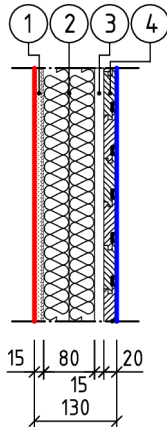
External wall 2 (loggia wall)								
Boundary conditions for interior $\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ $R_{si} = 0.13\text{ m}^2.\text{K/W}$						Boundary conditions for exterior $\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ $R_{se} = 0.04\text{ m}^2.\text{K/W}$		
No.	Material	Thickness	Apparent density	Thermal conductivity coefficient	Specific thermal capacity	Diffusion resistance factor	Thermal resistance	Diffusion resistance
	Symbol	d	ρ	λ	c	μ	R_i	$R_{d,j} \times 10^{-9}$
	Unit	m	kg/m ³	W/(m.K)	J/(kg.K)	(-)	m ² .K/W	m/s
1	Particle board	0.015	800	0.110	1500	12.5	0.136	1.00
2	Basalt wool	0.080	95	0.070	800	1.1	1.143	0.47
3	Closed air gap	0.015	1.2	0.090	1010	1.0	0.167	0.08
4	Batten siding	0.020	400	0.180	2510	157.0	0.111	16.68
Results of calculation of thermal-technical parameters								
Thermal resistance of a construction				$R = 1.557\text{ m}^2.\text{K/W}$				
Diffusion resistance of a construction				$R_d = 18.22 \times 10^{-9}\text{ m/s}$				
Thermal transmittance				$U = 0.579\text{ W}/(\text{m}^2.\text{K})$				
Internal surface temperature				$\theta_{si} = 17.37\text{ }^{\circ}\text{C}$				
Moisture regime				Water vapour condenses inside the construction				
Evaluation of a construction of the fragment							Rating	
Thermal resistance		$R = 1.56\text{ m}^2.\text{K/W} < R_N = 4.40\text{ m}^2.\text{K/W}$ - standard value					not meet	
Thermal transmittance		$U = 0.58\text{ W}/(\text{m}^2.\text{K}) > U_N = 0.22\text{ W}/(\text{m}^2.\text{K})$ - standard value					not meet	
Risk of growth of moulds		$\theta_{si} = 17.37\text{ }^{\circ}\text{C} > \theta_{si,80} + \Delta\theta_{si} = 12.82\text{ }^{\circ}\text{C}$					meet	
Moisture regime		$M_c = 4.386\text{ kg}/(\text{m}^2.\text{a}) < M_{ev} = 6.856\text{ kg}/(\text{m}^2.\text{a})$ - annual balance					meet	
		$M_c = 4.386\text{ kg}/(\text{m}^2.\text{a}) > M_{c,max} = 0.5\text{ kg}/(\text{m}^2.\text{a})$ - permissible amount					not meet	

Table 2.2.2 - Distribution of temperature and water vapour pressures in external wall 2

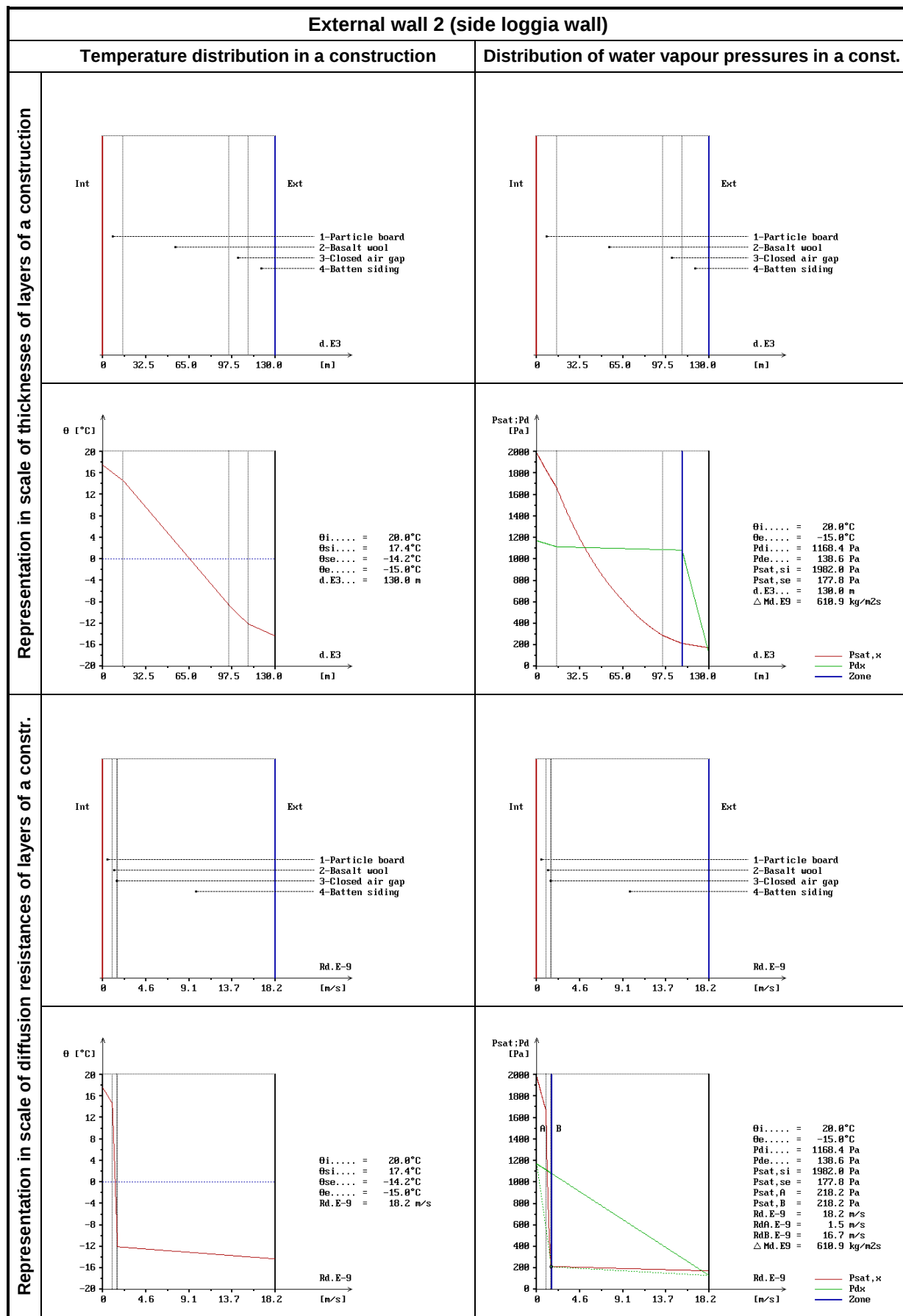


Table 2.3.1 - Thermal-technical properties and evaluation of flat roof

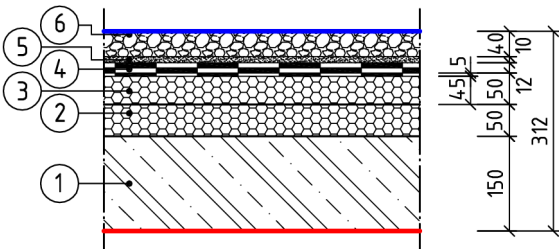
Flat roof								
Boundary conditions for interior						Boundary conditions for exterior		
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ $R_{si} = 0.10\text{ m}^2\cdot\text{K/W}$						$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$		
No.	Material	Thickness	Apparent density	Thermal conductivity coefficient	Specific thermal capacity	Diffusion resistance factor	Thermal resistance	Diffusion resistance
	Symbol	d	ρ	λ	c	μ	R_i	$R_{d,j} \times 10^{-9}$
	Unit	m	kg/m ³	W/(m.K)	J/(kg.K)	(-)	m ² .K/W	m/s
1	Reinforced concrete	0.150	2400	1.580	1020	29.0	0.095	23.11
2	Polystyrene foam	0.050	30	0.044	1270	50.0	1.136	13.28
3	Boards POLSID	0.045*	25	0.044	1270	45.0	1.023	10.76
4	Waterproof. membrane	0.017*	900	0.210	1470	19375.0	0.081	1749.8
5	Sand	0.010	1750	0.950	960	4.0	0.011	0.21
6	Gravel	0.040	1650	0.750	960	20.0	0.053	4.25
NOTE: Thermal insulation boards POLSID (total thickness 50 mm) is composed of polystyrene foam (45 mm) and bituminous strip (5 mm). The thickness of bituminous strip is included in the thickness of waterproofing membrane (layer No. 4).								
Results of calculation of thermal-technical parameters								
Thermal resistance of a construction				$R = 2.399\text{ m}^2\cdot\text{K/W}$				
Diffusion resistance of a construction				$R_d = 1801.37 \times 10^{-9}\text{ m/s}$				
Thermal transmittance				$U = 0.394\text{ W/(m}^2\cdot\text{K)}$				
Internal surface temperature				$\theta_{si} = 18.62\text{ }^{\circ}\text{C}$				
Moisture regime				Water vapour condenses inside the construction				
Evaluation of a construction of the fragment							Rating	
Thermal resistance		$R = 2.40\text{ m}^2\cdot\text{K/W} < R_N = 6.50\text{ m}^2\cdot\text{K/W}$ - standard value					not meet	
Thermal transmittance		$U = 0.39\text{ W/(m}^2\cdot\text{K)} > U_N = 0.15\text{ W/(m}^2\cdot\text{K)}$ - standard value					not meet	
Risk of growth of moulds		$\theta_{si} = 18.62\text{ }^{\circ}\text{C} > \theta_{si,80} + \Delta\theta_{si} = 12.82\text{ }^{\circ}\text{C}$					meet	
Moisture regime		$M_c = 0.153\text{ kg/(m}^2\cdot\text{a)} < M_{ev} = 0.210\text{ kg/(m}^2\cdot\text{a)}$ - annual balance					meet	
		$M_c = 0.153\text{ kg/(m}^2\cdot\text{a)} > M_{c,max} = 0.1\text{ kg/(m}^2\cdot\text{a)}$ - permissible amount					not meet	

Table 2.3.2 - Distribution of temperature and water vapour pressures in flat roof

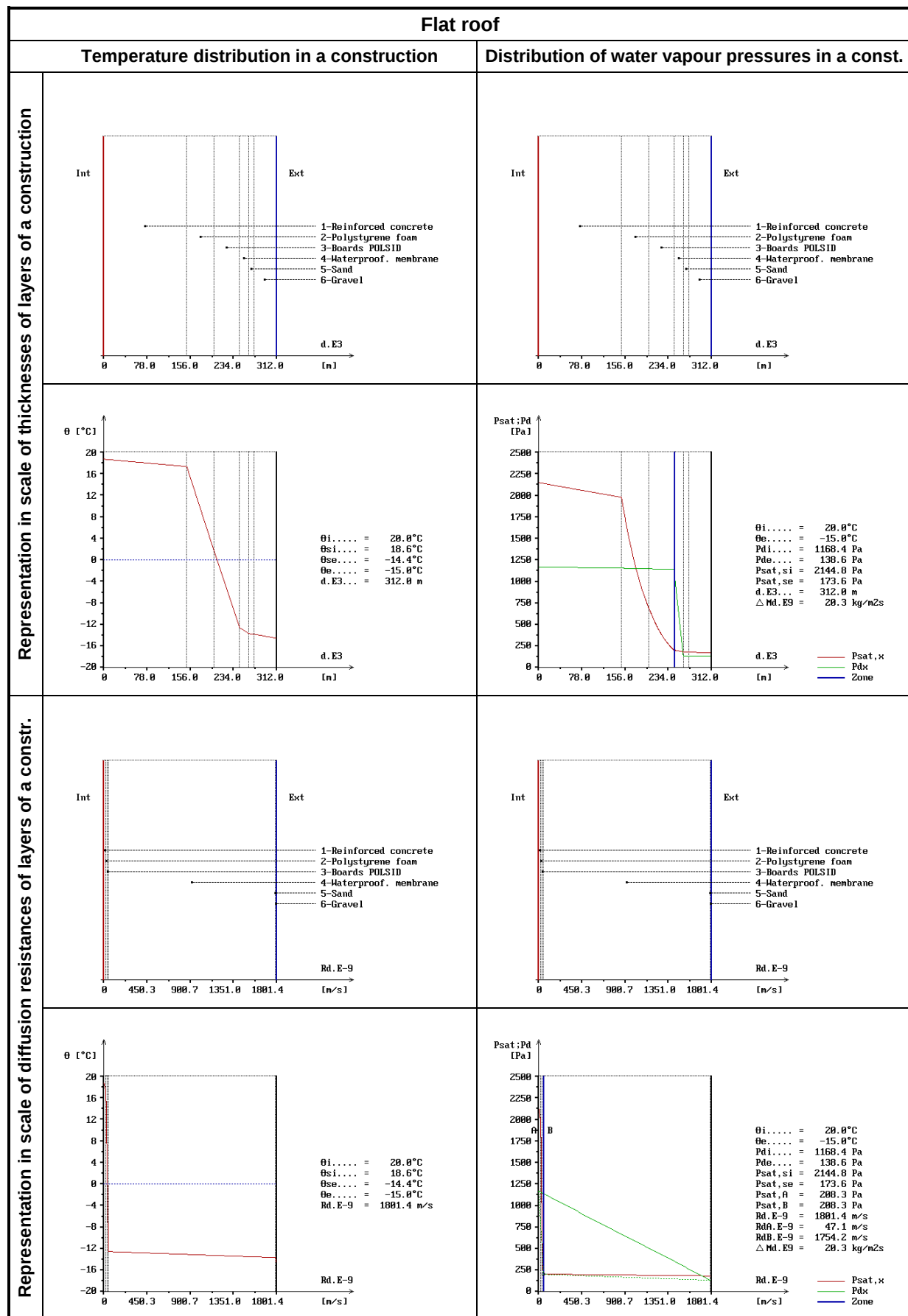


Table 2.4.1 - Thermal-technical properties and evaluation of floor on the ceiling

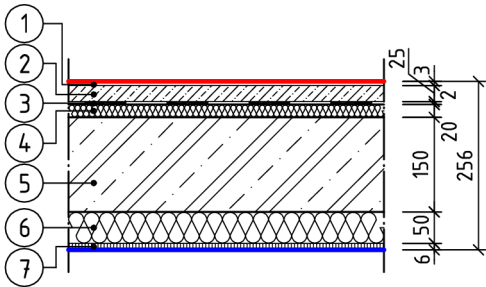
Floor on the ceiling (above the unheated space)								
Boundary conditions for interior $\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ $R_{si} = 0.17\text{ m}^2.\text{K/W}$						Boundary conditions for exterior (unheated basement) $\theta_e = 2.5\text{ }^{\circ}\text{C}$ $\varphi_e = 60\%$ $R_{se} = 0.17\text{ m}^2.\text{K/W}$		
No.	Material	Thickness	Apparent density	Thermal conductivity coefficient	Specific thermal capacity	Diffusion resistance factor	Thermal resistance	Diffusion resistance
	Symbol	d	ρ	λ	c	μ	R_i	$R_{d,j} \times 10^{-9}$
	Unit	m	kg/m ³	W/(m.K)	J/(kg.K)	(-)	m ² .K/W	m/s
1	PVC + adhesive	0.003	1400	0.160	1100	17110.0	0.019	272.68
2	Cement coating	0.025	2000	1.020	840	19.0	0.025	2.52
3	Tar paper	0.002	700	0.210	1470	9410.0	0.010	99.98
4	Boards FIBREX	0.020	115	0.050	840	2.0	0.400	0.21
5	Reinforced concrete	0.150	2400	1.340	1020	29.0	0.112	23.11
6	Basalt felt	0.050	95	0.060	800	1.1	0.833	0.29
7	Particle boards	0.006	1040	0.220	1580	6.5	0.027	0.21
Results of calculation of thermal-technical parameters								
Thermal resistance of a construction				$R = 1.425\text{ m}^2.\text{K/W}$				
Diffusion resistance of a construction				$R_d = 399.01 \times 10^{-9}\text{ m/s}$				
Thermal transmittance				$U = 0.566\text{ W}/(\text{m}^2.\text{K})$				
Internal surface temperature				$\theta_{si} = 18.31\text{ }^{\circ}\text{C}$				
Moisture regime				Water vapour does not condense inside the construct.				
Thermal effusivity of the floor				$b = 806.02\text{ W.s}^{1/2}/(\text{m}^2.\text{K})$				
Decrease of contact temperature of the floor				$\Delta\theta_{10} = 6.16\text{ }^{\circ}\text{C}$				
Evaluation of a construction of the fragment							Rating	
Thermal resistance		$R = 1.43\text{ m}^2.\text{K/W} < R_N = 1.70\text{ m}^2.\text{K/W}$ - standard value					not meet	
Thermal transmittance		$U = 0.57\text{ W}/(\text{m}^2.\text{K}) > U_N = 0.50\text{ W}/(\text{m}^2.\text{K})$ - standard value					not meet	
Risk of growth of moulds		$\theta_{si} = 18.31\text{ }^{\circ}\text{C} > \theta_{si,80} + \Delta\theta_{si} = 13.12\text{ }^{\circ}\text{C}$					meet	
Thermal effusivity		$b = 806\text{ W.s}^{1/2}/(\text{m}^2.\text{K}) \in b_N(701 - 850)$ - less warm floor					not meet	

Table 2.4.2 - Distribution of temperature and water vapour pressures in floor on the ceiling

Floor on the ceiling (above the unheated space)			
Temperature distribution in a construction		Distribution of water vapour pressures in a const.	
Representation in scale of thicknesses of layers of a construction	Int Ext 1-PVC + adhesive 2-Cement coating 3-Tar paper 4-Boards FIBREX 5-Reinforced concrete 6-Basalt felt 7-Particle boards d.E3 0 64.0 128.0 192.0 256.0 [m]	Int Ext 1-PVC + adhesive 2-Cement coating 3-Tar paper 4-Boards FIBREX 5-Reinforced concrete 6-Basalt felt 7-Particle boards d.E3 0 64.0 128.0 192.0 256.0 [m]	
	θ [°C] d.E3 0 64.0 128.0 192.0 256.0 [m] θ_i..... = 20.0°C θ_{si}..... = 18.3°C θ_{se}..... = 4.2°C θ_e..... = 2.5°C d.E3... = 256.0 m	Psat;Pd [Pa] d.E3 0 64.0 128.0 192.0 256.0 [m] θ_i..... = 20.0°C θ_e..... = 2.5°C P_{di}..... = 1168.4 Pa P_{de}..... = 438.7 Pa $P_{sat, si}$ = 2104.0 Pa $P_{sat, se}$ = 823.0 Pa d.E3... = 256.0 m Md.E9 = 1.8 kg/m²s — Psat,x — Pdx	
Representation in scale of diffusion resistances of layers of a constr.	Int Ext 1-PVC + adhesive 2-Cement coating 3-Tar paper 4-Boards FIBREX 5-Reinforced concrete 6-Basalt felt 7-Particle boards Rd.E-9 0 99.8 199.5 299.3 399.0 [m²/s]	Int Ext 1-PVC + adhesive 2-Cement coating 3-Tar paper 4-Boards FIBREX 5-Reinforced concrete 6-Basalt felt 7-Particle boards Rd.E-9 0 99.8 199.5 299.3 399.0 [m²/s]	
	θ [°C] Rd.E-9 0 99.8 199.5 299.3 399.0 [m²/s] θ_i..... = 20.0°C θ_{si}..... = 18.3°C θ_{se}..... = 4.2°C θ_e..... = 2.5°C Rd.E-9 = 399.0 m²/s	Psat;Pd [Pa] Rd.E-9 0 99.8 199.5 299.3 399.0 [m²/s] θ_i..... = 20.0°C θ_e..... = 2.5°C P_{di}..... = 1168.4 Pa P_{de}..... = 438.7 Pa $P_{sat, si}$ = 2104.0 Pa $P_{sat, se}$ = 823.0 Pa Rd.E-9 = 399.0 m²/s Md.E9 = 1.8 kg/m²s — Psat,x — Pdx	

Table 2.5.1 - Thermal-technical properties and evaluation of ceiling above the exterior

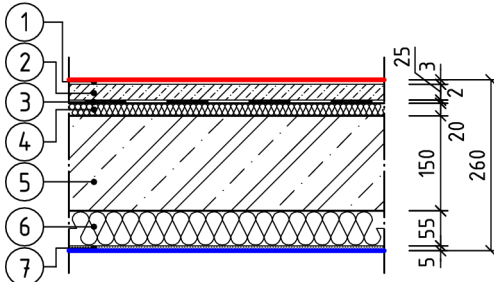
Ceiling above the exterior								
Boundary conditions for interior						Boundary conditions for exterior		
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ $R_{si} = 0.17\text{ m}^2\cdot\text{K/W}$						$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$		
No.	Material	Thickness	Apparent density	Thermal conductivity coefficient	Specific thermal capacity	Diffusion resistance factor	Thermal resistance	Diffusion resistance
	Symbol	d	ρ	λ	c	μ	R_j	$R_{d,j} \times 10^{-9}$
	Unit	m	kg/m ³	W/(m.K)	J/(kg.K)	(-)	m ² .K/W	m/s
1	PVC + adhesive	0.003	1400	0.160	1100	17110.0	0.019	272.68
2	Cement coating	0.025	2000	1.160	840	19.0	0.022	2.52
3	Tar paper	0.002	700	0.210	1470	9410.0	0.010	99.98
4	Boards FIBREX	0.020	115	0.052	840	2.0	0.385	0.21
5	Reinforced concrete	0.150	2400	1.580	1020	29.0	0.095	23.11
6	Boards LIGNOPOR	0.055	95	0.047	800	1.1	1.170	0.32
7	Plaster UNIFAS	0.005	2000	0.990	790	19.0	0.005	0.50
Results of calculation of thermal-technical parameters								
Thermal resistance of a construction				$R = 1.705\text{ m}^2\cdot\text{K/W}$				
Diffusion resistance of a construction				$R_d = 399.33 \times 10^9\text{ m/s}$				
Thermal transmittance				$U = 0.522\text{ W}/(\text{m}^2\cdot\text{K})$				
Internal surface temperature				$\theta_{si} = 16.89\text{ }^{\circ}\text{C}$				
Moisture regime				Water vapour does not condense inside the construct.				
Thermal effusivity of the floor				$b = 782.28\text{ W}\cdot\text{s}^{1/2}/(\text{m}^2\cdot\text{K})$				
Decrease of contact temperature of the floor				$\Delta\theta_{10} = 6.63\text{ }^{\circ}\text{C}$				
Evaluation of a construction of the fragment							Rating	
Thermal resistance		$R = 1.71\text{ m}^2\cdot\text{K/W} < R_N = 1.70\text{ m}^2\cdot\text{K/W}$ - standard value					not meet	
Thermal transmittance		$U = 0.52\text{ W}/(\text{m}^2\cdot\text{K}) > U_N = 0.15\text{ W}/(\text{m}^2\cdot\text{K})$ - standard value					not meet	
Risk of growth of moulds		$\theta_{si} = 16.89\text{ }^{\circ}\text{C} > \theta_{si,80} + \Delta\theta_{si} = 13.12\text{ }^{\circ}\text{C}$					meet	
Thermal effusivity		$b = 782\text{ W}\cdot\text{s}^{1/2}/(\text{m}^2\cdot\text{K}) \in b_N(701 - 850)$ - less warm floor					not meet	

Table 2.5.2 - Distribution of temperature and water vapour pressures in floor on the ceiling

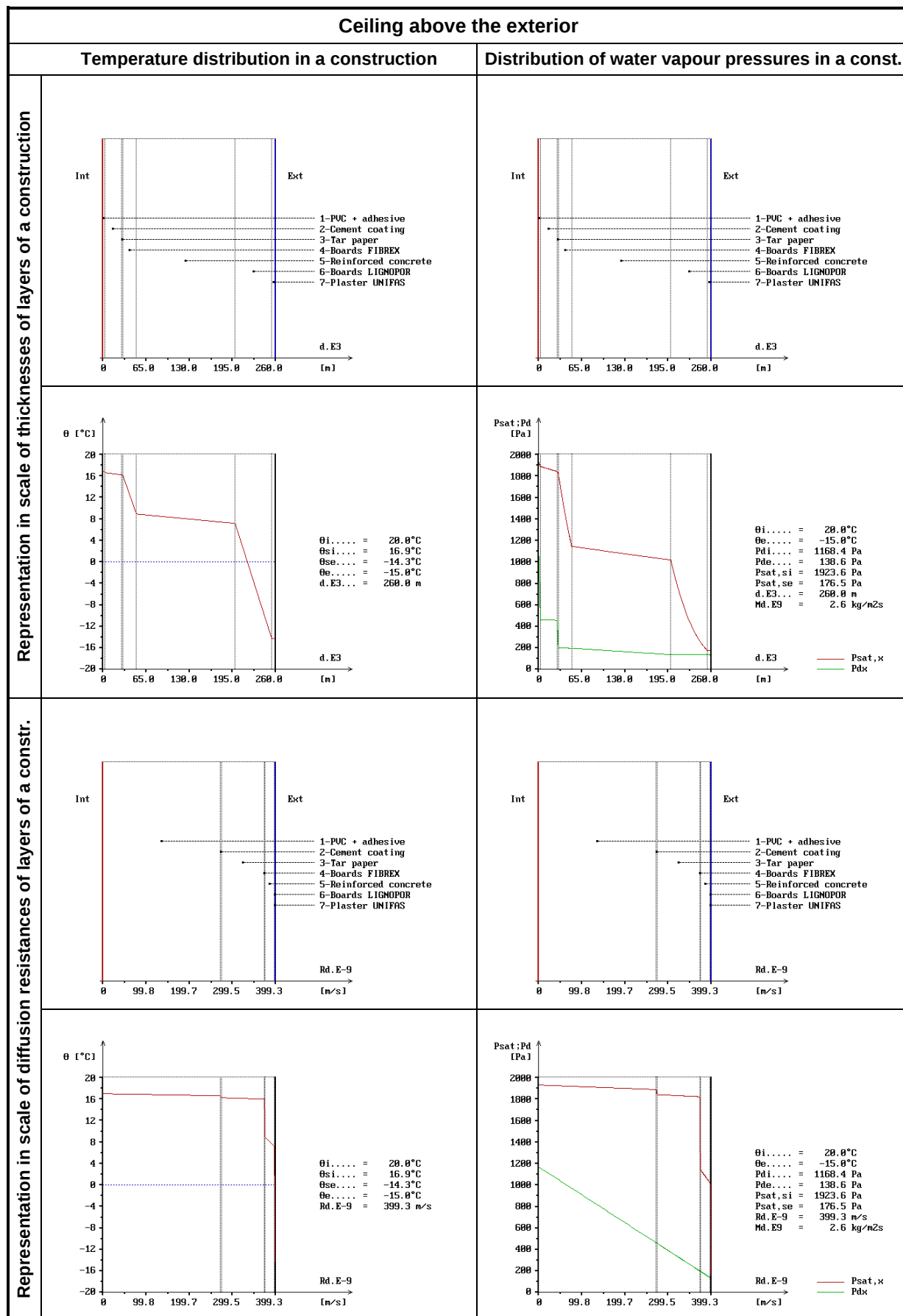


Table 2.6 - Thermal-technical properties and evaluation of wooden windows

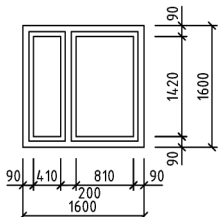
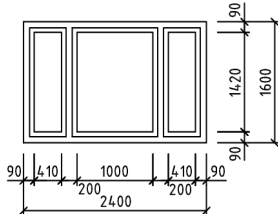
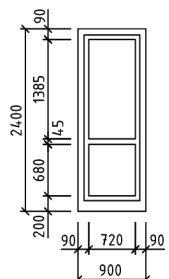
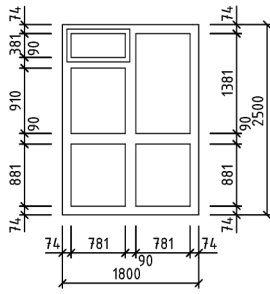
Order number	Number	Scheme of windows	Length of joints of windows / (m)	Gap permeability coefficient $i_{lv} \times 10^4$ (m ³ /(m.s.Pa ^{0.67}))	U_f (W/(m ² .K))	A_f (m ²)	U_{g_g} (W/(m ² .K))	A_{g_g} (m ²)	ψ_g (W/(m.K))	l_g (m)	A_w (m ²)
					Thermal transmittance of windows (W/(m ² .K)) $U_w = \frac{U_f \cdot A_f + U_g \cdot A_g + \psi_g \cdot l_g}{A_w}$						
1	152		8.836	1.4	1.627	0.828	2.798	1.732	0.050	8.120	2.560
					2.578						
2	24		13.232	1.4	1.627	1.256	2.798	2.584	0.050	12.160	3.840
					2.573						
3	24		6.240	1.4	1.627	0.673	2.798	1.487	0.050	7.010	2.160
					2.595						
Wooden: $\Sigma l = 1810.400$ m ²					Calculated air change rate is given in the next table Weighted average thermal transmittance of windows (W/(m ² .K)) $U_w = \frac{\sum (A_{wi} \cdot U_{wi})}{\sum A_{wi}}$						
$\sum (A_{wi} \cdot U_{wi})$ (W/K)		$\sum A_{wi}$ (m ²)									
1374.873		533.120			2.579						
Evaluation		$U_w = 2.58$ W/(m ² .K) > $U_{w.N} = 0.85$ W/(m ² .K) – not meet									

Table 2.7 - Thermal-technical properties and evaluation of steel windows

Order number	Number	Scheme of windows	Length of joints of windows <i>l</i> (m)	Gap permeability coefficient <i>i</i> _{LV} ×10 ⁴ (m ³ /(m.s.Pa ^{0.67}))	<i>U</i> _f (W/(m ² .K))	<i>A</i> _f (m ²)	<i>U</i> _g (W/(m ² .K))	<i>A</i> _g (m ²)	<i>ψ</i> _g (W/(m.K))	<i>l</i> _g (m)	<i>A</i> _w ² (m ²)
					Thermal transmittance of windows (W/(m ² .K)) $U_w = \frac{U_f \cdot A_f + U_g \cdot A_g + \psi_g \cdot l_g}{A_w}$						
1	8		2.652	1.4	5.900	1.037	5.747	3.463	0.123	16.678	4.500
					6.238						
Steel: Σ <i>l</i> = 21.216 m					Calculated air change rate taking into account also values from the previous table						
Wooden and steel: Σ <i>l</i> = 1831.62 m Volume of building: <i>V</i> _b = 10075.30 m ³					Calculated air change rate (1/h) $n = 25200 \frac{\sum (i_{LV} \cdot l)}{V_b} = 0.64$						
$\sum (A_{wi} \cdot U_{wi})$ (W/K)		$\sum A_{wi}$ (m ²)		Weighted average thermal transmittance of windows (W/(m ² .K)) $U_w = \frac{\sum (A_{wi} \cdot U_{wi})}{\sum A_{wi}}$							
224.568		36.00		6.238							
Evaluation		<i>U</i> _w = 6.24 W/(m ² .K) > <i>U</i> _{w.N} = 0.85 W/(m ² .K) – not meet									

3 Evaluation on Dew Point Temperature and Calculation of Thermal Transmittance of Windows for the Modeled Details

Table 3.1.1 – Thermal-technical properties and a construction of wooden window

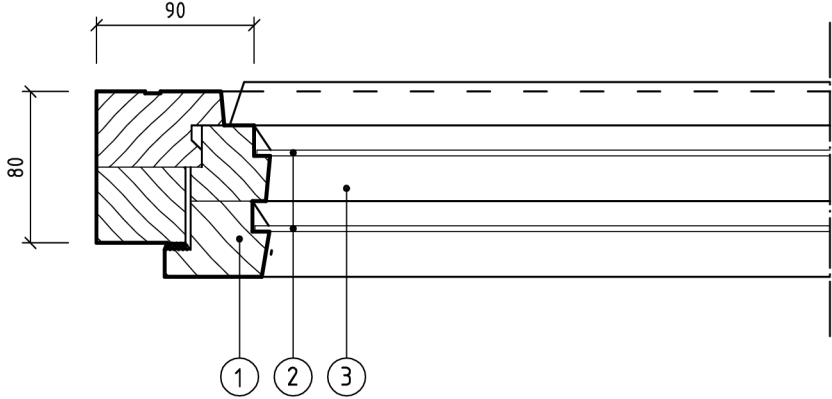
WOODEN WINDOW

Legend: 1. Wooden double window ($\lambda = 0.18 \text{ W/(m.K)}$) 2. Glass 3 mm ($\lambda = 1.00 \text{ W/(m.K)}$) 3. Closed air gap 37 mm ($\lambda = 0.204 \text{ W/(m.K)}$)
NOTE: Loggia doors are modeled like windows $U_{\text{window, wooden}} = 2.579 \text{ W/(m}^2\text{.K)}$ – see table 2.6

Table 3.1.2 – Boundary conditions for a calculation of wooden window

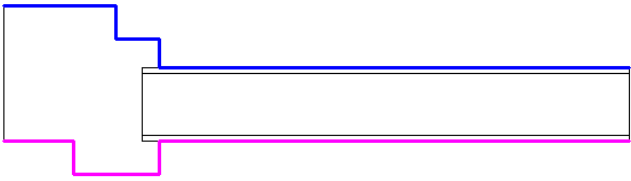
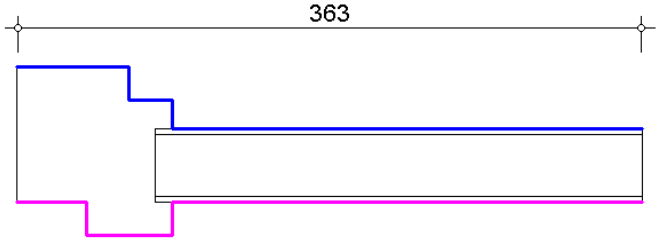
WOODEN WINDOW	
Boundary conditions for a calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ }\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ }\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding length of window for a calculation of the thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ }\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ }\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 3.1.3 – Thermal-technical evaluation of the wooden window

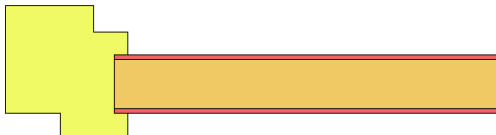
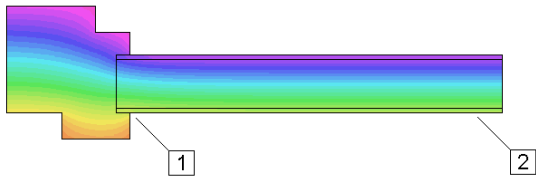
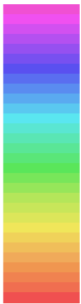
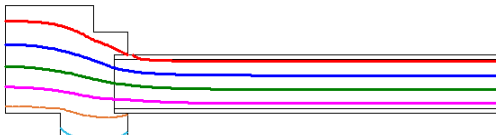
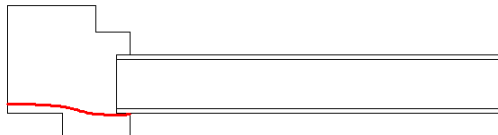
WOODEN WINDOW																								
Modeled detail with marking the materials			Temperature field with marked critical temperatures																					
																								
Legend: $\lambda = 1.000 \text{ W/(m.K)}$ $\lambda = 0.204 \text{ W/(m.K)}$ $\lambda = 0.180 \text{ W/(m.K)}$			 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
-15.0 °C	... -11.5 °C																							
-11.5 °C	... -8.0 °C																							
-8.0 °C	... -4.5 °C																							
-4.5 °C	... -1.0 °C																							
-1.0 °C	... 2.5 °C																							
2.5 °C	... 6.0 °C																							
6.0 °C	... 9.5 °C																							
9.5 °C	... 13.0 °C																							
13.0 °C	... 16.5 °C																							
16.5 °C	... 20.0 °C																							
Representation of characteristic isotherms			Representation of the critical isotherm																					
																								
-10 °C -5 °C 0 °C 5 °C 10 °C 15 °C			9.26 °C																					
Point	Temperature	Temperat. factor	Evaluation on dew point temperature	Rating																				
1	$\theta_{Si} = 8.63 \text{ °C}$	$f_{Rsi} = 0.675$	$\theta_{Si} = 7.27 \text{ °C} < \theta_{dp} = 9.26 \text{ °C}$	not meet																				
2	$\theta_{Si} = 7.27 \text{ °C}$	$f_{Rsi} = 0.636$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																					
Thermal transmittance			$U = 0.93630 / 0.363 = 2.579 \text{ W/(m}^2 \cdot \text{K)}$																					

Table 3.2.1 – Thermal-technical properties and a construction of steel window

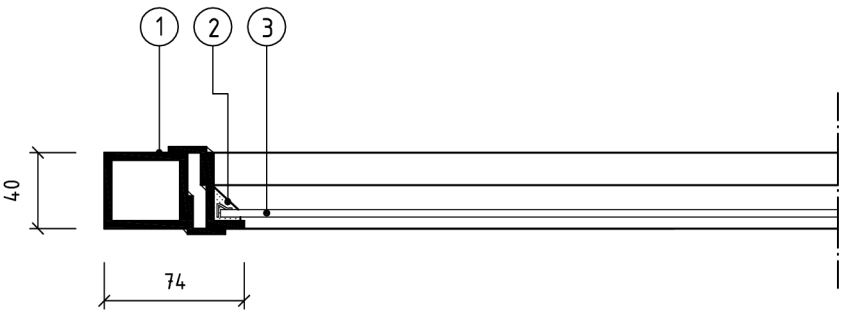
STEEL WINDOW
 Legend: 1. Steel window ($\lambda = 50 \text{ W/(m.K)}$ and $\lambda = 0.5 \text{ W/(m.K)}$) 2. Glazier's putty ($\lambda = 0.22 \text{ W/(m.K)}$) 3. Glass 4 mm ($\lambda = 1.00 \text{ W/(m.K)}$) $U_{\text{window, steel}} = 6.238 \text{ W/(m}^2\text{.K)}$ – see table 2.7

Table 3.2.2 – Boundary conditions for a calculation of steel window

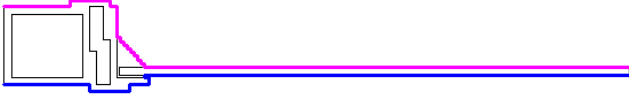
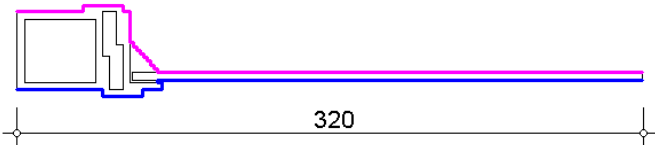
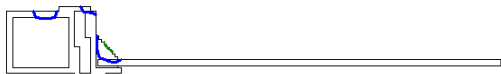
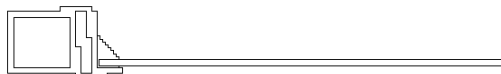
STEEL WINDOW	
Boundary conditions for a calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ }\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ }\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding length of window for a calculation of the thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ }\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ }\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 3.2.3 – Thermal-technical evaluation of the steel window

STEEL WINDOW				
Modeled detail with marking the materials			Temperature field with marked critical temperatures	
				
Legend: $\lambda = 1.000 \text{ W/(m.K)}$ $\lambda = 50.00 \text{ W/(m.K)}$ $\lambda = 0.220 \text{ W/(m.K)}$ $\lambda = 0.500 \text{ W/(m.K)}$			-15.0 °C ... -11.5 °C -11.5 °C ... -8.0 °C -8.0 °C ... -4.5 °C -4.5 °C ... -1.0 °C -1.0 °C ... 2.5 °C 2.5 °C ... 6.0 °C 6.0 °C ... 9.5 °C 9.5 °C ... 13.0 °C 13.0 °C ... 16.5 °C 16.5 °C ... 20.0 °C	
Representation of characteristic isotherms			Representation of the critical isotherm	
				
-10 °C -5 °C 0 °C 5 °C 10 °C 15 °C			9.26 °C	
Point	Temperature	Temperat. factor	Evaluation on dew point temperature	Rating
1	$\theta_{Si} = -4.66 \text{ °C}$	$f_{Rsi} = 0.295$	$\theta_{Si} = -6.15 \text{ °C} < \theta_{dp} = 9.26 \text{ °C}$	not meet
2	$\theta_{Si} = -6.15 \text{ °C}$	$f_{Rsi} = 0.253$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)	
Thermal transmittance			$U = 1.99612 / 0.320 = 6.238 \text{ W/(m}^2 \cdot \text{K)}$	

4 Evaluation of Hygienic Criterion and Calculation of the Linear Thermal Transmittance of Selected Details of the Building

Table 4.1.1 – Marking of the position of detail in the building – detail 01

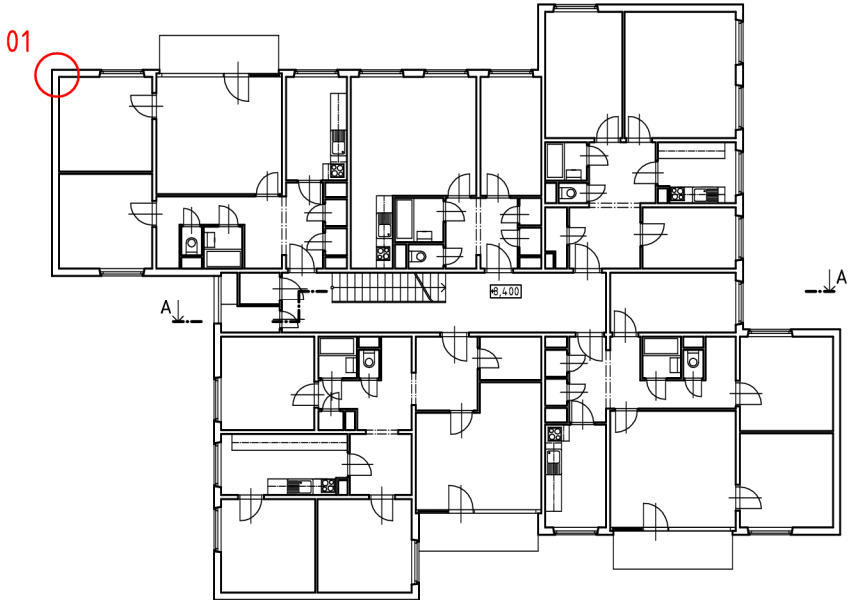
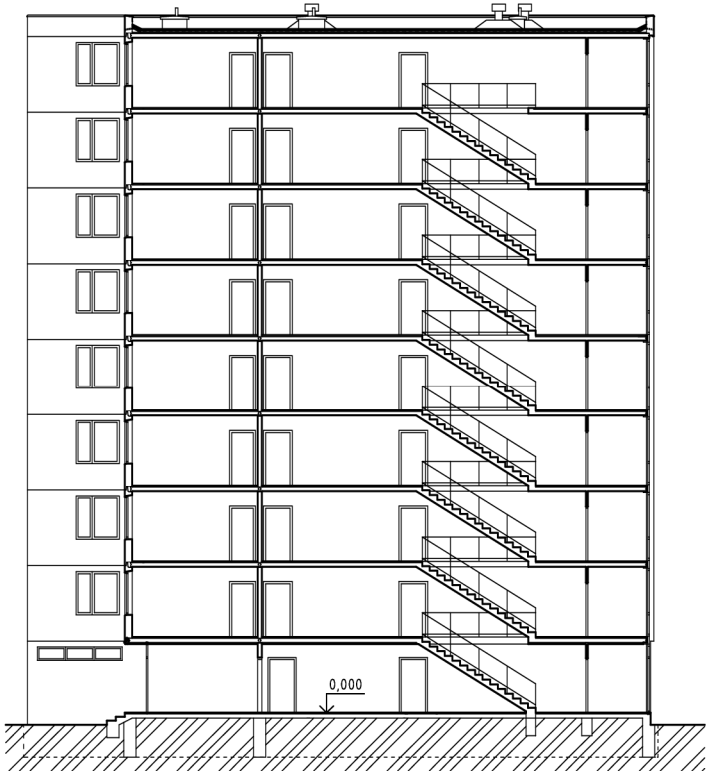
DETAIL 01
Floor plan

Section A-A


Table 4.1.2 – Structural composition of detail 01

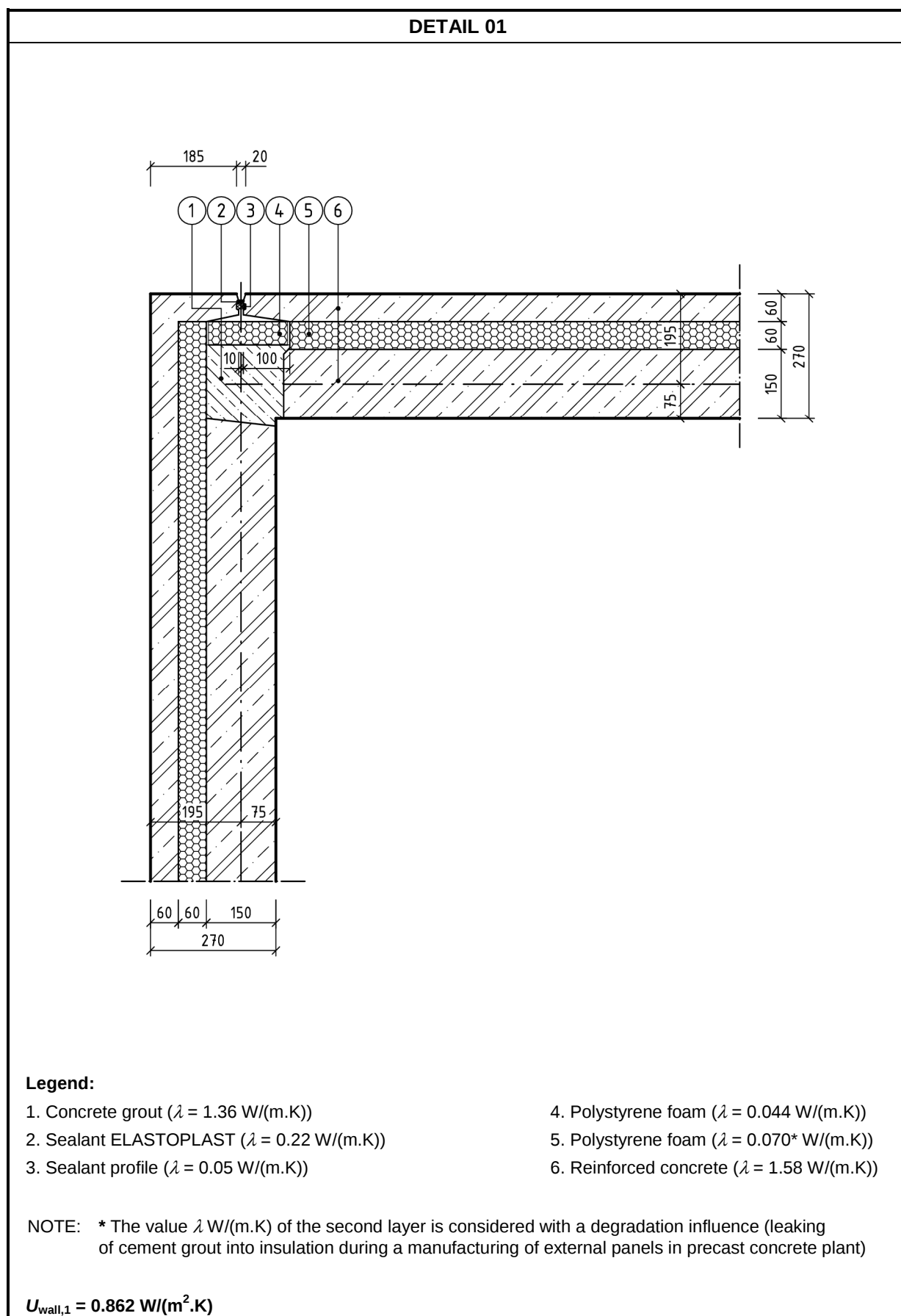


Table 4.1.3 – Boundary conditions for a calculation of detail 01

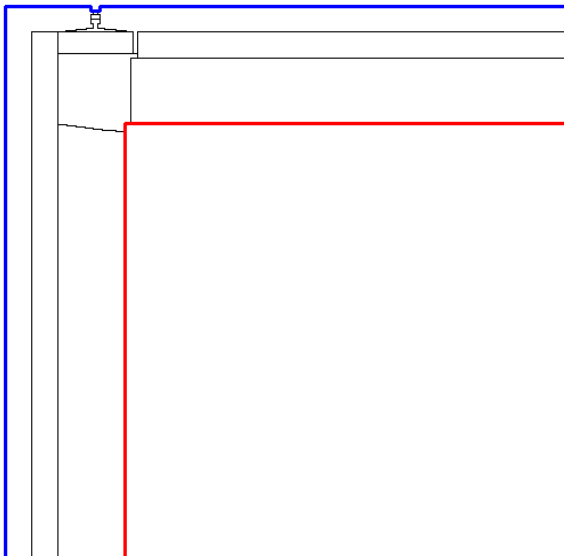
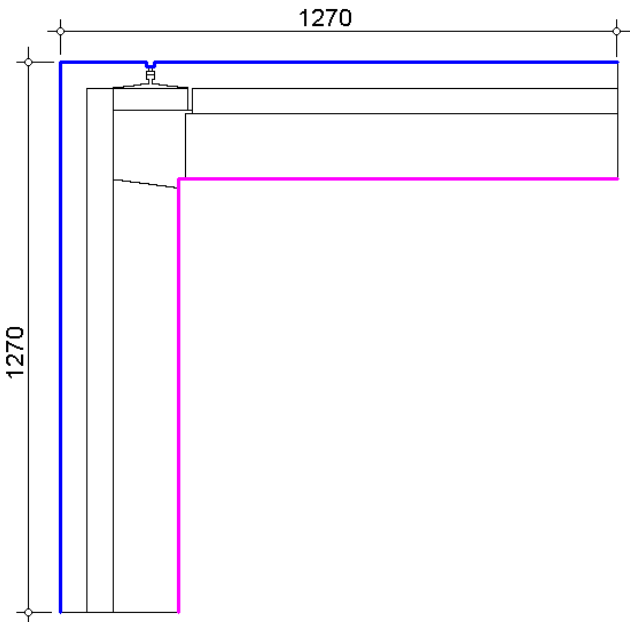
DETAIL 01	
Boundary conditions for a calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$

Table 4.1.4 – Thermal-technical evaluation of detail 01

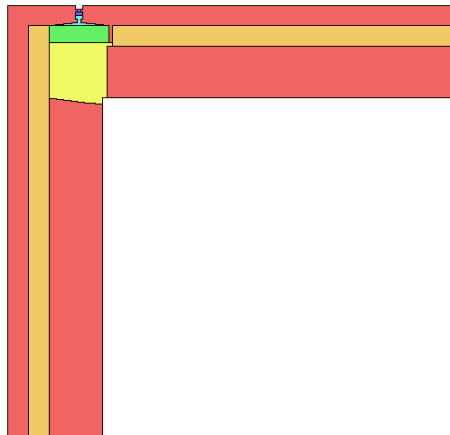
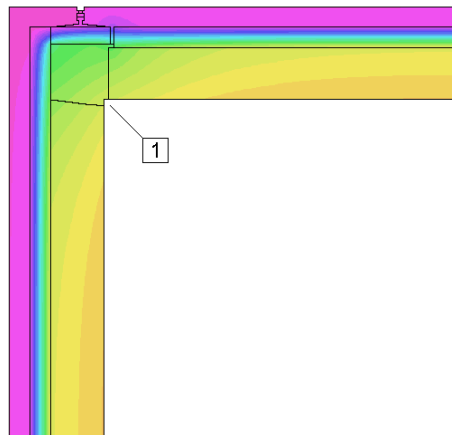
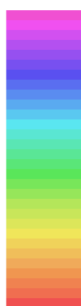
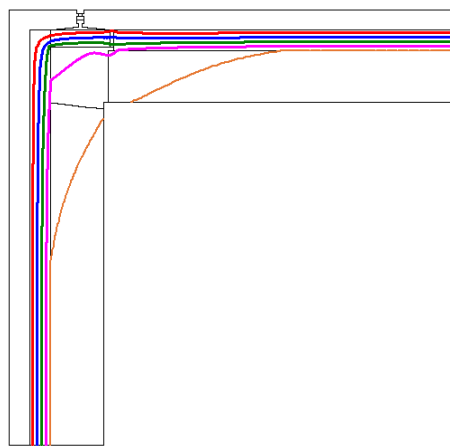
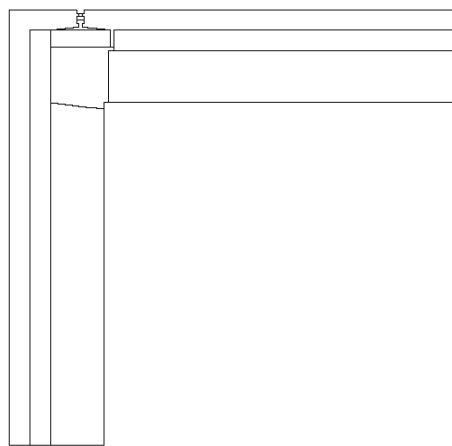
DETAIL 01																								
Modeled detail with marking the materials			Temperature field with marked critical temperatures																					
																								
Legend: ■ $\lambda = 1.580 \text{ W/(m.K)}$ ■ $\lambda = 0.070 \text{ W/(m.K)}$ ■ $\lambda = 1.360 \text{ W/(m.K)}$ ■ $\lambda = 0.044 \text{ W/(m.K)}$ ■ $\lambda = 0.119 \text{ W/(m.K)}$ ■ $\lambda = 0.050 \text{ W/(m.K)}$ ■ $\lambda = 0.220 \text{ W/(m.K)}$			 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
-15.0 °C	... -11.5 °C																							
-11.5 °C	... -8.0 °C																							
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-4.5 °C	... -1.0 °C																							
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2.5 °C	... 6.0 °C																							
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9.5 °C	... 13.0 °C																							
13.0 °C	... 16.5 °C																							
16.5 °C	... 20.0 °C																							
Representation of characteristic isotherms			Representation of the critical isotherm																					
																								
<table><tr><td>— -10 °C</td><td>— 5 °C</td></tr><tr><td>— -5 °C</td><td>— 10 °C</td></tr><tr><td>— 0 °C</td><td>— 15 °C</td></tr></table>			— -10 °C	— 5 °C	— -5 °C	— 10 °C	— 0 °C	— 15 °C	— 13.12 °C															
— -10 °C	— 5 °C																							
— -5 °C	— 10 °C																							
— 0 °C	— 15 °C																							
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																				
1	$\theta_{\text{Si}} = 9.05 \text{ °C}$	$f_{\text{Rsi}} = 0.687$	$\theta_{\text{Si}} = 9.05 \text{ °C} < \theta_{\text{Si},80} + \Delta\theta_{\text{Si}} = 13.12 \text{ °C}$	not meet																				
			$\theta_{\text{Si}} = f_{\text{Rsi}} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																					
Linear thermal transmittance			$\psi = 1.99724 - 0.862 \times (1.270 + 1.270) = -0.192 \text{ W/(m.K)}$																					

Table 4.2.1 – Marking of the position of detail in the building – detail 02

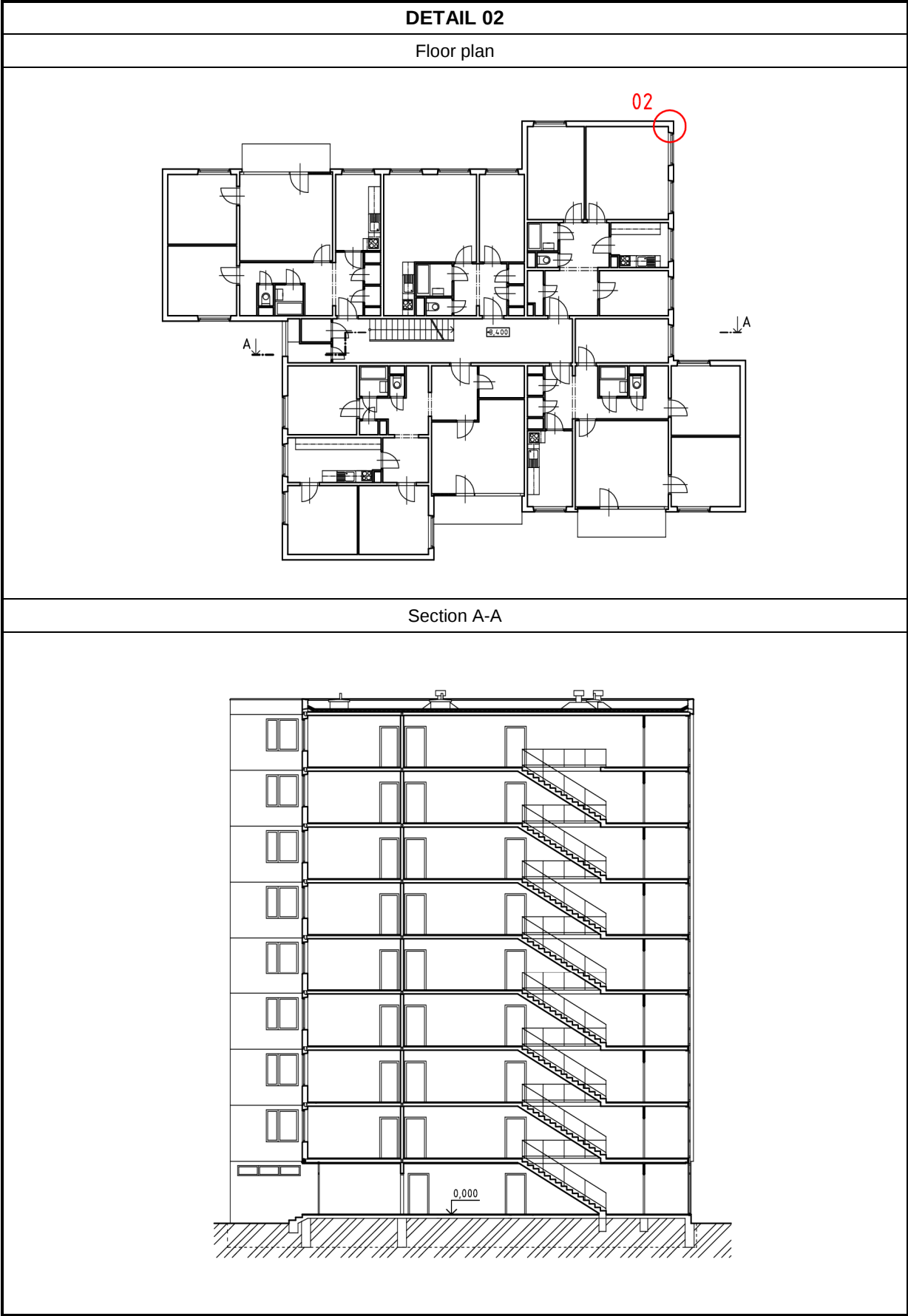


Table 4.2.2 – Structural composition of detail 02

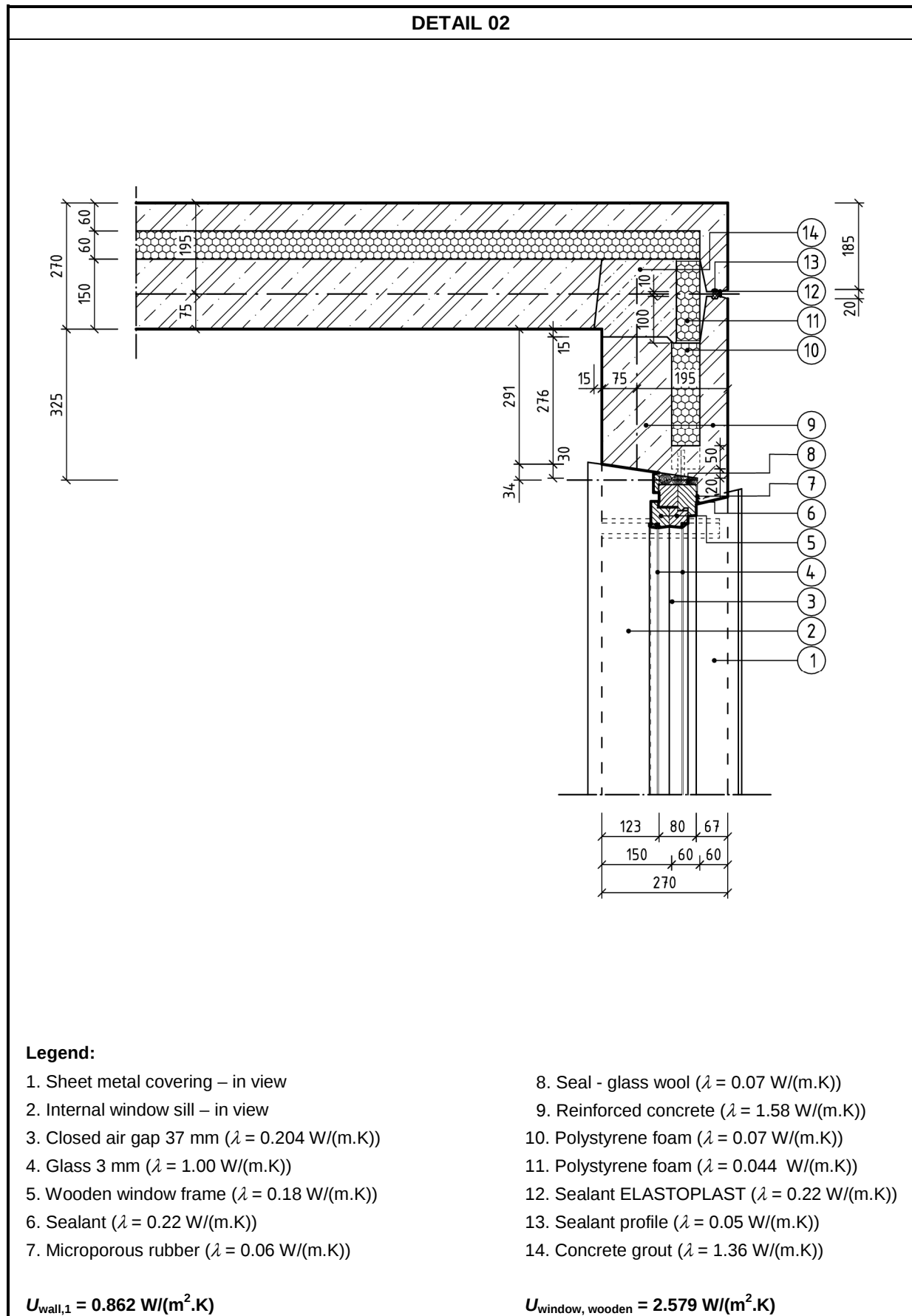


Table 4.2.3 – Boundary conditions for a calculation of detail 02

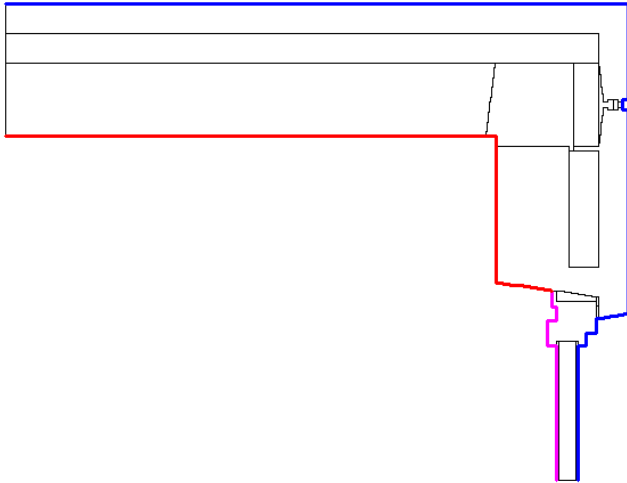
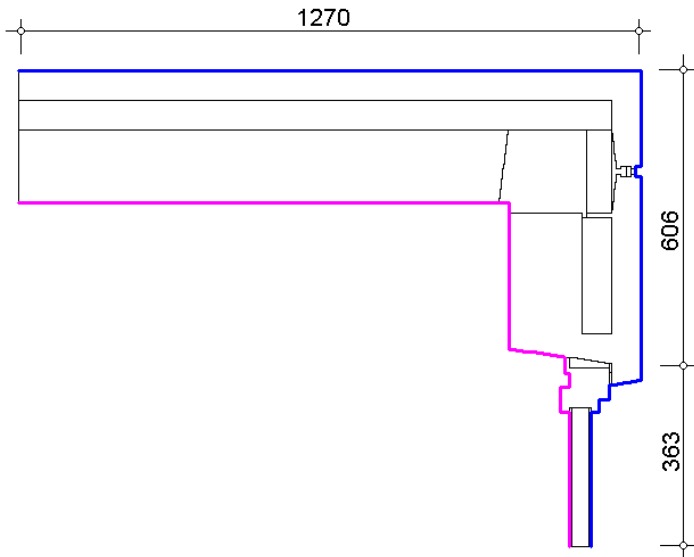
DETAIL 02	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\text{ %}$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\text{ %}$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\text{ %}$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\text{ %}$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$

Table 4.2.4 Thermal-technical evaluation of detail 02

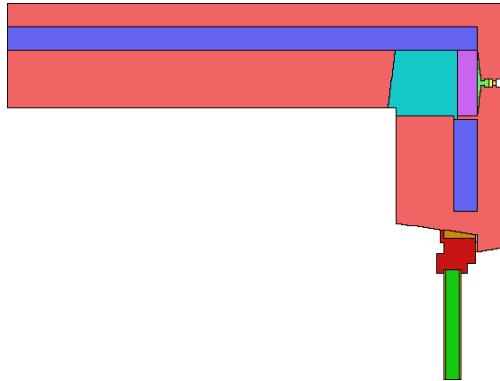
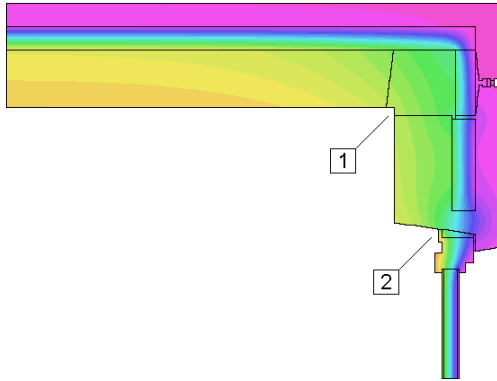
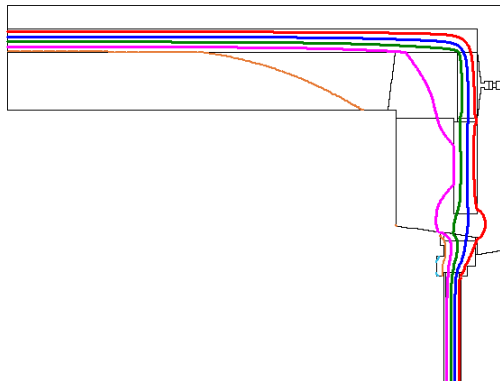
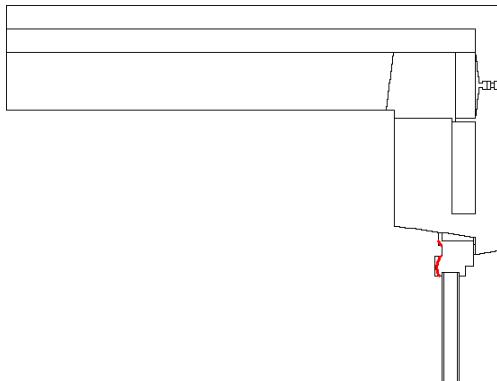
DETAIL 02																																																
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																													
																																																
Legend: <table><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.119 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.119 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$																																													
	$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$																																													
	$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																													
	$\lambda = 0.119 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$																																													
	$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$																																													
	$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$																																													
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13.0 °C	... 16.5 °C																																															
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Representation of characteristic isotherms			Representation of the critical isotherm																																													
																																																
<table><tr><td></td><td>-10 °C</td><td></td><td>5 °C</td></tr><tr><td></td><td>-5 °C</td><td></td><td>10 °C</td></tr><tr><td></td><td>0 °C</td><td></td><td>15 °C</td></tr></table>				-10 °C		5 °C		-5 °C		10 °C		0 °C		15 °C	13.12 °C																																	
	-10 °C		5 °C																																													
	-5 °C		10 °C																																													
	0 °C		15 °C																																													
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																												
1	$\theta_{Si} = 8.15 \text{ °C}$	$f_{Rsi} = 0.661$	$\theta_{Si} = 4.74 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																												
2	$\theta_{Si} = 4.74 \text{ °C}$	$f_{Rsi} = 0.564$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																													
Linear thermal transmittance		$\psi = 2.67538 - 0.862 \times (1.270 + 0.606) - 2.579 \times 0.363 = 0.122 \text{ W/(m.K)}$																																														

Table 4.3.1 – Marking of the position of detail in the building – detail 03

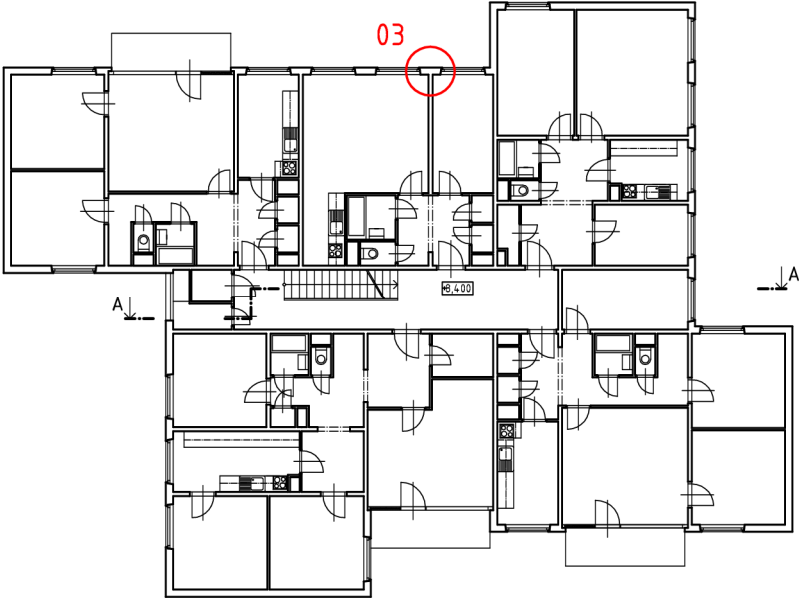
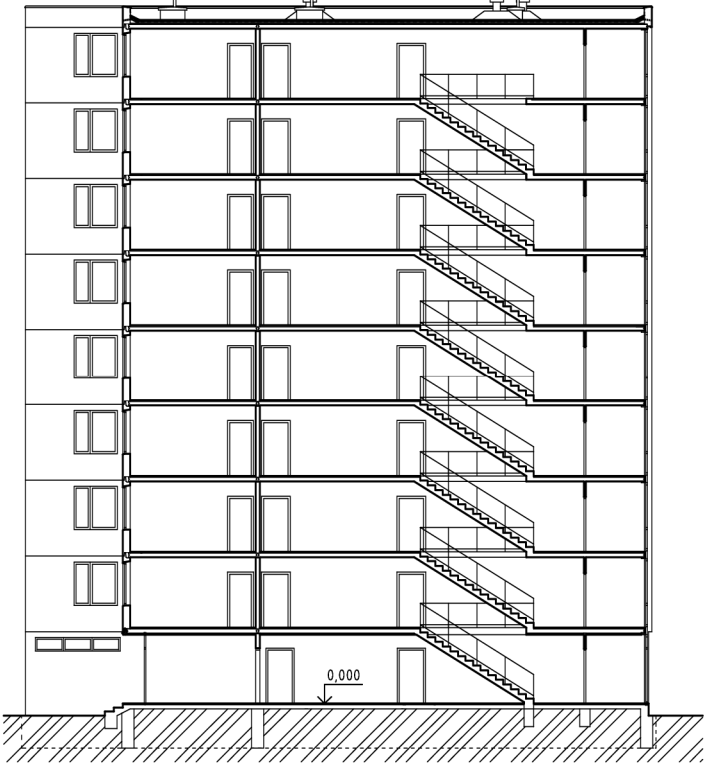
DETAIL 03
Floor plan 
Section A-A 

Table 4.3.2 – Structural composition of detail 03

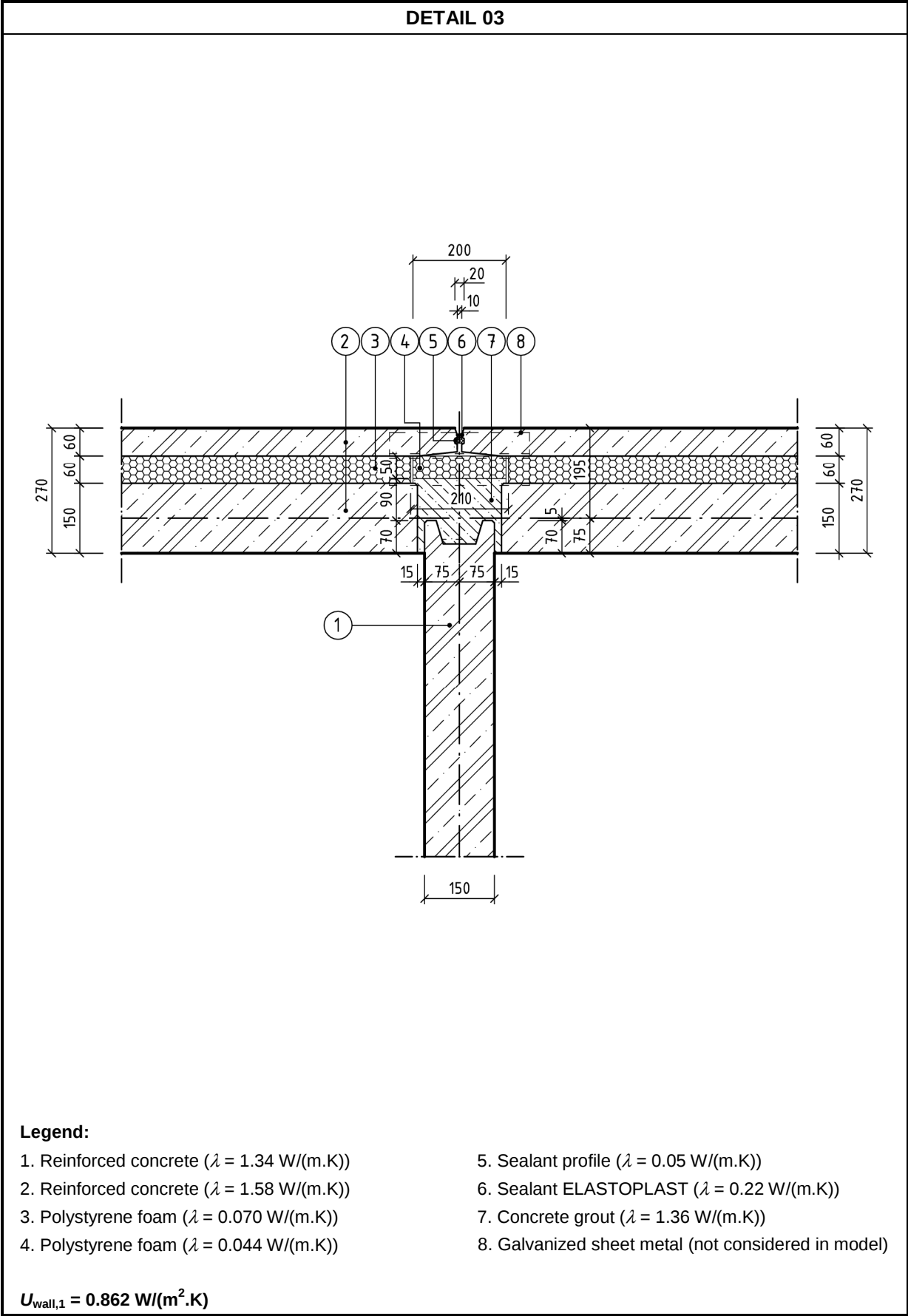


Table 4.3.3 – Boundary conditions for a calculation of detail 03

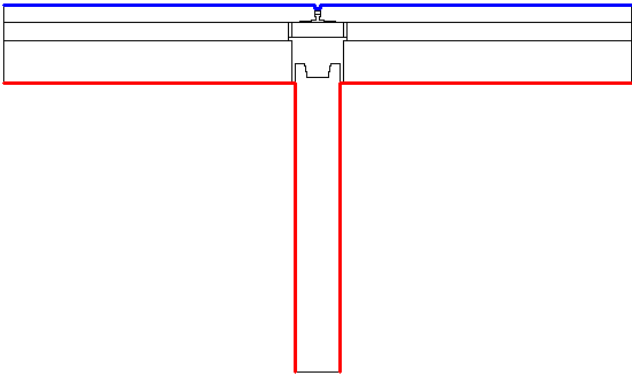
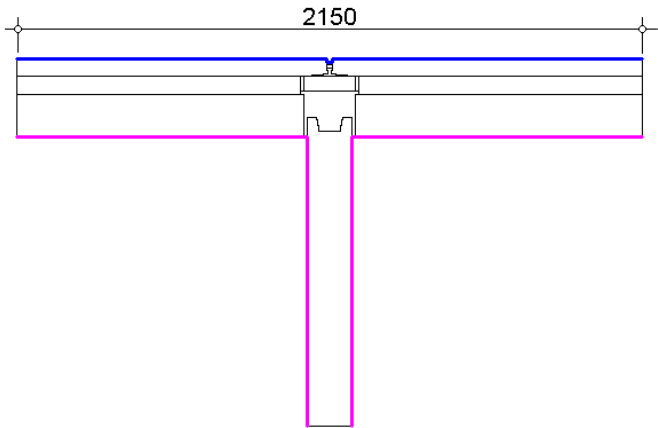
DETAIL 03	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.3.4 – Thermal-technical evaluation of detail 03

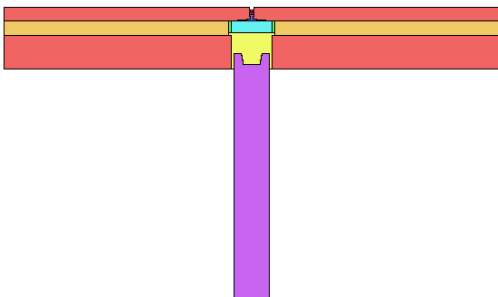
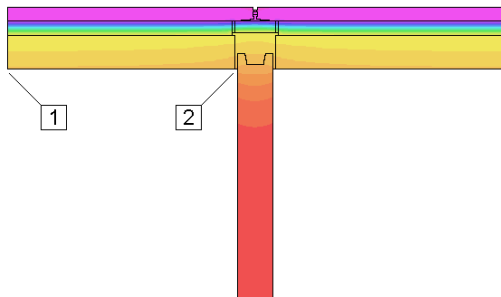
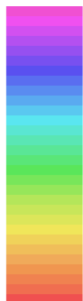
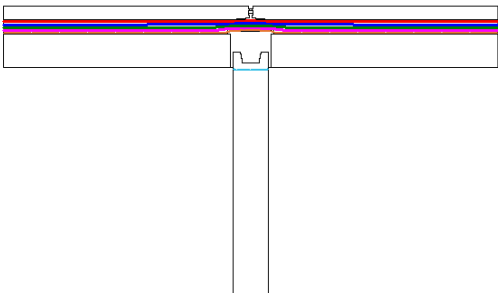
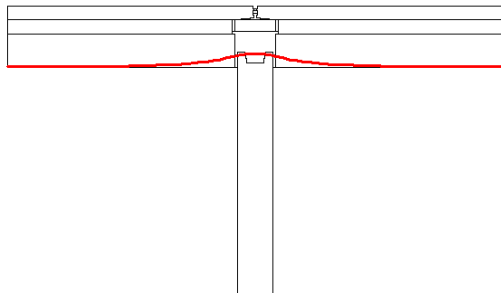
DETAIL 03																																		
Modeled detail with marking the materials			Temperature field with marked critical temperatures																															
																																		
Legend: $\lambda = 1.580 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ $\lambda = 1.360 \text{ W/(m.K)}$ $\lambda = 0.278 \text{ W/(m.K)}$ $\lambda = 0.044 \text{ W/(m.K)}$ $\lambda = 0.119 \text{ W/(m.K)}$ $\lambda = 1.340 \text{ W/(m.K)}$ $\lambda = 0.050 \text{ W/(m.K)}$ $\lambda = 0.220 \text{ W/(m.K)}$			 <table><tr><td>-15.0 °C</td><td>...</td><td>-11.5 °C</td></tr><tr><td>-11.5 °C</td><td>...</td><td>-8.0 °C</td></tr><tr><td>-8.0 °C</td><td>...</td><td>-4.5 °C</td></tr><tr><td>-4.5 °C</td><td>...</td><td>-1.0 °C</td></tr><tr><td>-1.0 °C</td><td>...</td><td>2.5 °C</td></tr><tr><td>2.5 °C</td><td>...</td><td>6.0 °C</td></tr><tr><td>6.0 °C</td><td>...</td><td>9.5 °C</td></tr><tr><td>9.5 °C</td><td>...</td><td>13.0 °C</td></tr><tr><td>13.0 °C</td><td>...</td><td>16.5 °C</td></tr><tr><td>16.5 °C</td><td>...</td><td>20.0 °C</td></tr></table>		-15.0 °C	...	-11.5 °C	-11.5 °C	...	-8.0 °C	-8.0 °C	...	-4.5 °C	-4.5 °C	...	-1.0 °C	-1.0 °C	...	2.5 °C	2.5 °C	...	6.0 °C	6.0 °C	...	9.5 °C	9.5 °C	...	13.0 °C	13.0 °C	...	16.5 °C	16.5 °C	...	20.0 °C
-15.0 °C	...	-11.5 °C																																
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16.5 °C	...	20.0 °C																																
Representation of characteristic isotherms			Representation of the critical isotherm																															
																																		
<table><tr><td> -10 °C</td><td> 5 °C</td></tr><tr><td> -5 °C</td><td> 10 °C</td></tr><tr><td> 0 °C</td><td> 15 °C</td></tr></table>			 -10 °C	 5 °C	 -5 °C	 10 °C	 0 °C	 15 °C	 13.12 °C																									
 -10 °C	 5 °C																																	
 -5 °C	 10 °C																																	
 0 °C	 15 °C																																	
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																														
1	$\theta_{Si} = 13.18 \text{ °C}$	$f_{Rsi} = 0.805$	$\theta_{Si} = 13.18 \text{ °C} > \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	meet																														
2	$\theta_{Si} = 14.17 \text{ °C}$	$f_{Rsi} = 0.833$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																															
Linear thermal transmittance			$\psi = 1.87294 - 0.862 \times 2.150 = 0.020 \text{ W/(m.K)}$																															

Table 4.4.1 – Marking of the position of detail in the building – detail 04

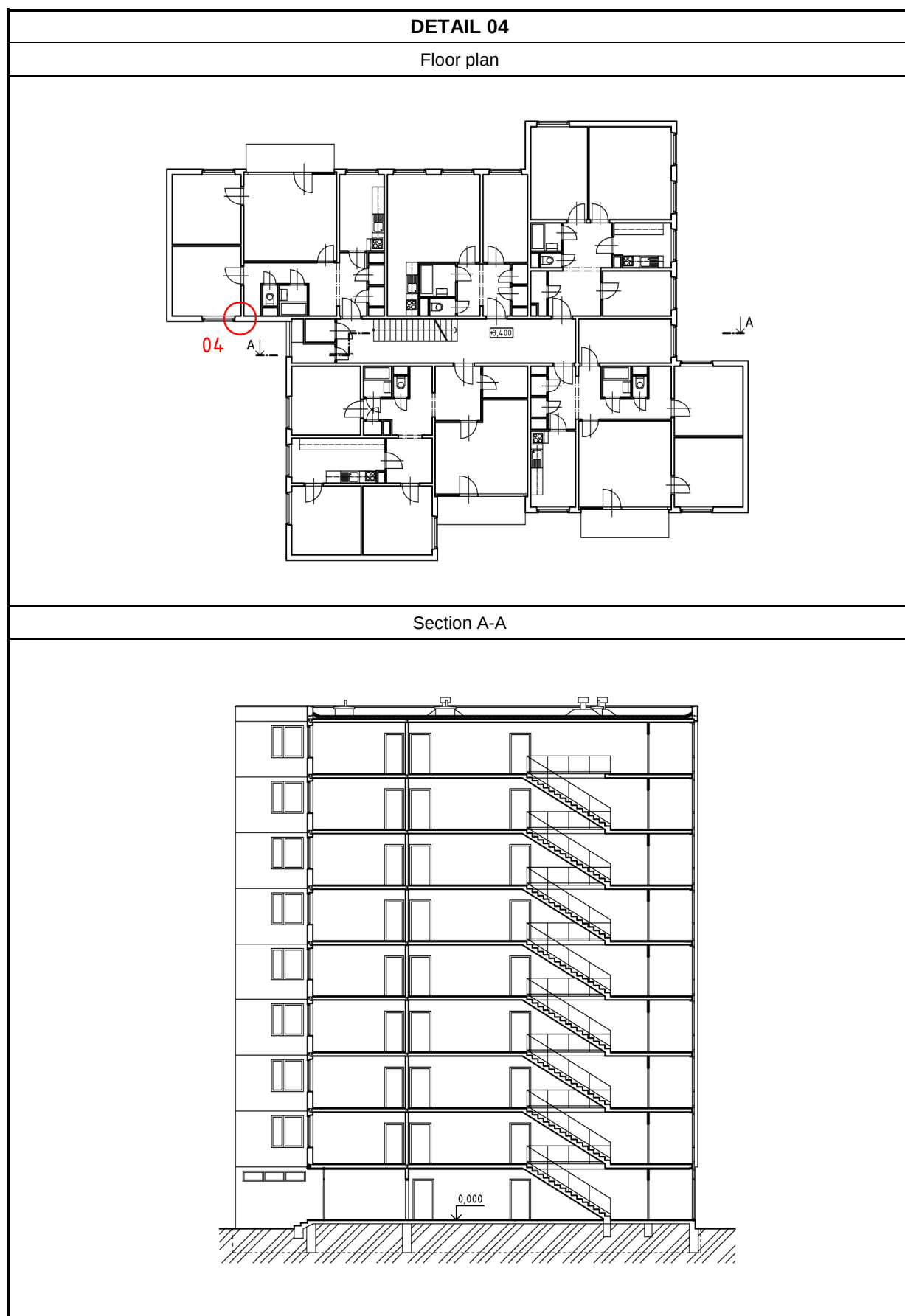


Table 4.4.2 – Structural composition of detail 04

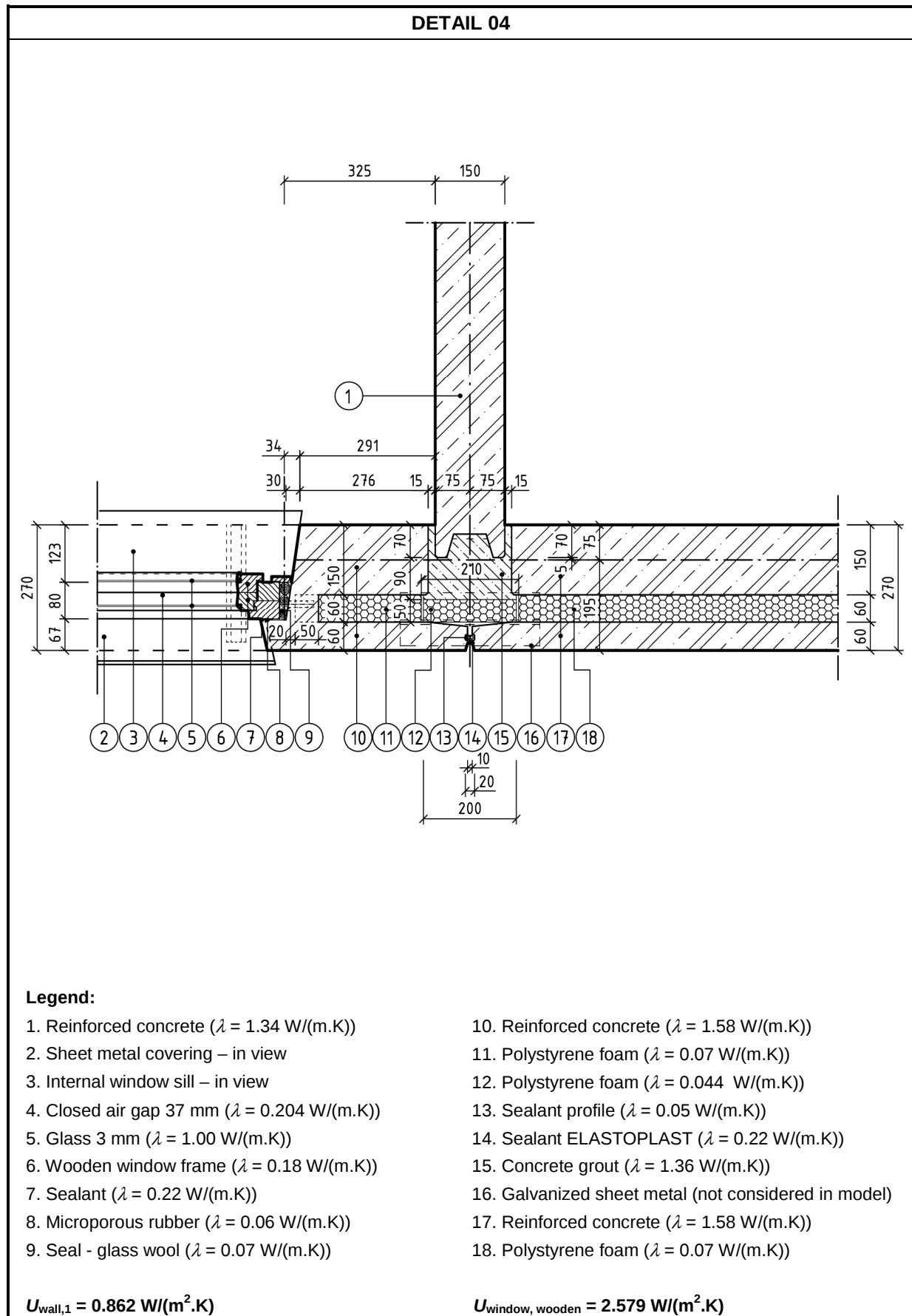


Table 4.4.3 – Boundary conditions for a calculation of detail 04

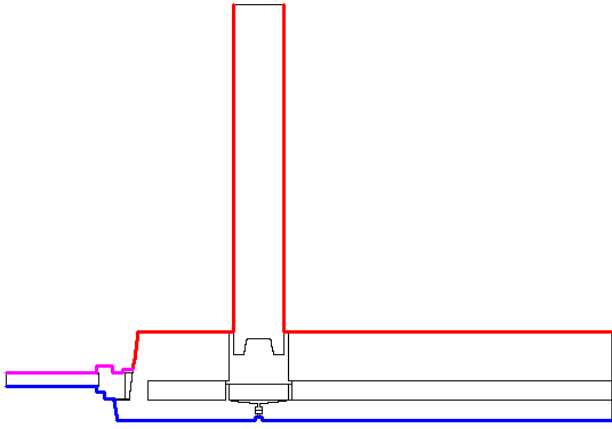
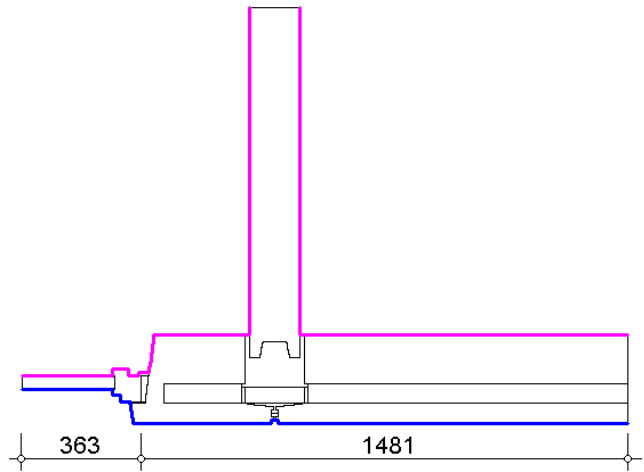
DETAIL 04	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$

Table 4.4.4 Thermal-technical evaluation of detail 04

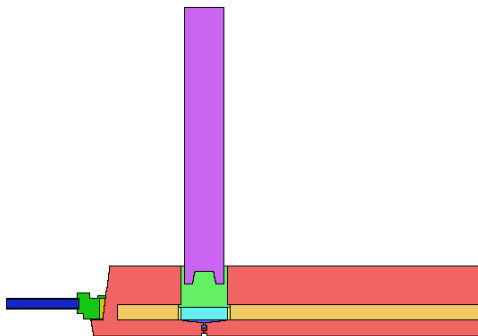
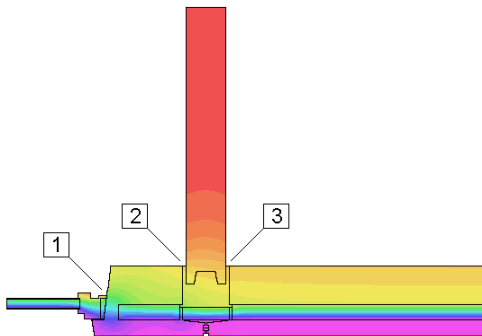
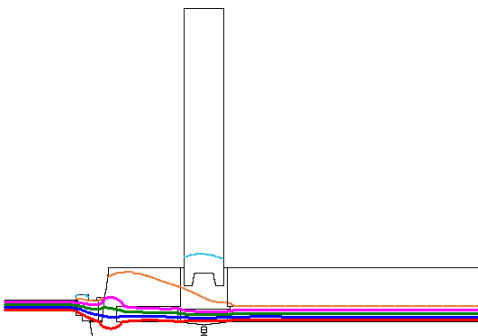
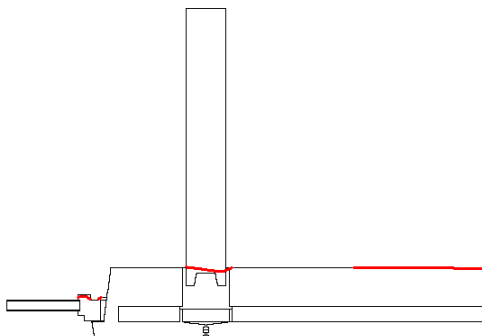
DETAIL 04																																																				
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																																	
																																																				
Legend: <table><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.278 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.044 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.119 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.278 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 0.119 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$																																																	
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	$\lambda = 0.278 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																																	
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	$\lambda = 0.119 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$																																																	
	$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$																																																	
-15.0 °C	... -11.5 °C																																																			
-11.5 °C	... -8.0 °C																																																			
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13.0 °C	... 16.5 °C																																																			
16.5 °C	... 20.0 °C																																																			
Representation of characteristic isotherms			Representation of the critical isotherm																																																	
																																																				
<table><tr><td></td><td>-10 °C</td><td></td><td>5 °C</td></tr><tr><td></td><td>-5 °C</td><td></td><td>10 °C</td></tr><tr><td></td><td>0 °C</td><td></td><td>15 °C</td></tr></table>				-10 °C		5 °C		-5 °C		10 °C		0 °C		15 °C	13.12 °C																																					
	-10 °C		5 °C																																																	
	-5 °C		10 °C																																																	
	0 °C		15 °C																																																	
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																																
1	$\theta_{Si} = 5.62 \text{ °C}$	$f_{Rsi} = 0.589$	$\theta_{Si} = 5.62 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																																
2	$\theta_{Si} = 12.92 \text{ °C}$	$f_{Rsi} = 0.780$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																																	
3	$\theta_{Si} = 13.58 \text{ °C}$	$f_{Rsi} = 0.817$																																																		
Linear thermal transmittance			$\psi = 2.57189 - 0.862 \times 1.481 - 2.579 \times 0.363 = 0.359 \text{ W/(m.K)}$																																																	

Table 4.5.1 – Marking of the position of detail in the building – detail 05

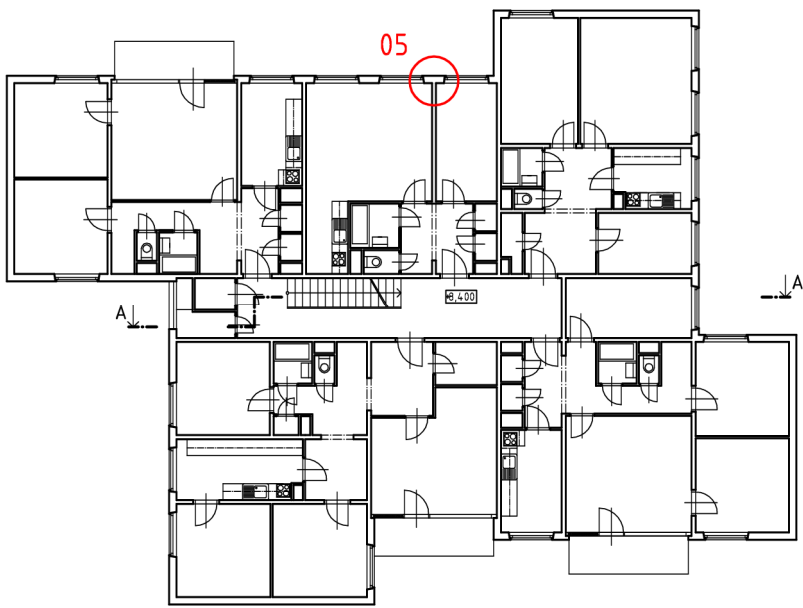
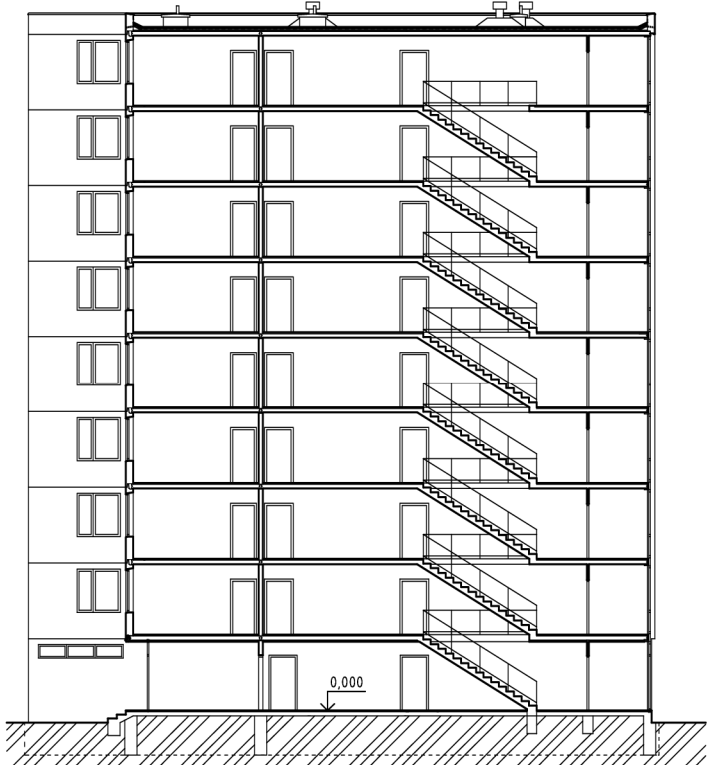
DETAIL 05
Floor plan 
Section A-A 

Table 4.5.2 – Structural composition of detail 05

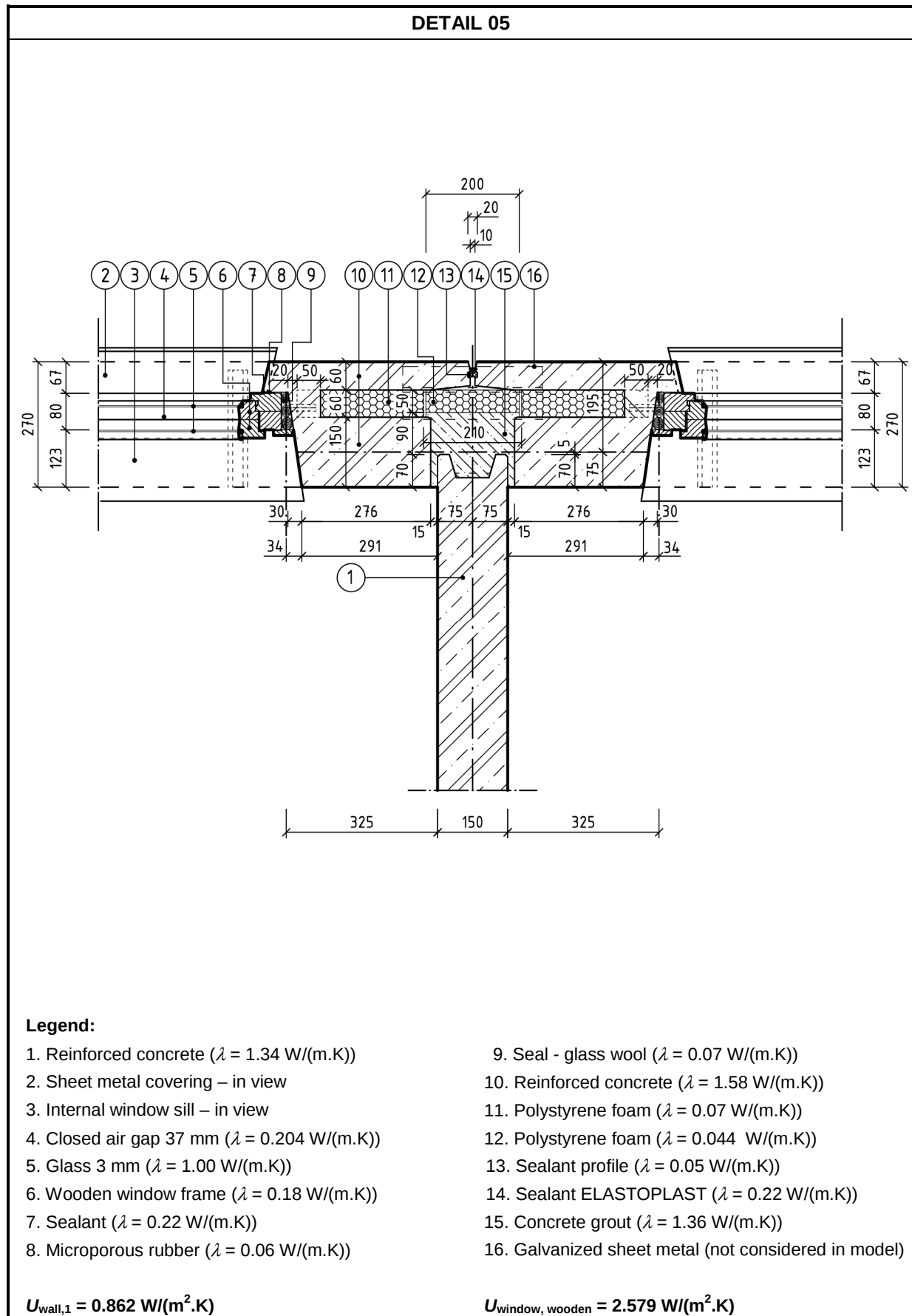


Table 4.5.3 – Boundary conditions for a calculation of detail 05

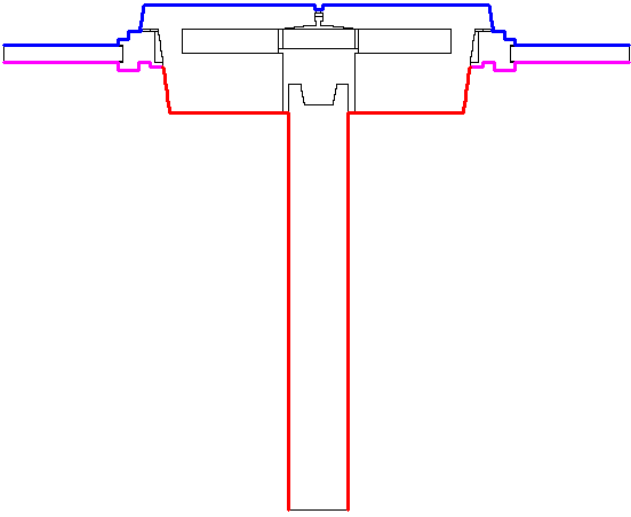
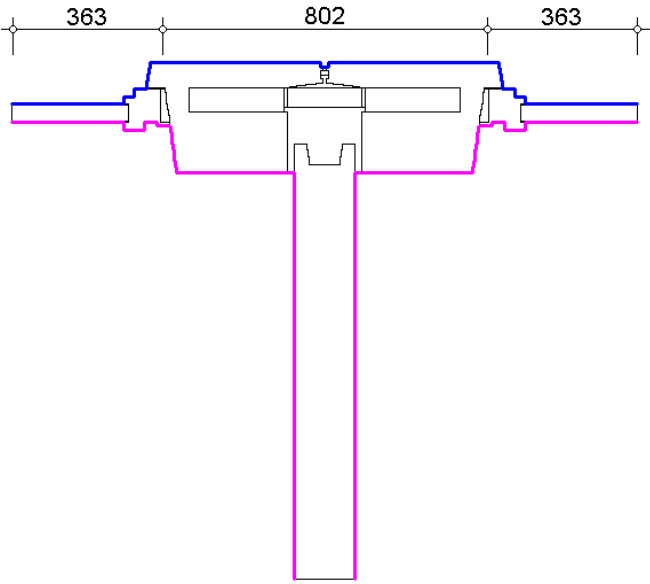
DETAIL 05	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.5.4 – Thermal-technical evaluation of detail 05

DETAIL 05																																																				
Modeled detail with marking the materials		Temperature field with marked critical temperatures																																																		
Legend: <table><tr><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.278 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.119 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td></tr></table>			$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.278 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.119 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$	<table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>			-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																																	
	$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$																																																	
	$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.278 \text{ W/(m.K)}$																																																	
	$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$																																																	
	$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.119 \text{ W/(m.K)}$																																																	
	$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$																																																	
	$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$																																																	
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16.5 °C	... 20.0 °C																																																			
Representation of characteristic isotherms		Representation of the critical isotherm																																																		
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	-10 °C		5 °C																																																	
	-5 °C		10 °C																																																	
	0 °C		15 °C																																																	
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																																
1	$\theta_{Si} = 5.72 \text{ °C}$	$f_{Rsi} = 0.592$	$\theta_{Si} = 5.72 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																																
2	$\theta_{Si} = 12.34 \text{ °C}$	$f_{Rsi} = 0.781$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																																	
Linear thermal transmittance		$\psi = 3.30469 - 0.862 \times 0.802 - 2.579 \times (0.363 + 0.363) = 0.741 \text{ W/(m.K)}$																																																		

Table 4.6.1 – Marking of the position of detail in the building – detail 06

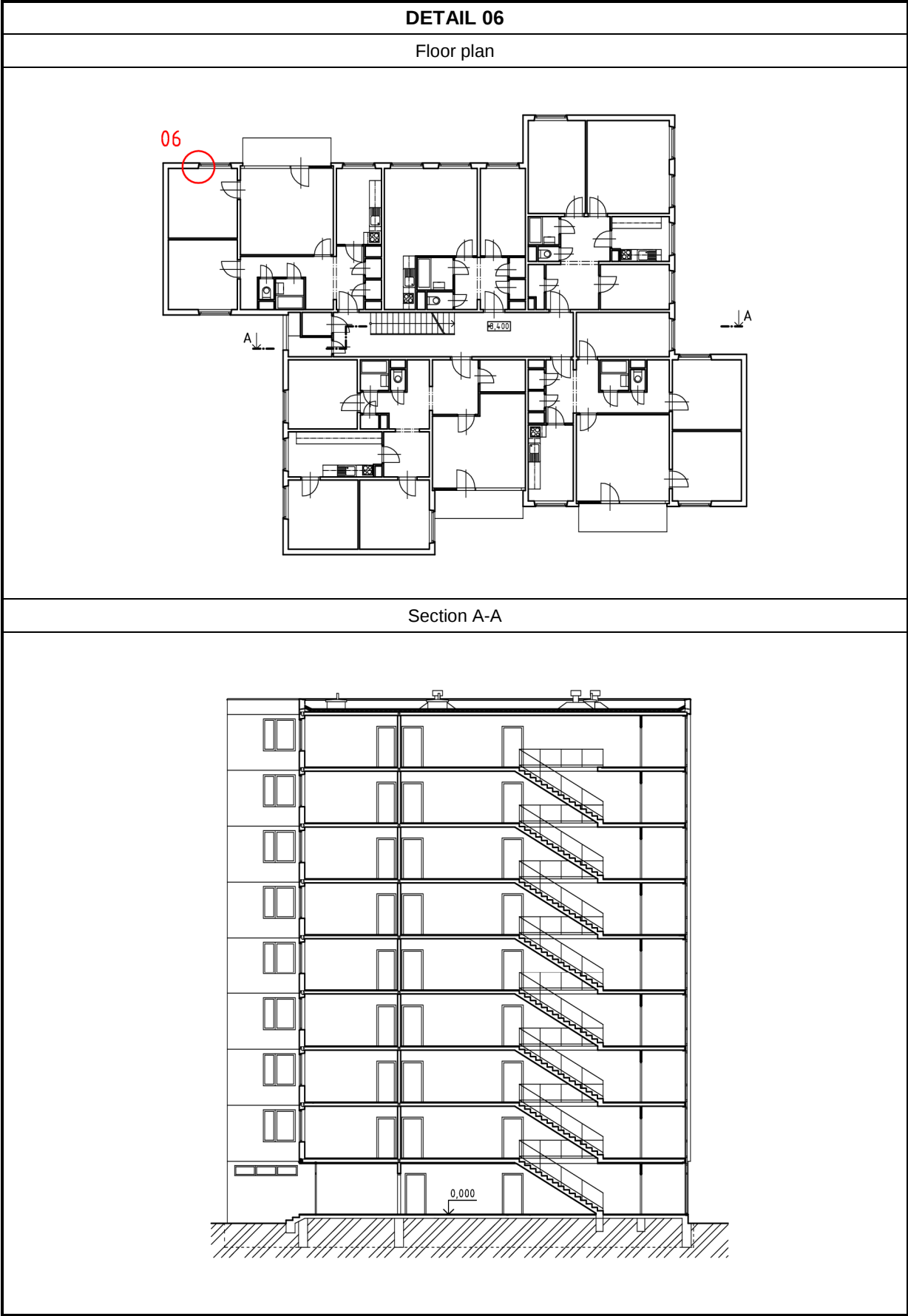


Table 4.6.2 – Structural composition of detail 06

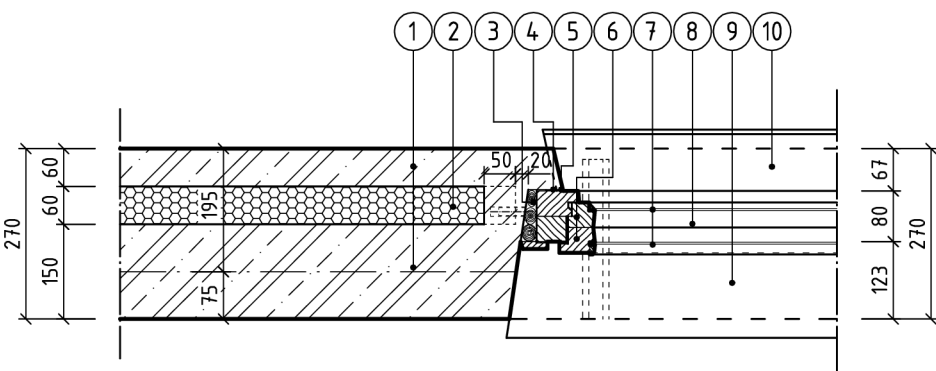
DETAIL 06											
											
Legend: <table><tbody><tr><td>1. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)</td><td>6. Wooden window frame ($\lambda = 0.18 \text{ W/(m.K)}$)</td></tr><tr><td>2. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)</td><td>7. Glass 3 mm ($\lambda = 1.00 \text{ W/(m.K)}$)</td></tr><tr><td>3. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)</td><td>8. Closed air gap 37 mm ($\lambda = 0.204 \text{ W/(m.K)}$)</td></tr><tr><td>4. Microporous rubber ($\lambda = 0.06 \text{ W/(m.K)}$)</td><td>9. Internal window sill – in view</td></tr><tr><td>5. Sealant ($\lambda = 0.22 \text{ W/(m.K)}$)</td><td>10. Sheet metal covering – in view</td></tr></tbody></table>		1. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)	6. Wooden window frame ($\lambda = 0.18 \text{ W/(m.K)}$)	2. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)	7. Glass 3 mm ($\lambda = 1.00 \text{ W/(m.K)}$)	3. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)	8. Closed air gap 37 mm ($\lambda = 0.204 \text{ W/(m.K)}$)	4. Microporous rubber ($\lambda = 0.06 \text{ W/(m.K)}$)	9. Internal window sill – in view	5. Sealant ($\lambda = 0.22 \text{ W/(m.K)}$)	10. Sheet metal covering – in view
1. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)	6. Wooden window frame ($\lambda = 0.18 \text{ W/(m.K)}$)										
2. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)	7. Glass 3 mm ($\lambda = 1.00 \text{ W/(m.K)}$)										
3. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)	8. Closed air gap 37 mm ($\lambda = 0.204 \text{ W/(m.K)}$)										
4. Microporous rubber ($\lambda = 0.06 \text{ W/(m.K)}$)	9. Internal window sill – in view										
5. Sealant ($\lambda = 0.22 \text{ W/(m.K)}$)	10. Sheet metal covering – in view										
$U_{\text{wall},1} = 0.862 \text{ W/(m}^2\text{.K)}$	$U_{\text{window, wooden}} = 2.579 \text{ W/(m}^2\text{.K)}$										

Table 4.6.3 – Boundary conditions for a calculation of detail 06

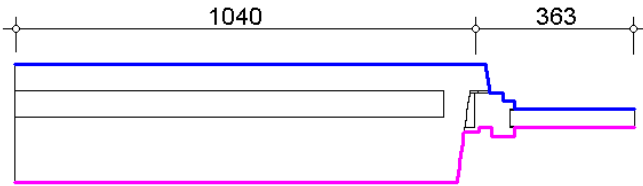
DETAIL 06	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.6.4 – Thermal-technical evaluation of detail 06

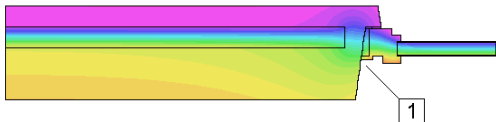
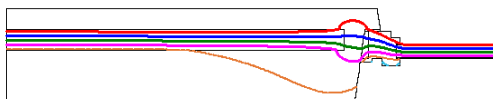
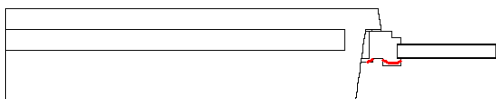
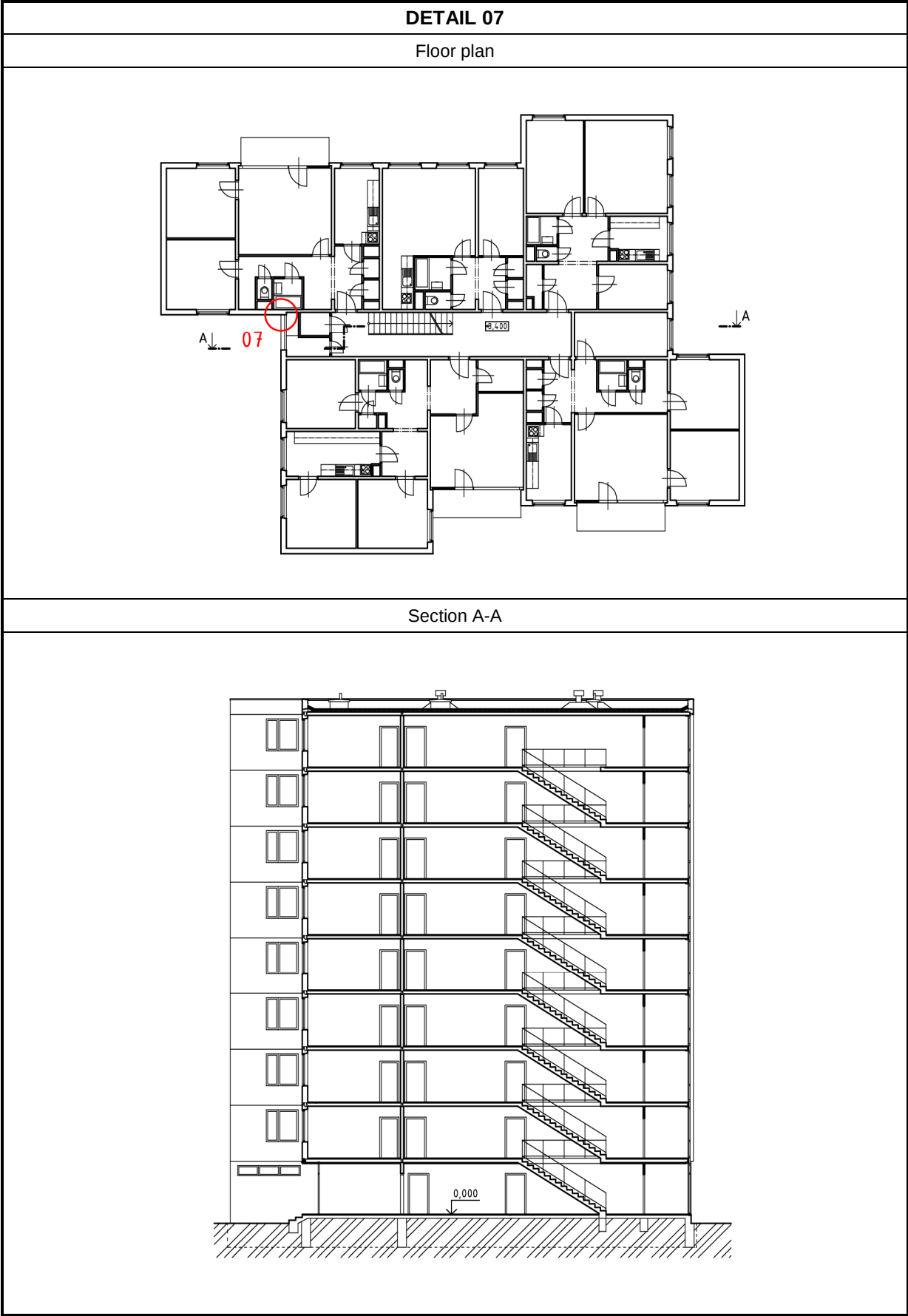
DETAIL 06																								
Modeled detail with marking the materials			Temperature field with marked critical temperatures																					
																								
Legend: $\lambda = 1.000 \text{ W/(m.K)}$ $\lambda = 0.204 \text{ W/(m.K)}$ $\lambda = 0.180 \text{ W/(m.K)}$ $\lambda = 1.580 \text{ W/(m.K)}$ $\lambda = 0.220 \text{ W/(m.K)}$ $\lambda = 0.060 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>			-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C		
-15.0 °C	... -11.5 °C																							
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16.5 °C	... 20.0 °C																							
Representation of characteristic isotherms			Representation of the critical isotherm																					
																								
-10 °C -5 °C 0 °C 5 °C 10 °C 15 °C 13.12 °C																								
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																				
1	$\theta_{si} = 5.75 \text{ °C}$	$f_{Rsi} = 0.593$	$\theta_{si} = 5.75 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet																				
			$\theta_{si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																					
Linear thermal transmittance			$\psi = 2.16905 - 0.862 \times 1.040 - 2.579 \times 0.363 = 0.336 \text{ W/(m.K)}$																					

Table 4.7.1 – Marking of the position of detail in the building – detail 07



DETAIL 07

Legend:

1. Glass 4 mm ($\lambda = 1.00 \text{ W/(m.K)}$)	5. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)
2. Steel window ($\lambda = 50 \text{ W/(m.K)}$ and $\lambda = 0.5 \text{ W/(m.K)}$)	6. Concrete grout ($\lambda = 1.36 \text{ W/(m.K)}$)
3. Seal - glass wool ($\lambda = 0.05 \text{ W/(m.K)}$)	7. Reinforced concrete ($\lambda = 1.34 \text{ W/(m.K)}$)
4. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)	

U_{wall,1} = 0.862 W/(m².K)

U_{window, steel} = 6.238 W/(m².K)

Table 4.7.3 – Boundary conditions for a calculation detail 07

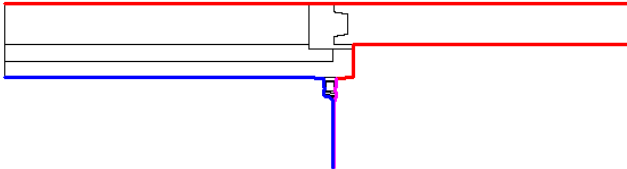
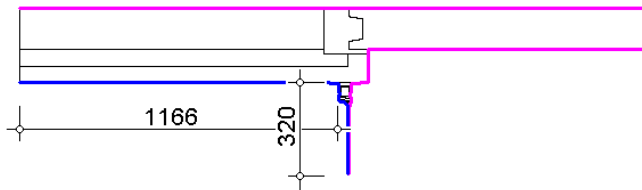
DETAIL 07	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.7.4 – Thermal-technical evaluation of detail 07

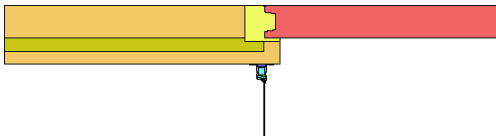
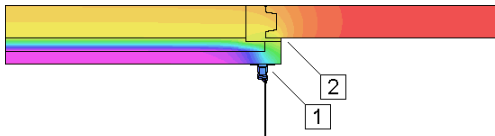
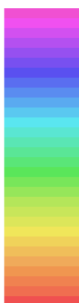
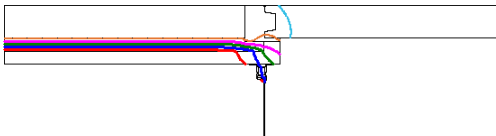
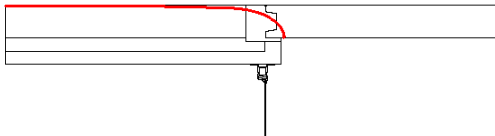
DETAIL 07																																		
Modeled detail with marking the materials			Temperature field with marked critical temperatures																															
																																		
Legend: <table><tr><td>■ $\lambda = 1.340 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.050 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 1.580 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.067 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 1.360 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.220 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 50.00 \text{ W/(m.K)}$</td><td>■ $\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 0.500 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.070 \text{ W/(m.K)}$</td></tr></table>			■ $\lambda = 1.340 \text{ W/(m.K)}$	■ $\lambda = 0.050 \text{ W/(m.K)}$	■ $\lambda = 1.580 \text{ W/(m.K)}$	■ $\lambda = 0.067 \text{ W/(m.K)}$	■ $\lambda = 1.360 \text{ W/(m.K)}$	■ $\lambda = 0.220 \text{ W/(m.K)}$	■ $\lambda = 50.00 \text{ W/(m.K)}$	■ $\lambda = 1.000 \text{ W/(m.K)}$	■ $\lambda = 0.500 \text{ W/(m.K)}$	■ $\lambda = 0.070 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
■ $\lambda = 1.340 \text{ W/(m.K)}$	■ $\lambda = 0.050 \text{ W/(m.K)}$																																	
■ $\lambda = 1.580 \text{ W/(m.K)}$	■ $\lambda = 0.067 \text{ W/(m.K)}$																																	
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■ $\lambda = 0.500 \text{ W/(m.K)}$	■ $\lambda = 0.070 \text{ W/(m.K)}$																																	
-15.0 °C	... -11.5 °C																																	
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Representation of characteristic isotherms			Representation of the critical isotherm																															
																																		
<table><tr><td>— -10 °C</td><td>— 5 °C</td></tr><tr><td>— -5 °C</td><td>— 10 °C</td></tr><tr><td>— 0 °C</td><td>— 15 °C</td></tr></table>			— -10 °C	— 5 °C	— -5 °C	— 10 °C	— 0 °C	— 15 °C	<table><tr><td>— 13.12 °C</td></tr></table>		— 13.12 °C																							
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— -5 °C	— 10 °C																																	
— 0 °C	— 15 °C																																	
— 13.12 °C																																		
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																														
1	$\theta_{Si} = -2.53 \text{ °C}$	$f_{Rsi} = 0.356$	$\theta_{Si} = -2.53 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																														
2	$\theta_{Si} = 11.42 \text{ °C}$	$f_{Rsi} = 0.755$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																															
Linear thermal transmittance			$\psi = 3.69604 - 0.862 \times 1.166 - 6.238 \times 0.320 = 0.695 \text{ W/(m.K)}$																															

Table 4.8.1 – Marking of the position of detail in the building – detail 08

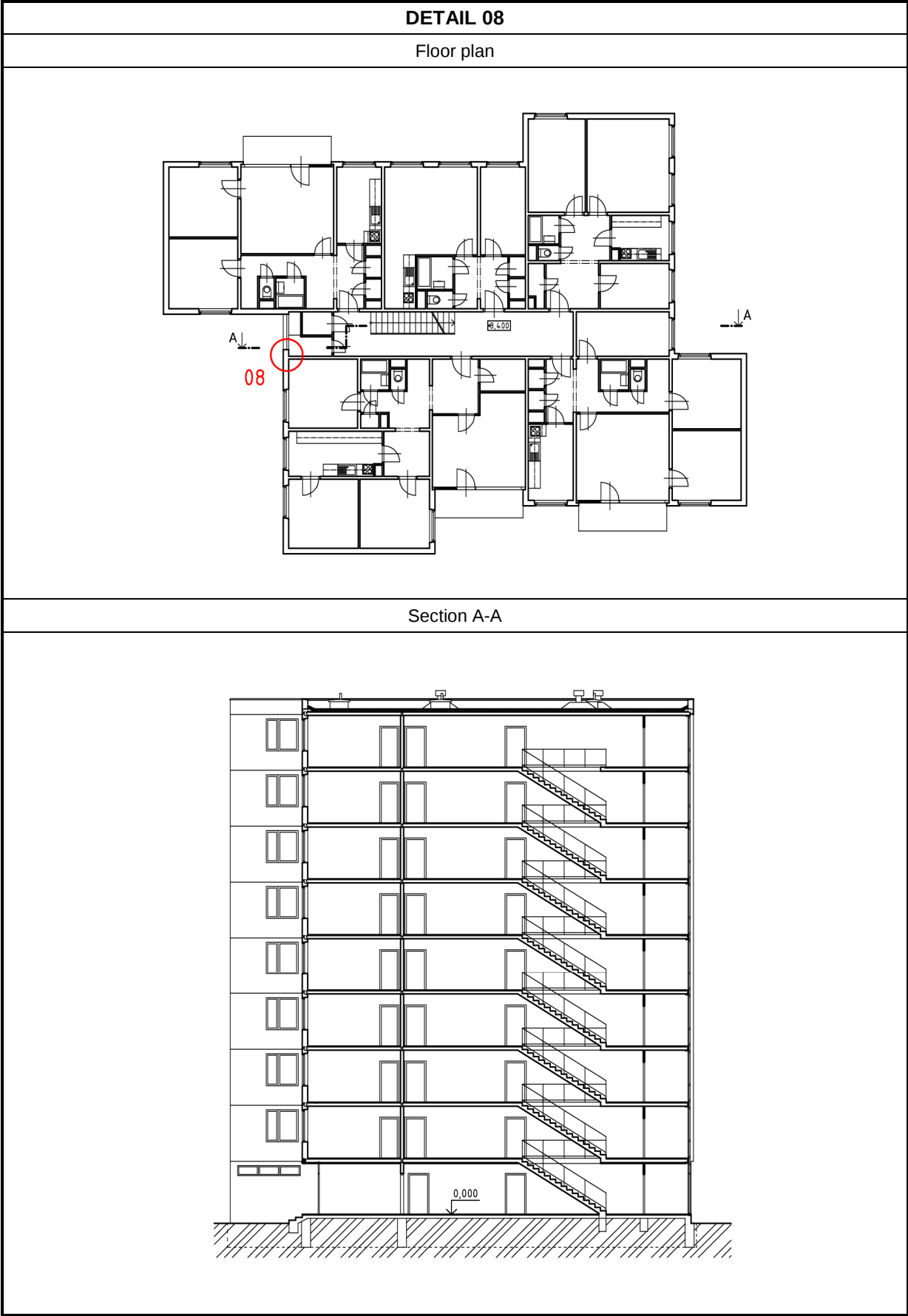


Table 4.8.2 – Structural composition of detail 08

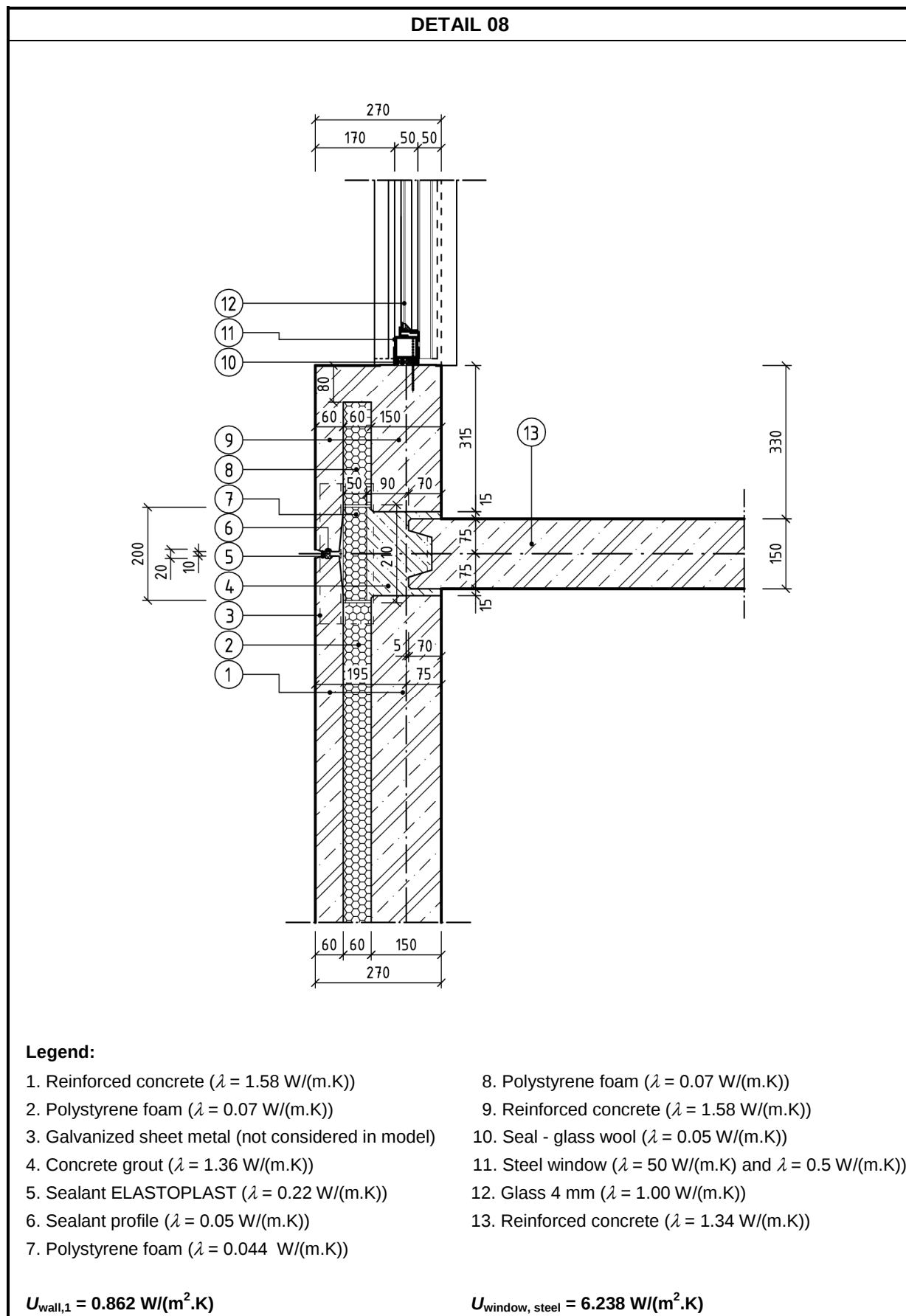


Table 4.8.3 – Boundary conditions for a calculation detail 08

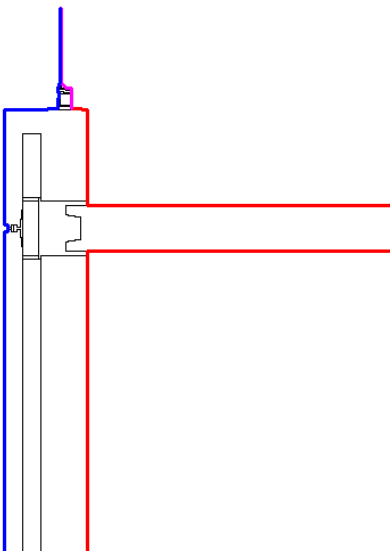
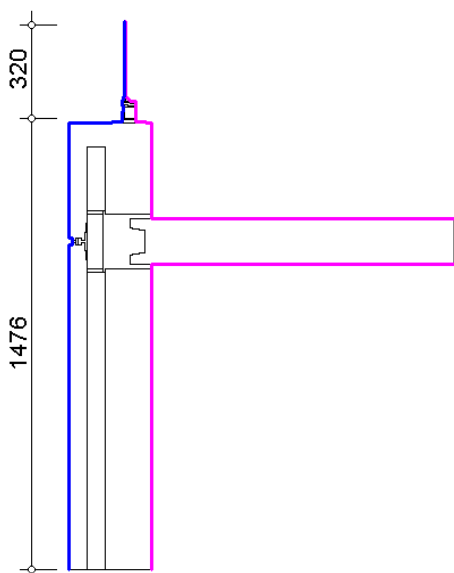
DETAIL 08	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.8.4 – Thermal-technical evaluation of detail 08

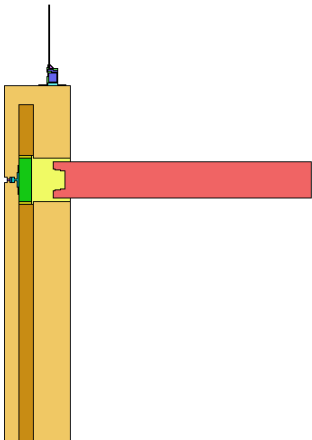
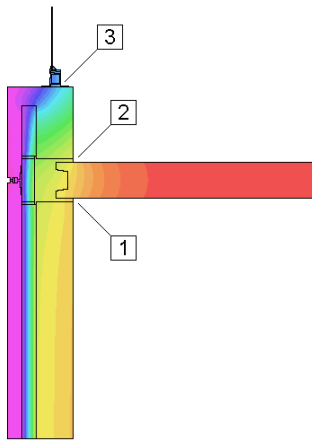
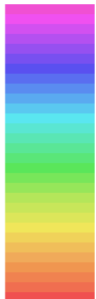
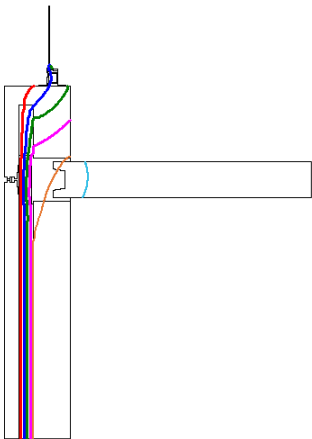
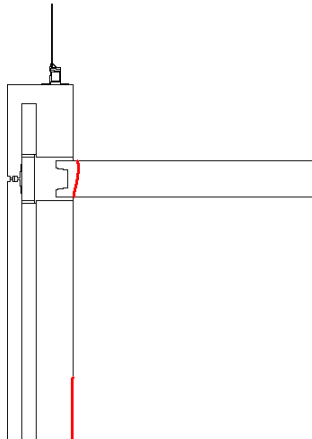
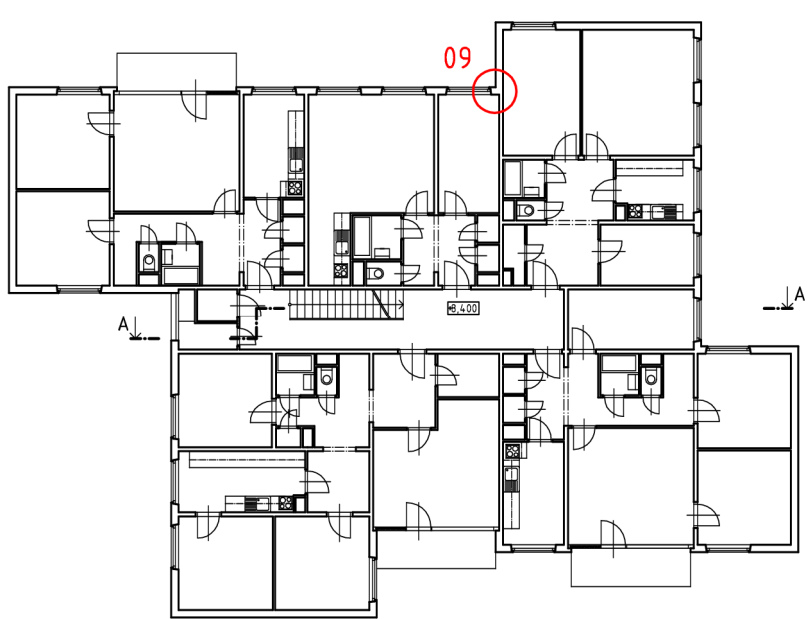
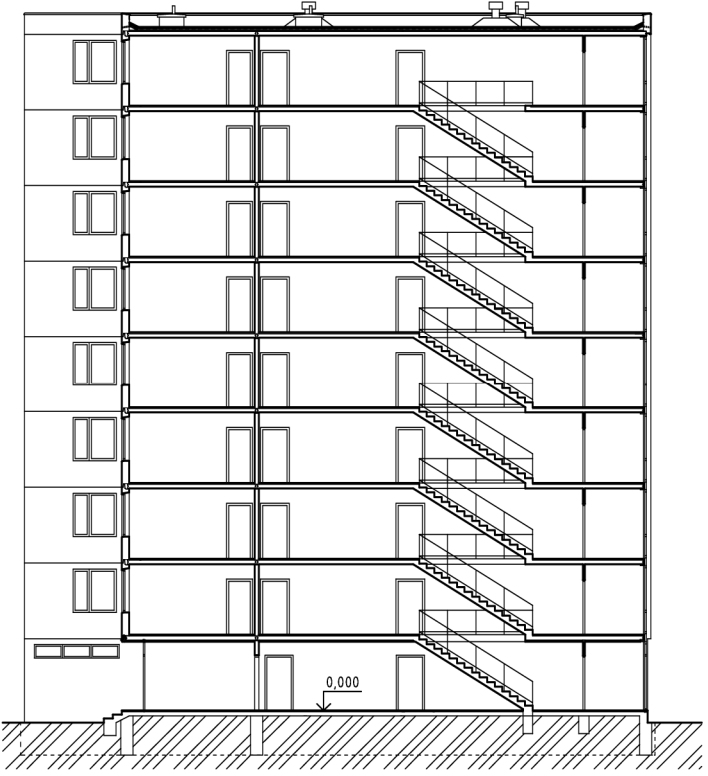
DETAIL 08																																						
Modeled detail with marking the materials		Temperature field with marked critical temperatures																																				
																																						
Legend: <table><tr><td> $\lambda = 1.340 \text{ W/(m.K)}$</td><td> $\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 1.580 \text{ W/(m.K)}$</td><td> $\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 1.360 \text{ W/(m.K)}$</td><td> $\lambda = 0.278 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 50.00 \text{ W/(m.K)}$</td><td> $\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.050 \text{ W/(m.K)}$</td><td> $\lambda = 0.119 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.500 \text{ W/(m.K)}$</td><td> $\lambda = 0.050 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.220 \text{ W/(m.K)}$</td><td></td></tr></table>		$\lambda = 1.340 \text{ W/(m.K)}$	$\lambda = 1.000 \text{ W/(m.K)}$	$\lambda = 1.580 \text{ W/(m.K)}$	$\lambda = 0.070 \text{ W/(m.K)}$	$\lambda = 1.360 \text{ W/(m.K)}$	$\lambda = 0.278 \text{ W/(m.K)}$	$\lambda = 50.00 \text{ W/(m.K)}$	$\lambda = 0.044 \text{ W/(m.K)}$	$\lambda = 0.050 \text{ W/(m.K)}$	$\lambda = 0.119 \text{ W/(m.K)}$	$\lambda = 0.500 \text{ W/(m.K)}$	$\lambda = 0.050 \text{ W/(m.K)}$	$\lambda = 0.220 \text{ W/(m.K)}$		 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>			-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
$\lambda = 1.340 \text{ W/(m.K)}$	$\lambda = 1.000 \text{ W/(m.K)}$																																					
$\lambda = 1.580 \text{ W/(m.K)}$	$\lambda = 0.070 \text{ W/(m.K)}$																																					
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Representation of characteristic isotherms		Representation of the critical isotherm																																				
																																						
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-10 °C	5 °C																																					
-5 °C	10 °C																																					
0 °C	15 °C																																					
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																		
1	$\theta_{Si} = 12.88 \text{ °C}$	$f_{Rsi} = 0.797$	$\theta_{Si} = -2.85 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																		
2	$\theta_{Si} = 11.43 \text{ °C}$	$f_{Rsi} = 0.755$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																			
3	$\theta_{Si} = -2.85 \text{ °C}$	$f_{Rsi} = 0.347$																																				
Linear thermal transmittance			$\psi = 4.07222 - 0.862 \times 1.476 - 6.238 \times 0.320 = 0.804 \text{ W/(m.K)}$																																			

Table 4.9.1 – Marking of the position of detail in the building – detail 09

DETAIL 09
Floor plan 
Section A-A 

DETAIL 09

The drawing shows a cross-section of a wall and window frame. The wall has a total width of 270 mm, with a central opening of 150 mm. The frame is 150 mm wide and 90 mm high. The wall is composed of reinforced concrete (1) and concrete grout (2). The frame is composed of reinforced concrete (6) and polystyrene foam (7). The sealant (5) is applied to the joint between the frame and the wall. The sealant profile (4) is shown in the joint. The dimensions are as follows: wall width 270 mm, frame width 150 mm, frame height 90 mm, wall opening 150 mm, frame opening 150 mm, wall thickness 195 mm, frame thickness 75 mm, sealant profile height 5 mm, sealant profile width 15 mm, sealant profile depth 75 mm, sealant profile width 75 mm, sealant profile depth 75 mm, sealant profile width 75 mm, sealant profile depth 75 mm. The legend is as follows:

Legend:	Material	Thermal Conductivity (λ)
1.	Reinforced concrete	$\lambda = 1.34 \text{ W/(m.K)}$
2.	Concrete grout	$\lambda = 1.36 \text{ W/(m.K)}$
3.	Filling - polystyrene foam	$\lambda = 0.050 \text{ W/(m.K)}$
4.	Sealant profile	$\lambda = 0.05 \text{ W/(m.K)}$
5.	Sealant ELASTOPLAST	$\lambda = 0.22 \text{ W/(m.K)}$
6.	Reinforced concrete	$\lambda = 1.58 \text{ W/(m.K)}$
7.	Polystyrene foam	$\lambda = 0.07 \text{ W/(m.K)}$

Legend:

1. Reinforced concrete ($\lambda = 1.34 \text{ W/(m.K)}$)	5. Sealant ELASTOPLAST ($\lambda = 0.22 \text{ W/(m.K)}$)
2. Concrete grout ($\lambda = 1.36 \text{ W/(m.K)}$)	6. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)
3. Filling - polystyrene foam ($\lambda = 0.050 \text{ W/(m.K)}$)	7. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)
4. Sealant profile ($\lambda = 0.05 \text{ W/(m.K)}$)	

$$U_{\text{wall},1} = 0.862 \text{ W/(m}^2\text{.K)}$$

Table 4.9.3 – Boundary conditions for a calculation of detail 09

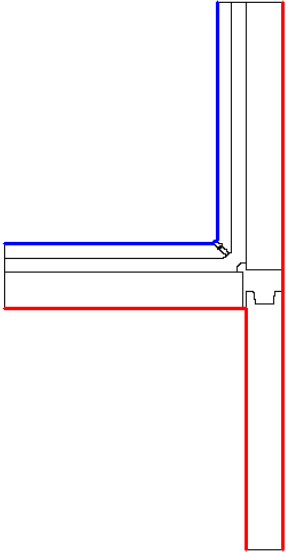
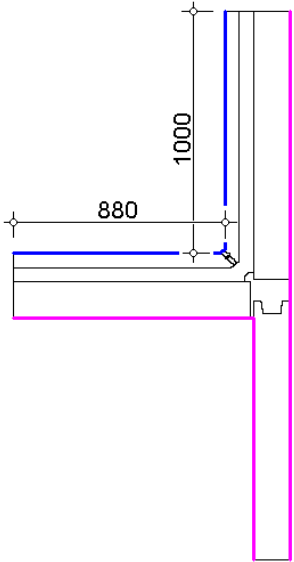
DETAIL 09	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ \%}$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ \%}$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ \%}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ \%}$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.9.4 – Thermal-technical evaluation of detail 09

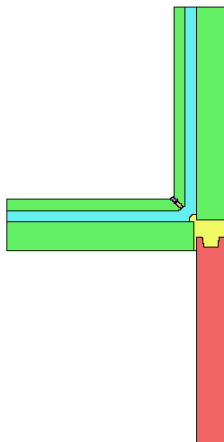
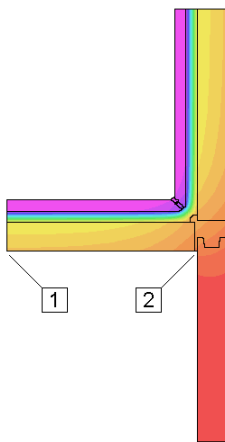
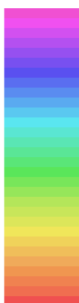
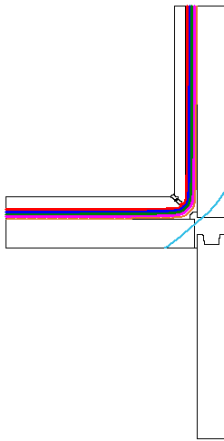
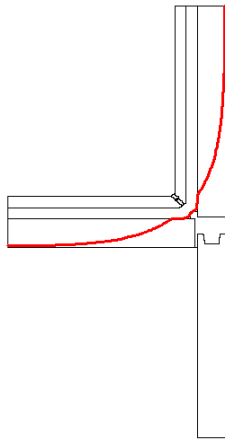
DETAIL 09																								
Modeled detail with marking the materials			Temperature field with marked critical temperatures																					
																								
Legend: ■ $\lambda = 1.340 \text{ W/(m.K)}$ ■ $\lambda = 0.067 \text{ W/(m.K)}$ ■ $\lambda = 1.360 \text{ W/(m.K)}$ ■ $\lambda = 1.580 \text{ W/(m.K)}$ ■ $\lambda = 0.070 \text{ W/(m.K)}$ ■ $\lambda = 0.050 \text{ W/(m.K)}$ ■ $\lambda = 0.220 \text{ W/(m.K)}$			 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
-15.0 °C	... -11.5 °C																							
-11.5 °C	... -8.0 °C																							
-8.0 °C	... -4.5 °C																							
-4.5 °C	... -1.0 °C																							
-1.0 °C	... 2.5 °C																							
2.5 °C	... 6.0 °C																							
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9.5 °C	... 13.0 °C																							
13.0 °C	... 16.5 °C																							
16.5 °C	... 20.0 °C																							
Representation of characteristic isotherms			Representation of the critical isotherm																					
																								
<table><tr><td>— -10 °C</td><td>— 5 °C</td></tr><tr><td>— -5 °C</td><td>— 10 °C</td></tr><tr><td>— 0 °C</td><td>— 15 °C</td></tr></table>			— -10 °C	— 5 °C	— -5 °C	— 10 °C	— 0 °C	— 15 °C	— 13.12 °C															
— -10 °C	— 5 °C																							
— -5 °C	— 10 °C																							
— 0 °C	— 15 °C																							
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																				
1	$\theta_{Si} = 13.22 \text{ °C}$	$f_{Rsi} = 0.806$	$\theta_{Si} = 13.22 \text{ °C} > \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	meet																				
2	$\theta_{Si} = 16.43 \text{ °C}$	$f_{Rsi} = 0.898$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																					
Linear thermal transmittance			$\psi = 1.74967 - 0.862 \times (1.000 + 0.880) = 0.129 \text{ W/(m.K)}$																					

Table 4.10.1 – Marking of the position of detail in the building – detail 10

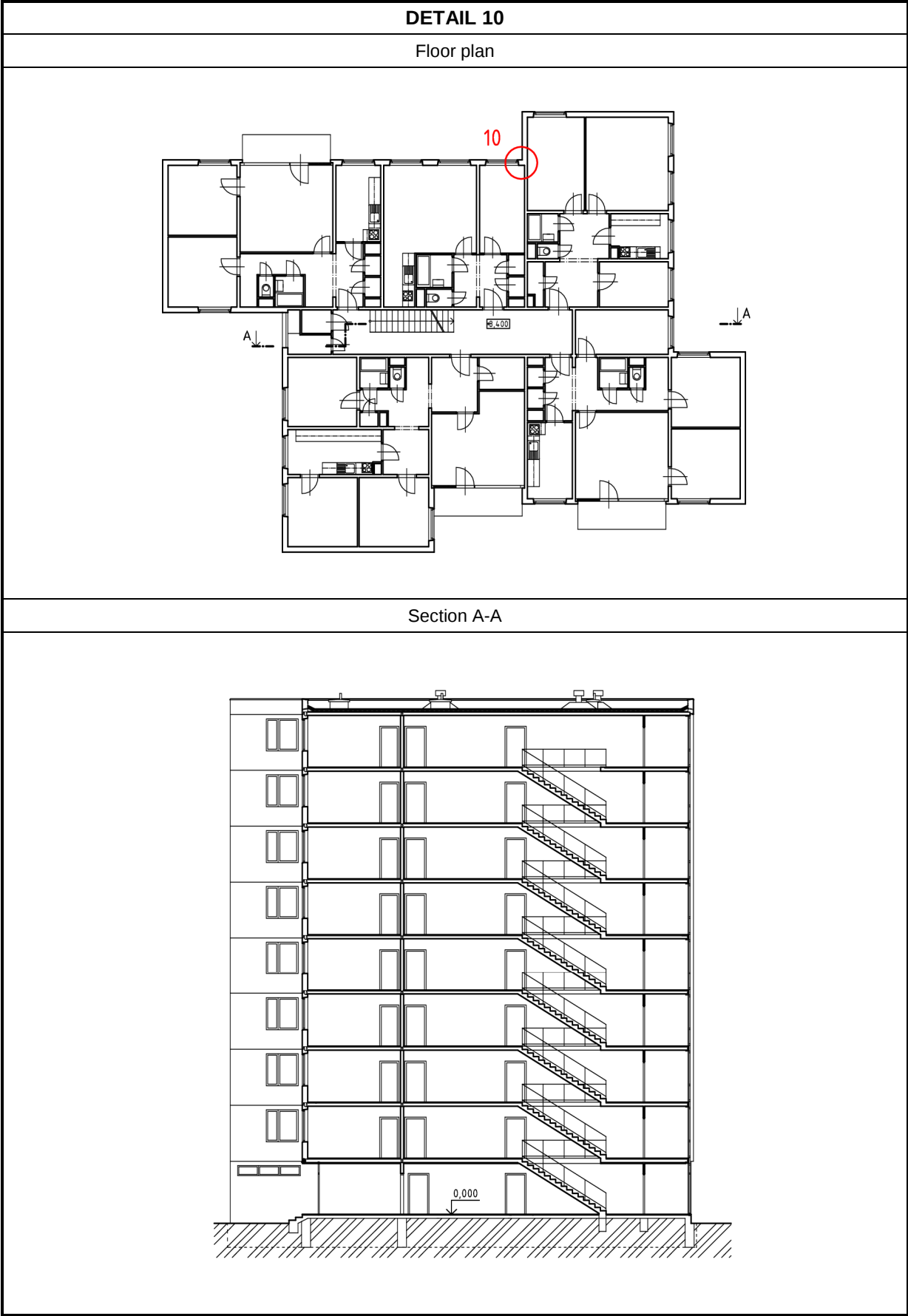


Table 4.10.2 – Structural composition of detail 10

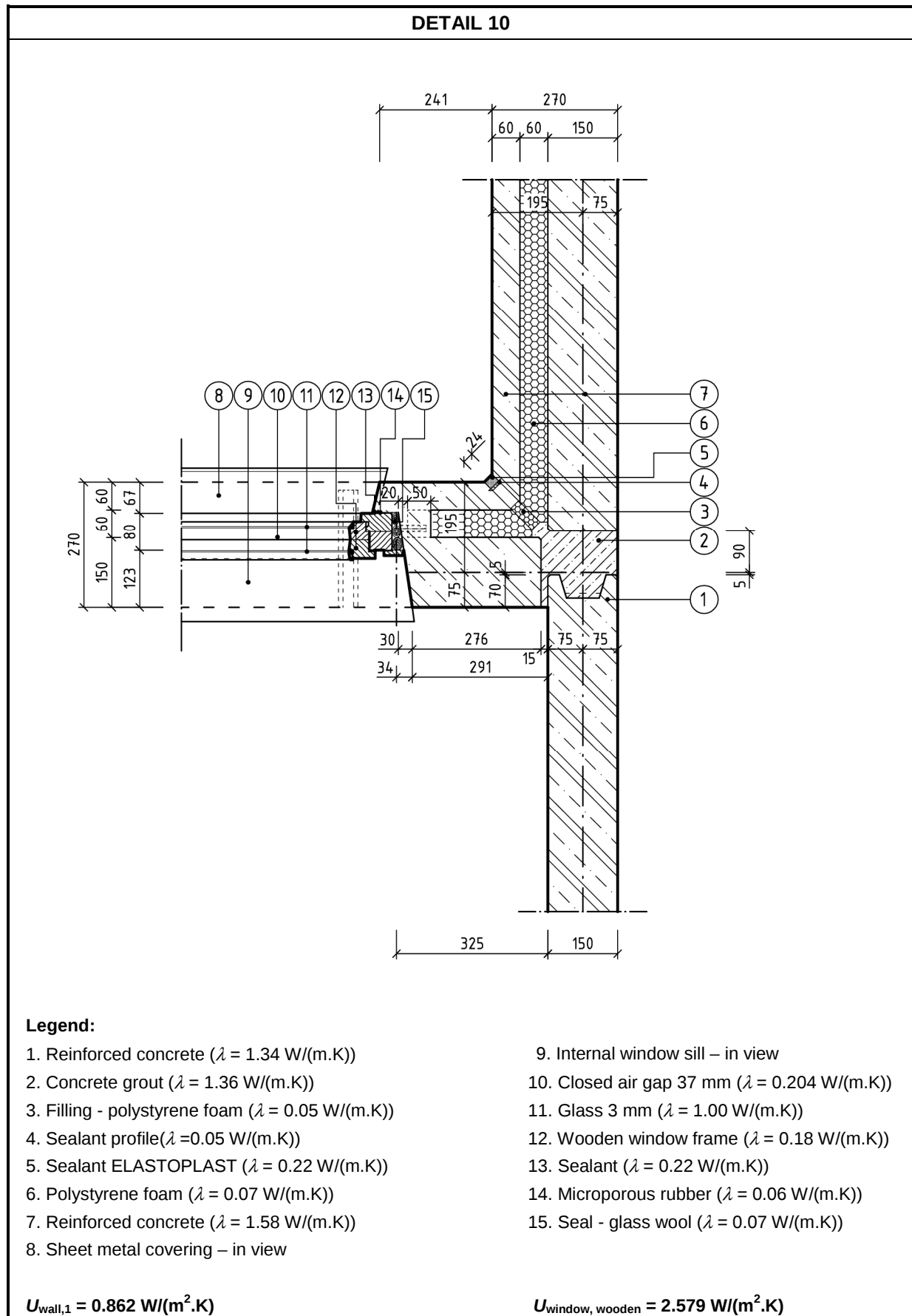


Table 4.10.3 – Boundary conditions for a calculation of detail 10

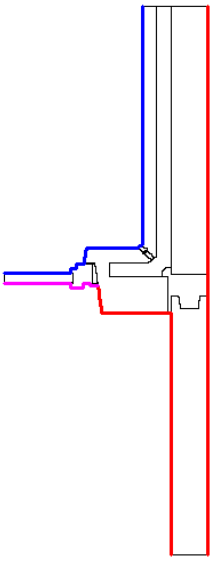
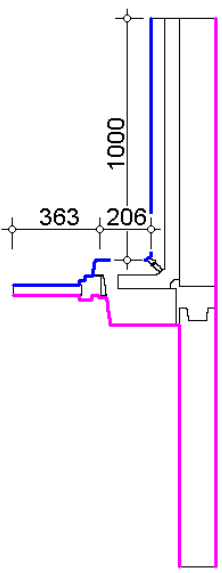
DETAIL 10	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.10.4 – Thermal-technical evaluation of detail 10

DETAIL 10																																																
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																													
Legend: <table><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.067 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.067 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$	<table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$																																													
	$\lambda = 0.067 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$																																													
	$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																													
	$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$																																													
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-15.0 °C	... -11.5 °C																																															
-11.5 °C	... -8.0 °C																																															
-8.0 °C	... -4.5 °C																																															
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2.5 °C	... 6.0 °C																																															
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9.5 °C	... 13.0 °C																																															
13.0 °C	... 16.5 °C																																															
16.5 °C	... 20.0 °C																																															
Representation of characteristic isotherms			Representation of the critical isotherm																																													
<table><tr><td></td><td>-10 °C</td><td></td><td>5 °C</td></tr><tr><td></td><td>-5 °C</td><td></td><td>10 °C</td></tr><tr><td></td><td>0 °C</td><td></td><td>15 °C</td></tr></table>				-10 °C		5 °C		-5 °C		10 °C		0 °C		15 °C	13.12 °C																																	
	-10 °C		5 °C																																													
	-5 °C		10 °C																																													
	0 °C		15 °C																																													
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																												
1	$\theta_{Si} = 6.84 \text{ °C}$	$f_{Rsi} = 0.624$	$\theta_{Si} = 6.84 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																												
2	$\theta_{Si} = 15.58 \text{ °C}$	$f_{Rsi} = 0.874$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																													
Linear thermal transmittance		$\psi = 2.45615 - 0.862 \times (1.000 + 0.206) - 2.579 \times 0.363 = 0.480 \text{ W/(m.K)}$																																														

Table 4.11.1 – Marking of the position of detail in the building – detail 11

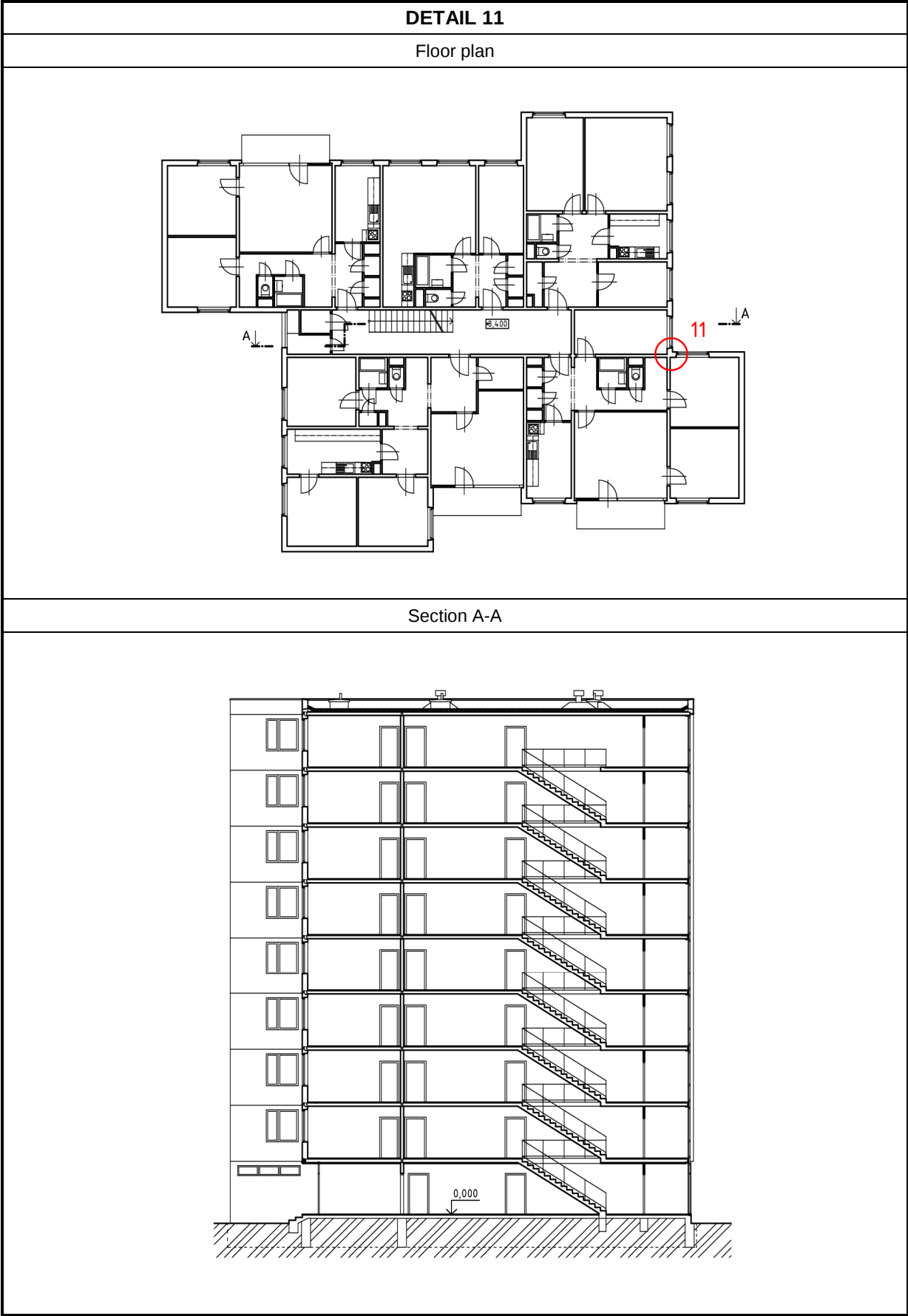


Table 4.11.2 – Structural composition of detail 11

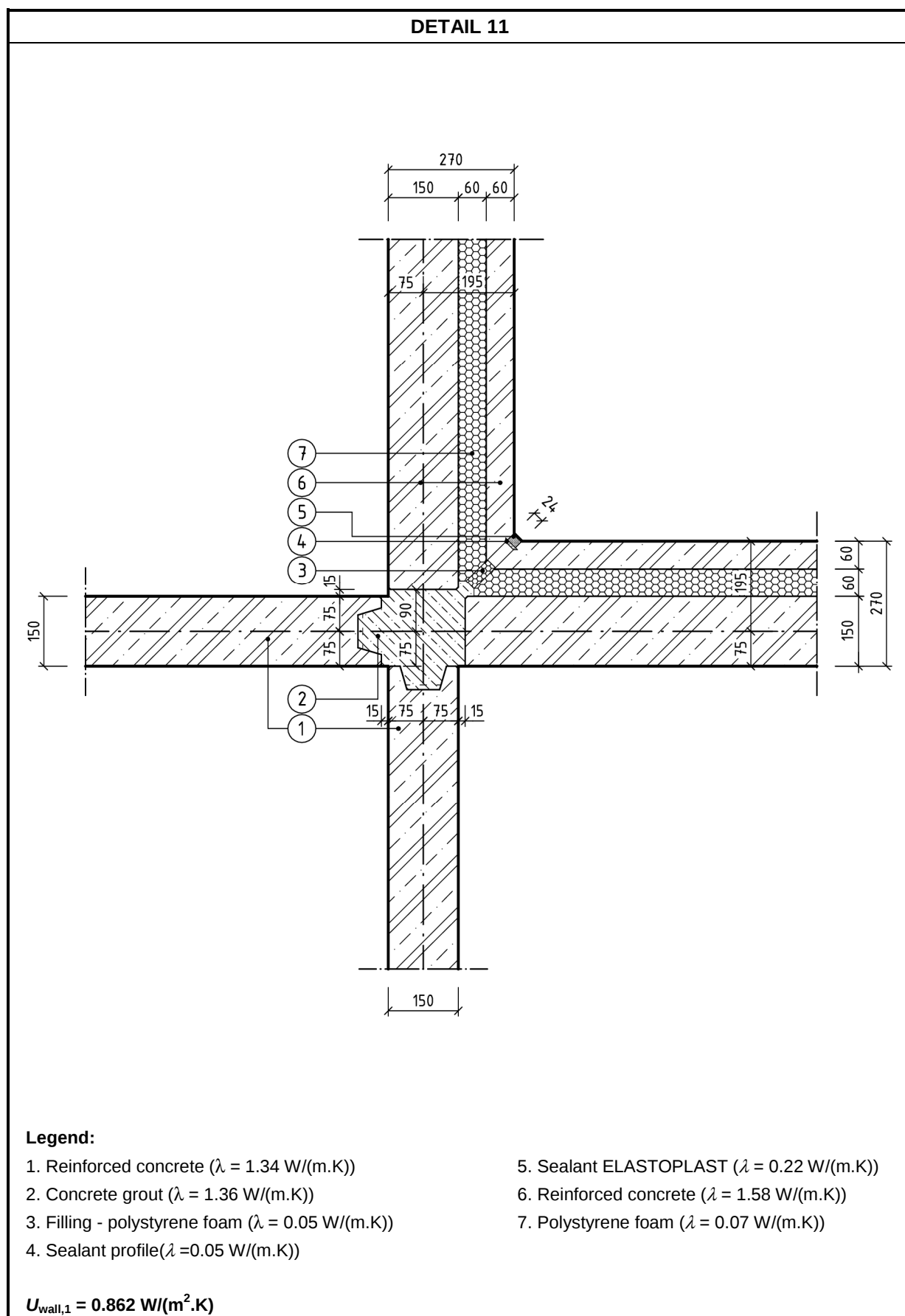


Table 4.11.3 – Boundary conditions for a calculation of detail 11

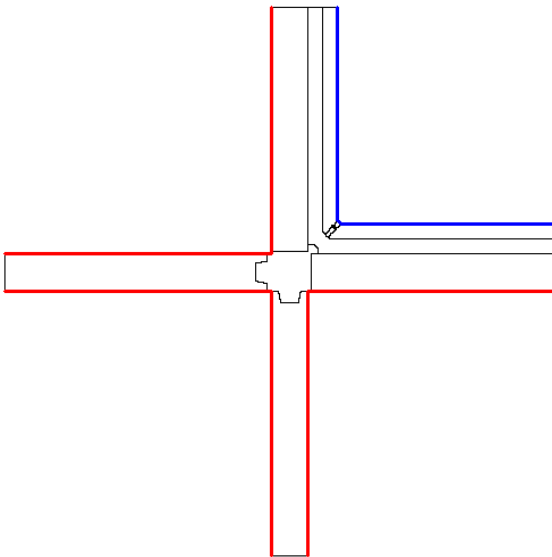
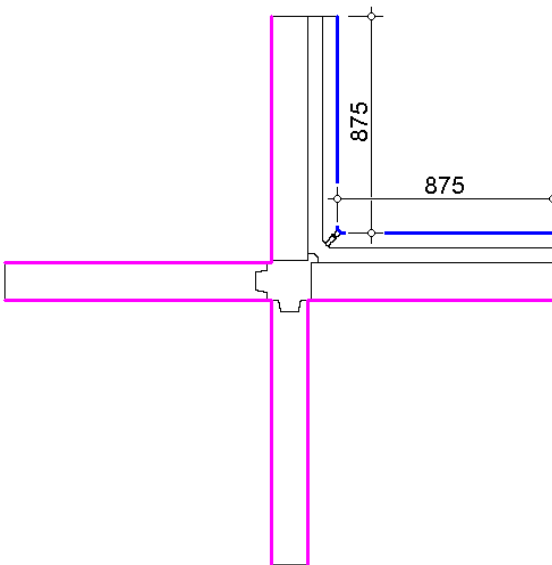
DETAIL 11	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ }\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ }\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\text{ }\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\text{ }\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.11.4 – Thermal-technical evaluation of detail 11

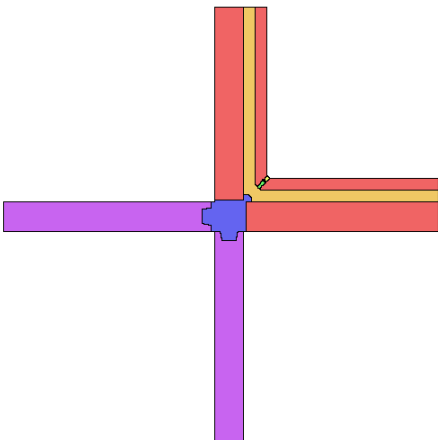
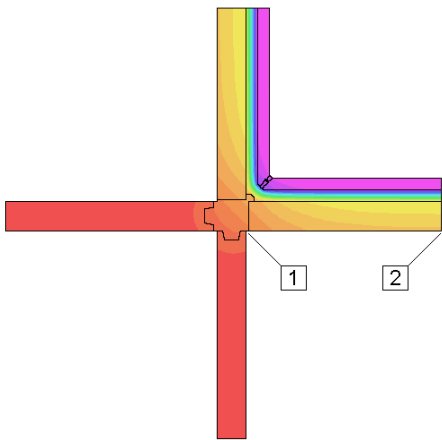
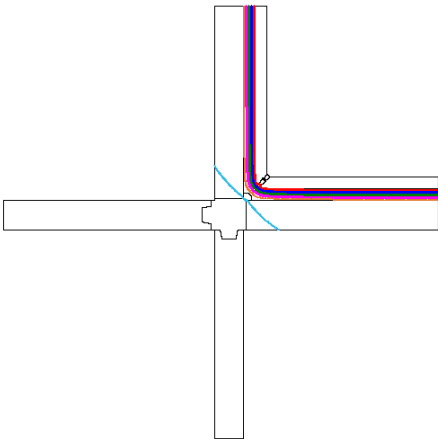
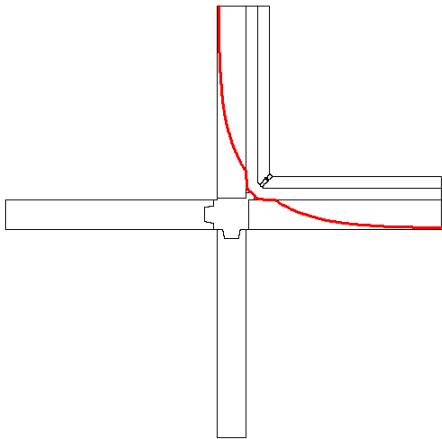
DETAIL 11																								
Modeled detail with marking the materials			Temperature field with marked critical temperatures																					
																								
Legend: ■ $\lambda = 1.580 \text{ W/(m.K)}$ ■ $\lambda = 0.070 \text{ W/(m.K)}$ ■ $\lambda = 0.220 \text{ W/(m.K)}$ ■ $\lambda = 0.067 \text{ W/(m.K)}$ ■ $\lambda = 0.050 \text{ W/(m.K)}$ ■ $\lambda = 1.360 \text{ W/(m.K)}$ ■ $\lambda = 1.340 \text{ W/(m.K)}$			 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
-15.0 °C	... -11.5 °C																							
-11.5 °C	... -8.0 °C																							
-8.0 °C	... -4.5 °C																							
-4.5 °C	... -1.0 °C																							
-1.0 °C	... 2.5 °C																							
2.5 °C	... 6.0 °C																							
6.0 °C	... 9.5 °C																							
9.5 °C	... 13.0 °C																							
13.0 °C	... 16.5 °C																							
16.5 °C	... 20.0 °C																							
Representation of characteristic isotherms			Representation of the critical isotherm																					
																								
<table><tr><td>— -10 °C</td><td>— 5 °C</td></tr><tr><td>— -5 °C</td><td>— 10 °C</td></tr><tr><td>— 0 °C</td><td>— 15 °C</td></tr></table>			— -10 °C	— 5 °C	— -5 °C	— 10 °C	— 0 °C	— 15 °C	— 13.12 °C															
— -10 °C	— 5 °C																							
— -5 °C	— 10 °C																							
— 0 °C	— 15 °C																							
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																				
1	$\theta_{Si} = 17.15 \text{ °C}$	$f_{Rsi} = 0.919$	$\theta_{Si} = 13.27 \text{ °C} > \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	meet																				
2	$\theta_{Si} = 13.27 \text{ °C}$	$f_{Rsi} = 0.808$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																					
Linear thermal transmittance			$\psi = 1.64216 - 0.862 \times 0.875 \times 2 = 0.134 \text{ W/(m.K)}$																					

Table 4.12.1 – Marking of the position of detail in the building – detail 12

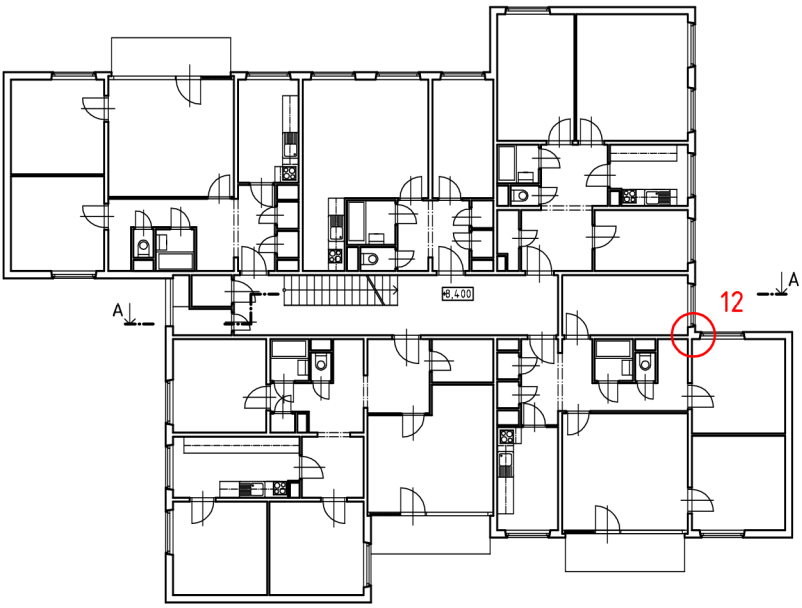
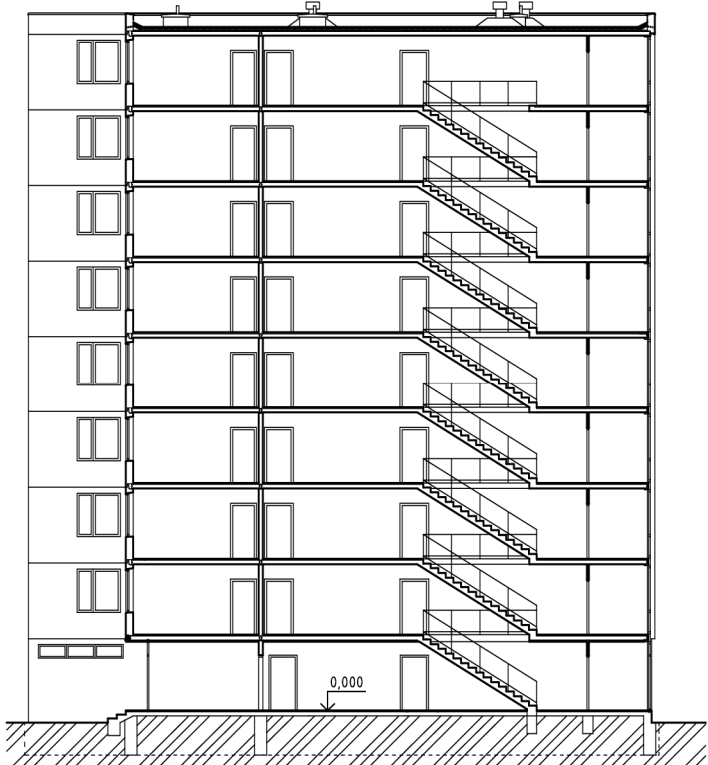
DETAIL 12
Floor plan

Section A-A


Table 4.12.2 – Structural composition of detail 12

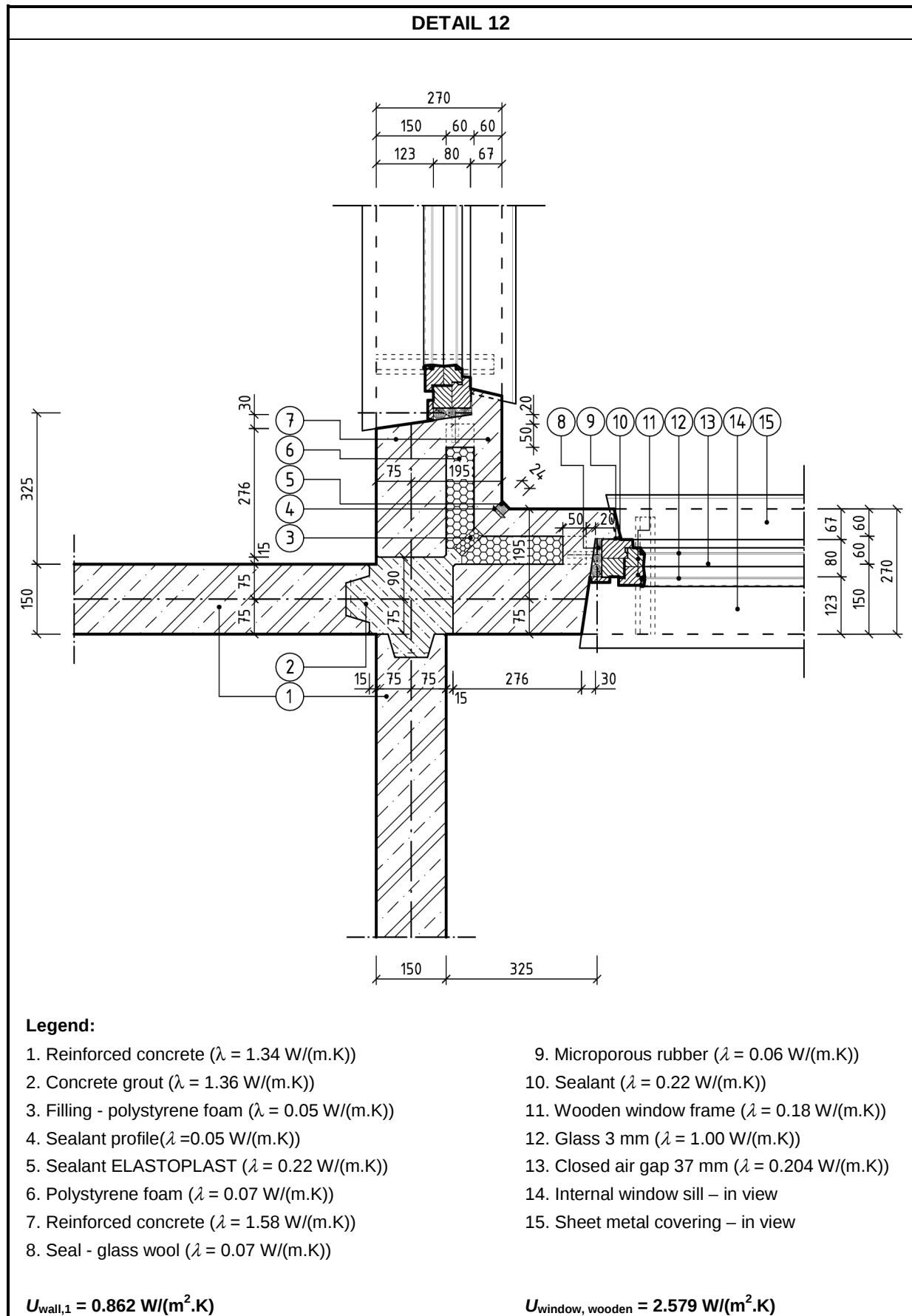


Table 4.12.3 – Boundary conditions for a calculation of detail 12

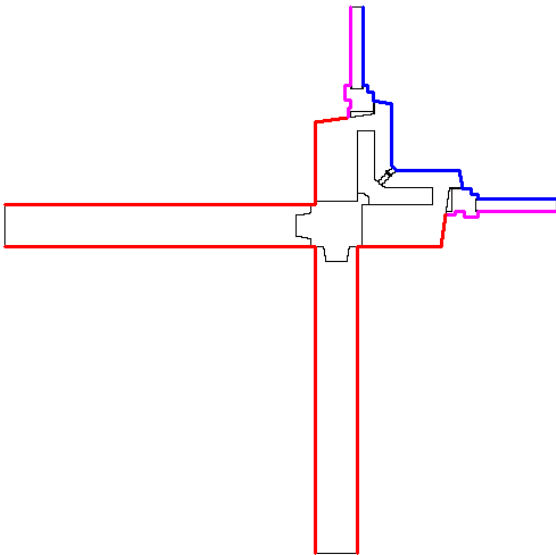
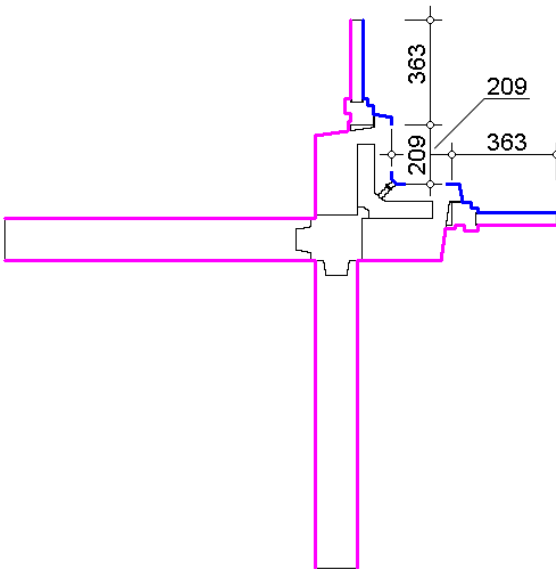
DETAIL 12	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$

Table 4.12.4 – Thermal-technical evaluation of detail 12

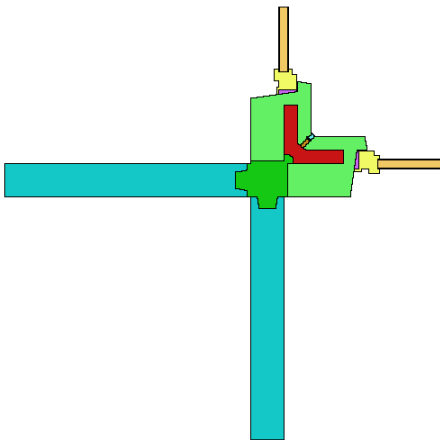
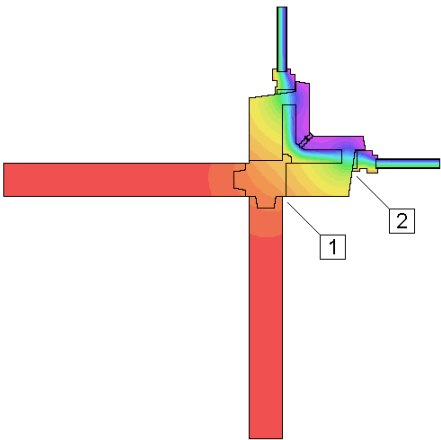
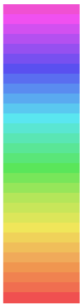
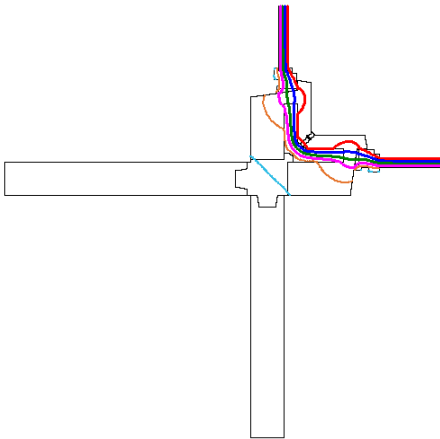
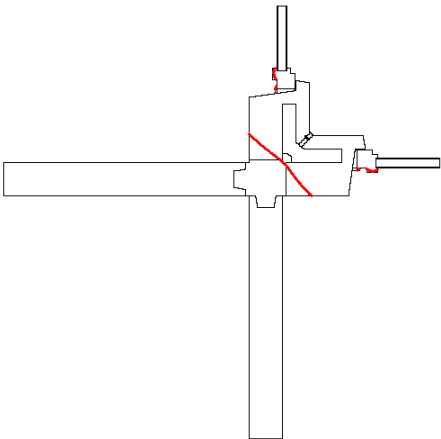
DETAIL 12																																																
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																													
																																																
Legend: <table><tr><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.067 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.067 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																													
	$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																													
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	$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$																																													
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	-5 °C		10 °C																																													
	0 °C		15 °C																																													
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																												
1	$\theta_{Si} = 15.85 \text{ °C}$	$f_{Rsi} = 0.881$	$\theta_{Si} = 6.65 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																												
2	$\theta_{Si} = 6.65 \text{ °C}$	$f_{Rsi} = 0.619$	$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																													
Linear thermal transmittance		$\psi = 3.07590 - (0.862 \times 0.209 \times 2) - (2.579 \times 0.363 \times 2) = 0.843 \text{ W/(m.K)}$																																														

Table 4.13.1 – Marking of the position of detail in the building – detail 13

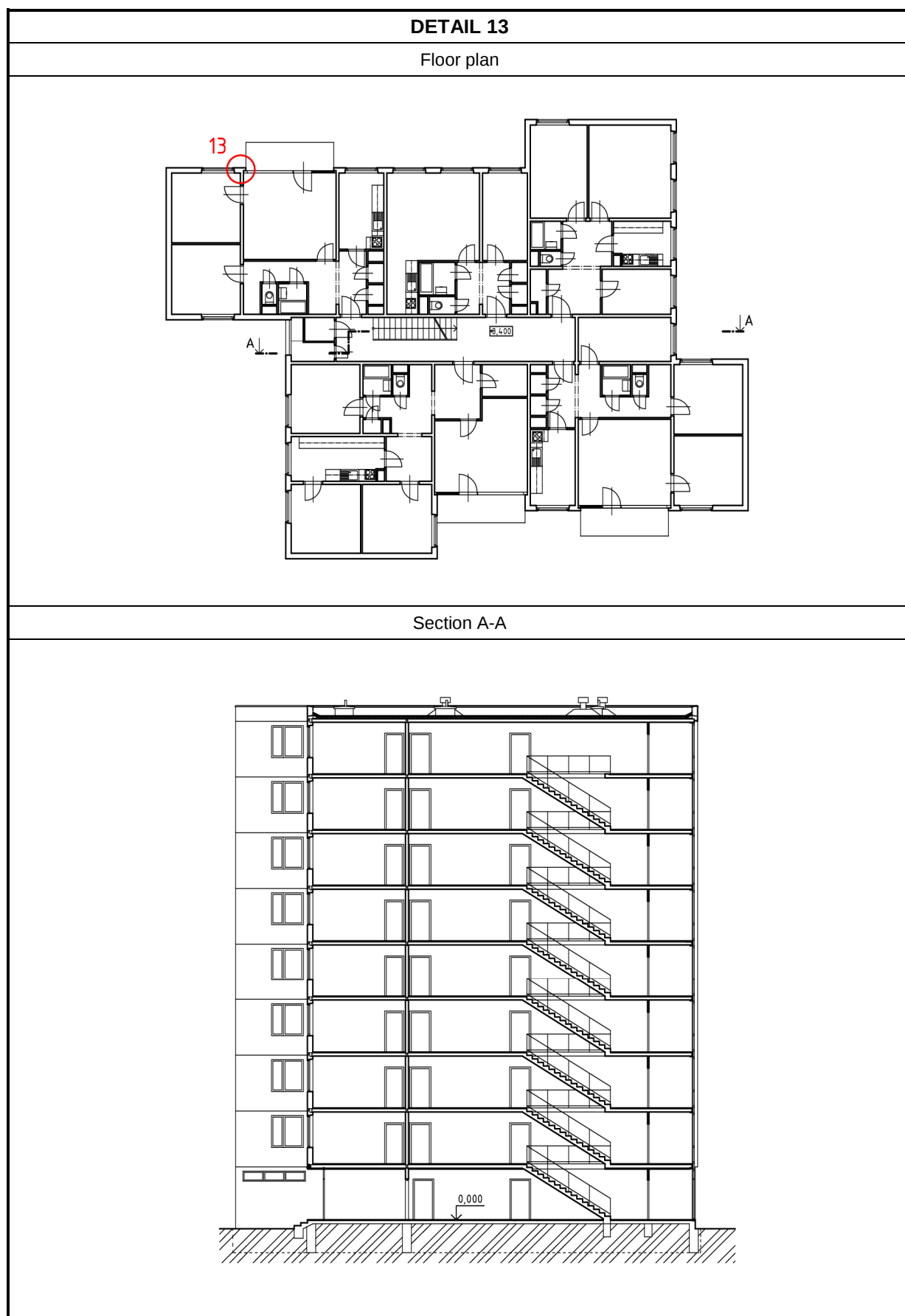


Table 4.13.2 – Structural composition of detail 13

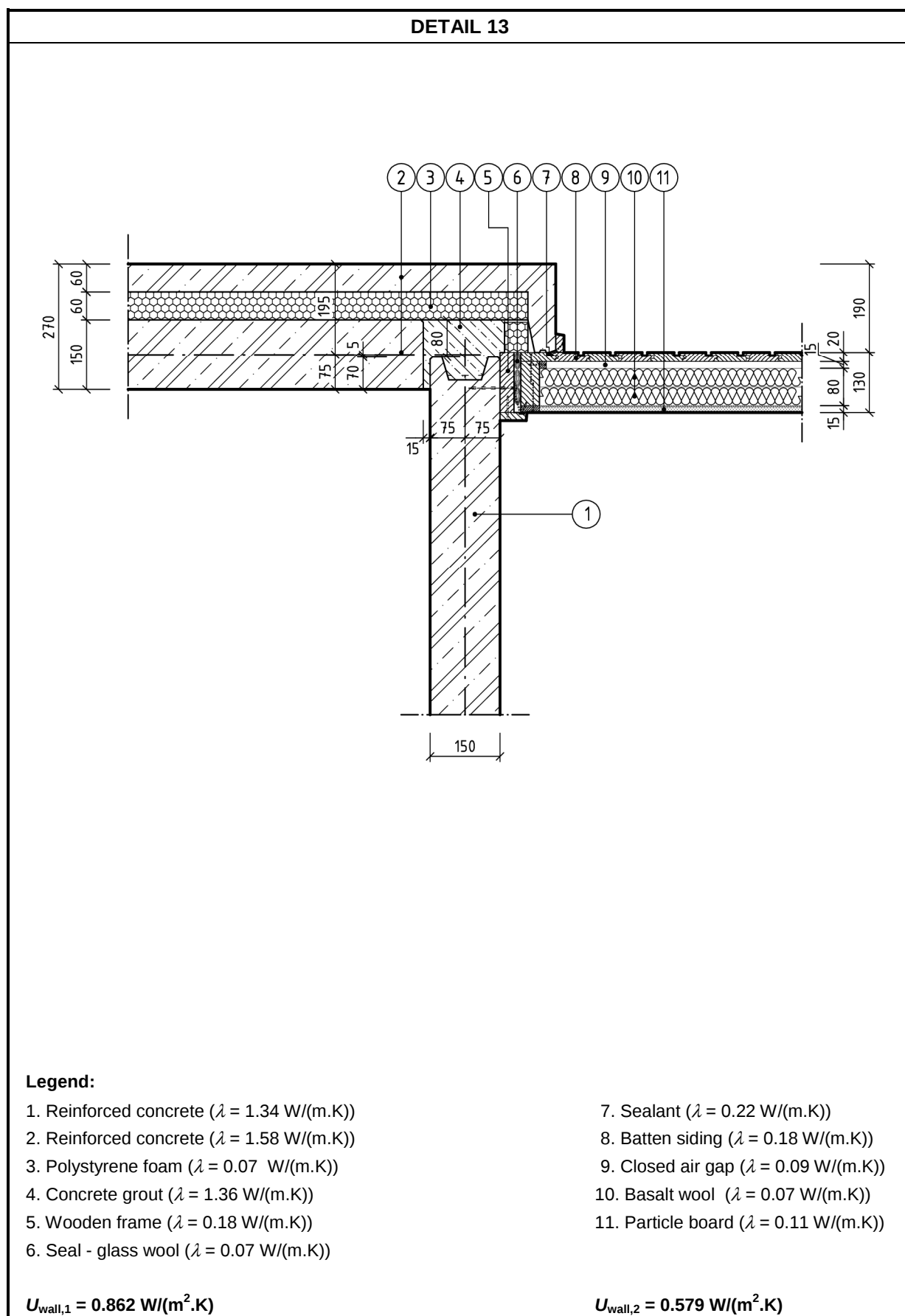


Table 4.13.3 – Boundary conditions for a calculation of detail 13

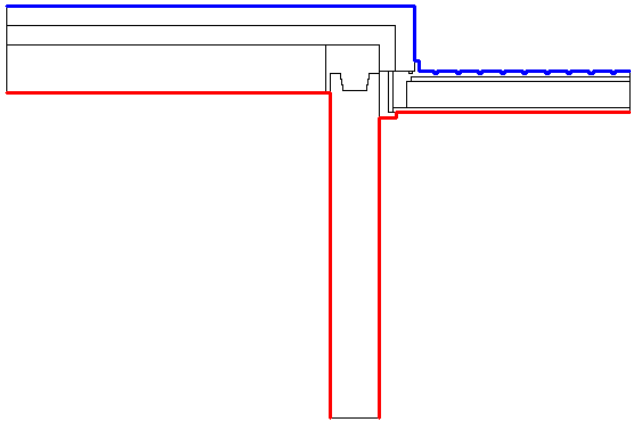
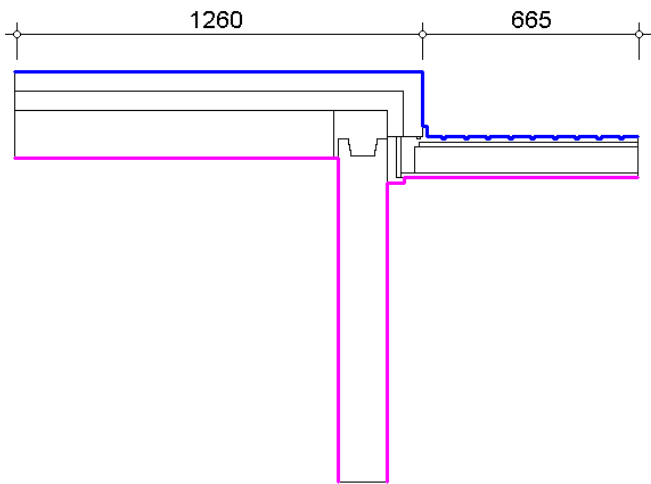
DETAIL 13	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$

Table 4.13.4 – Thermal-technical evaluation of detail 13

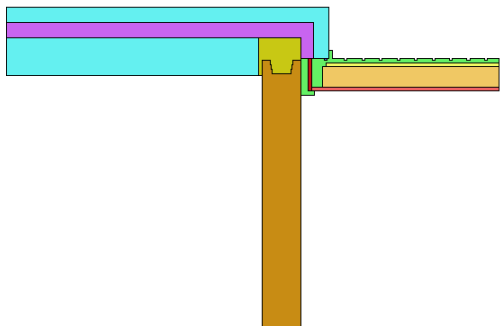
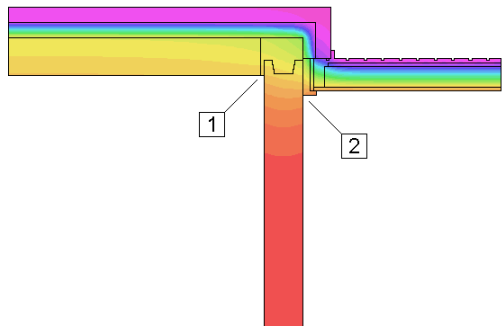
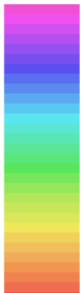
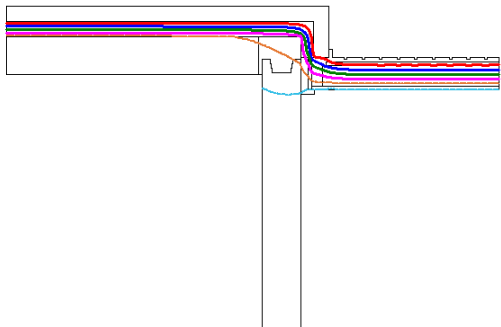
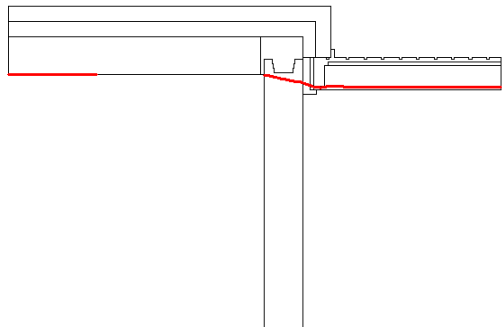
DETAIL 13																																												
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																									
																																												
Legend: <table><tr><td></td><td>$\lambda = 0.110 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.090 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 0.110 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.090 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 0.110 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$																																									
	$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																									
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Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																								
1	$\theta_{si} = 12.67 \text{ °C}$	$f_{Rsi} = 0.791$	$\theta_{si} = 12.67 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet																																								
2	$\theta_{si} = 15.39 \text{ °C}$	$f_{Rsi} = 0.868$	$\theta_{si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																									
Linear thermal transmittance			$\psi = 1.56271 - 0.862 \times 1.260 - 0.579 \times 0.665 = 0.092 \text{ W/(m.K)}$																																									

Table 4.14.1 – Marking of the position of detail in the building – detail 14

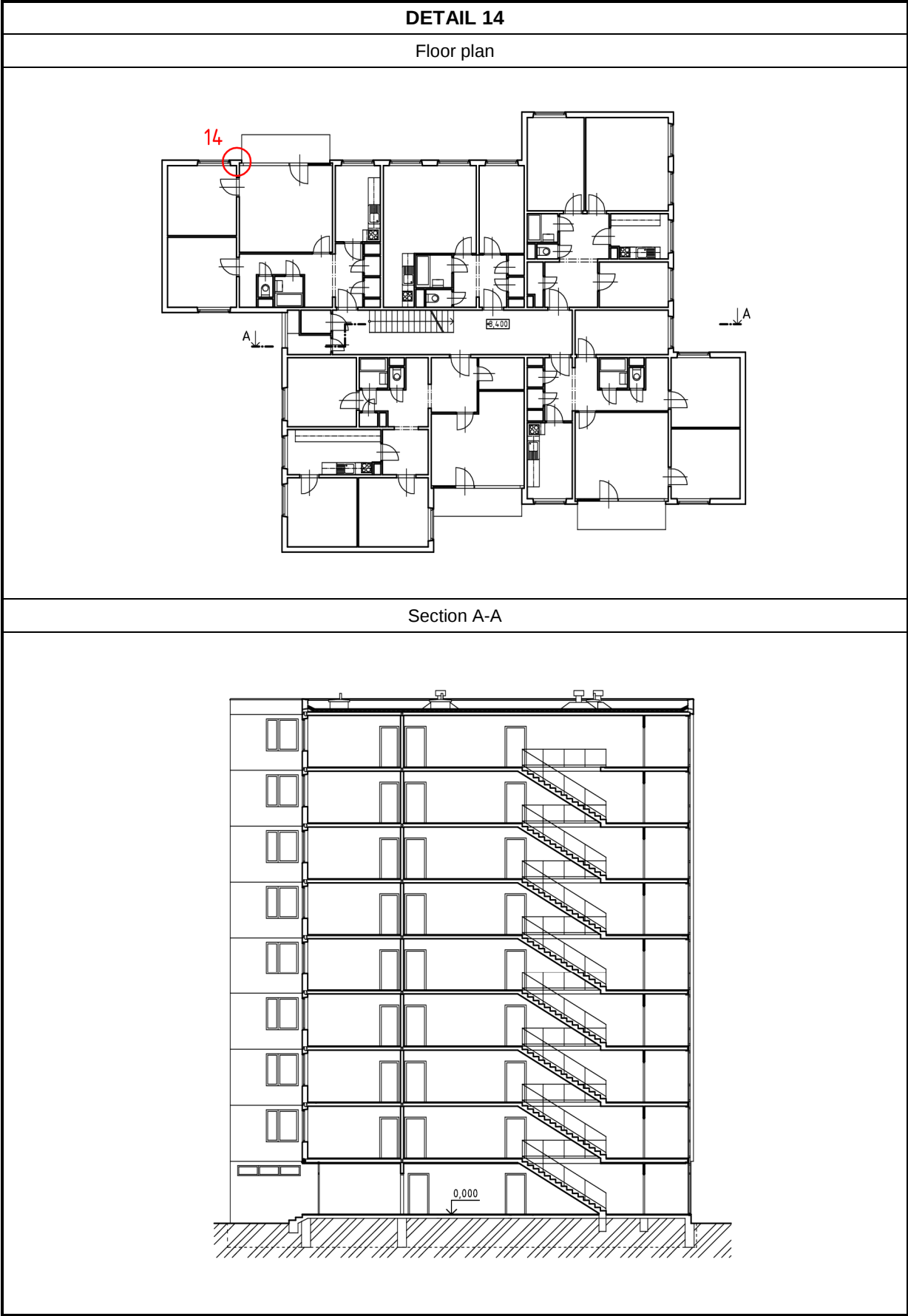


Table 4.14.2 – Structural composition of detail 14

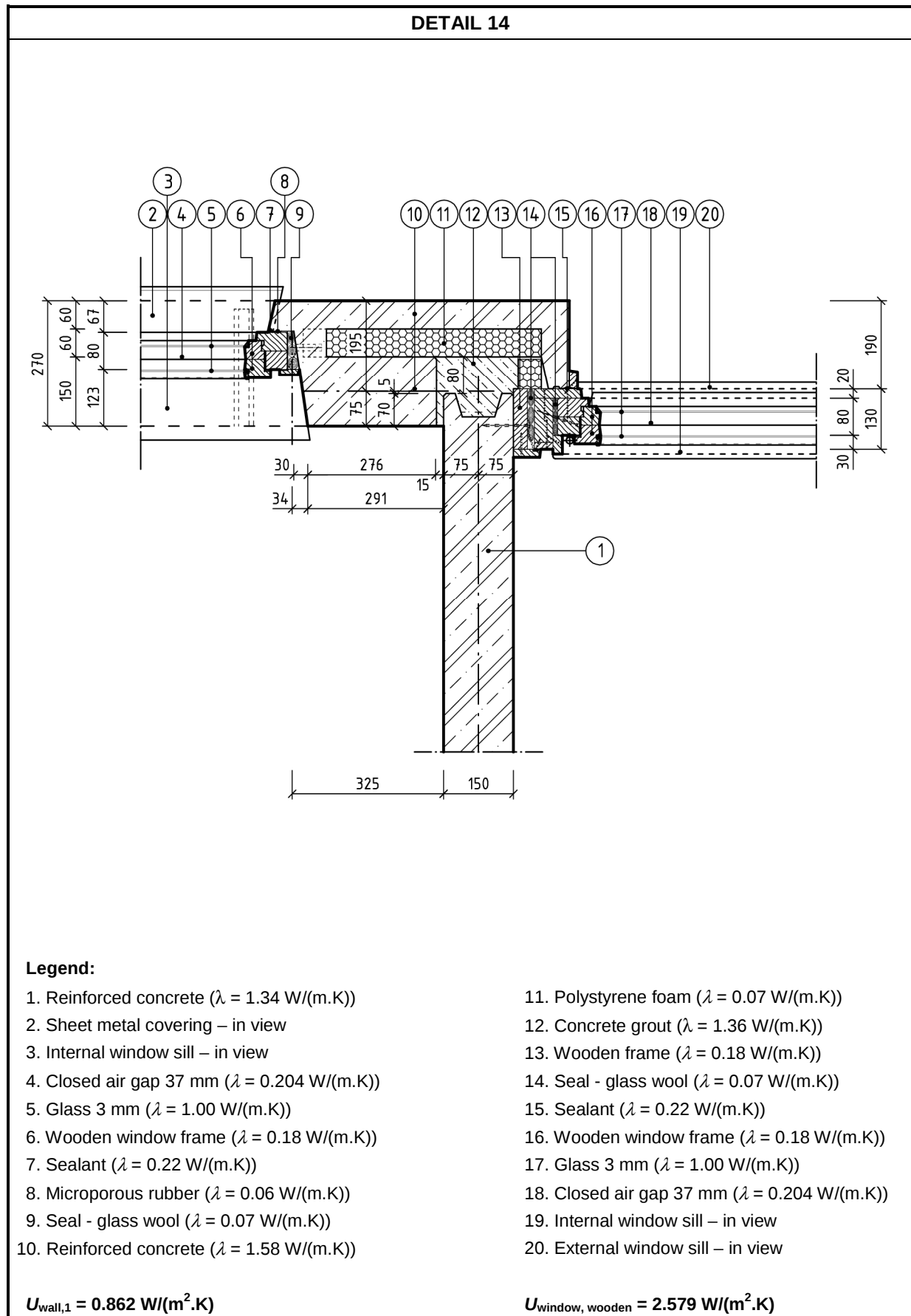


Table 4.14.3 – Boundary conditions for a calculation of detail 14

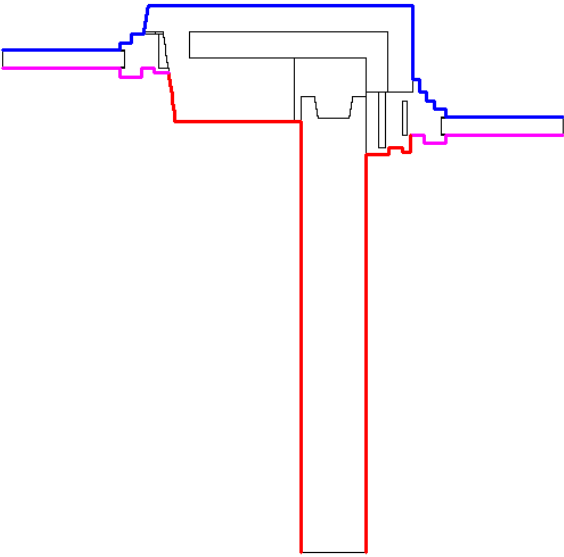
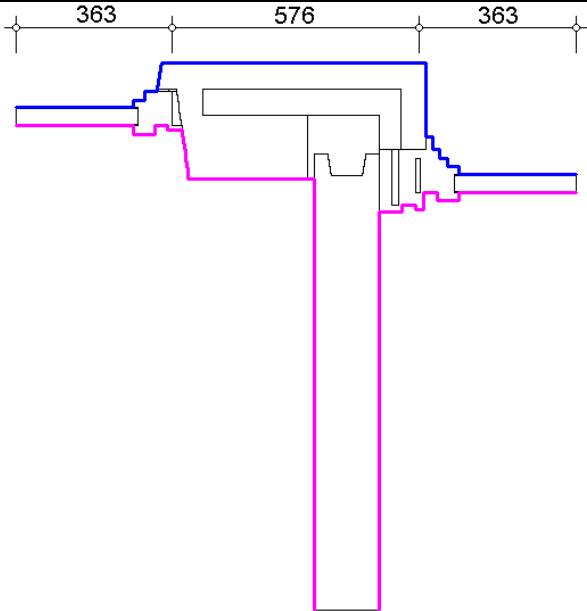
DETAIL 14	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.14.4 – Thermal-technical evaluation of detail 14

DETAIL 14																																		
Modeled detail with marking the materials			Temperature field with marked critical temperatures																															
Legend: <table><tr><td>■ $\lambda = 1.000 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 0.204 \text{ W/(m.K)}$</td><td>■ $\lambda = 1.340 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 0.180 \text{ W/(m.K)}$</td><td>■ $\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 1.580 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.060 \text{ W/(m.K)}$</td></tr><tr><td>■ $\lambda = 0.070 \text{ W/(m.K)}$</td><td>■ $\lambda = 0.220 \text{ W/(m.K)}$</td></tr></table>			■ $\lambda = 1.000 \text{ W/(m.K)}$	■ $\lambda = 0.070 \text{ W/(m.K)}$	■ $\lambda = 0.204 \text{ W/(m.K)}$	■ $\lambda = 1.340 \text{ W/(m.K)}$	■ $\lambda = 0.180 \text{ W/(m.K)}$	■ $\lambda = 1.360 \text{ W/(m.K)}$	■ $\lambda = 1.580 \text{ W/(m.K)}$	■ $\lambda = 0.060 \text{ W/(m.K)}$	■ $\lambda = 0.070 \text{ W/(m.K)}$	■ $\lambda = 0.220 \text{ W/(m.K)}$	<table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
■ $\lambda = 1.000 \text{ W/(m.K)}$	■ $\lambda = 0.070 \text{ W/(m.K)}$																																	
■ $\lambda = 0.204 \text{ W/(m.K)}$	■ $\lambda = 1.340 \text{ W/(m.K)}$																																	
■ $\lambda = 0.180 \text{ W/(m.K)}$	■ $\lambda = 1.360 \text{ W/(m.K)}$																																	
■ $\lambda = 1.580 \text{ W/(m.K)}$	■ $\lambda = 0.060 \text{ W/(m.K)}$																																	
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-11.5 °C	... -8.0 °C																																	
-8.0 °C	... -4.5 °C																																	
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13.0 °C	... 16.5 °C																																	
16.5 °C	... 20.0 °C																																	
Representation of characteristic isotherms			Representation of the critical isotherm																															
<table><tr><td>— -10 °C</td><td>— 5 °C</td></tr><tr><td>— -5 °C</td><td>— 10 °C</td></tr><tr><td>— 0 °C</td><td>— 15 °C</td></tr></table>			— -10 °C	— 5 °C	— -5 °C	— 10 °C	— 0 °C	— 15 °C	— 13.12 °C																									
— -10 °C	— 5 °C																																	
— -5 °C	— 10 °C																																	
— 0 °C	— 15 °C																																	
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																														
1	$\theta_{Si} = 5.55 \text{ °C}$	$f_{RSi} = 0.587$	$\theta_{Si} = 5.55 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																														
2	$\theta_{Si} = 12.01 \text{ °C}$	$f_{RSi} = 0.772$	$\theta_{Si} = f_{RSi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																															
3	$\theta_{Si} = 14.76 \text{ °C}$	$f_{RSi} = 0.850$																																
Linear thermal transmittance			$\psi = 2.79616 - 0.862 \times 0.576 - (2.579 \times 0.363 \times 2) = 0.427 \text{ W/(m.K)}$																															

Table 4.15.1 – Marking of the position of detail in the building – detail 15

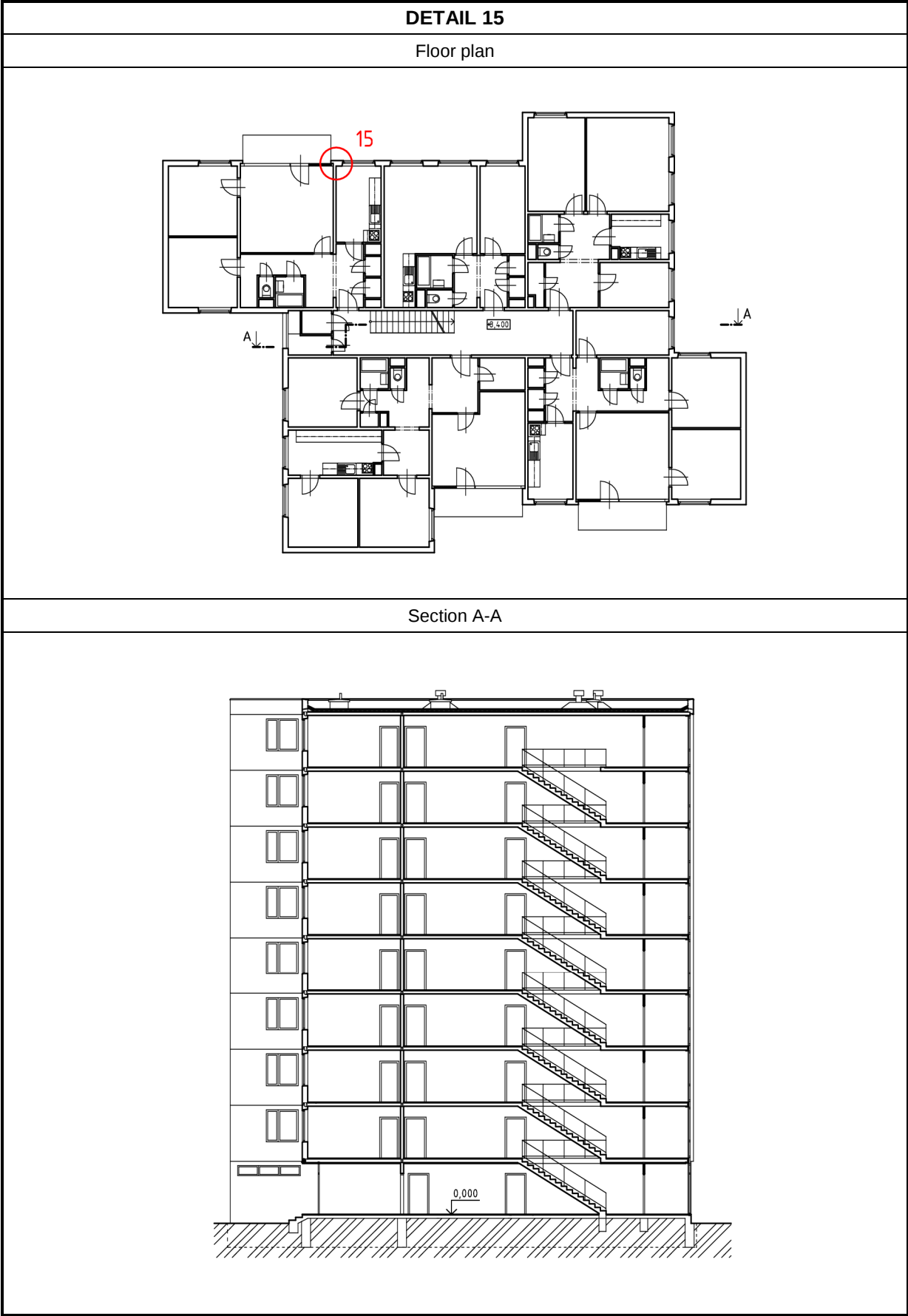


Table 4.15.2 – Structural composition of detail 15

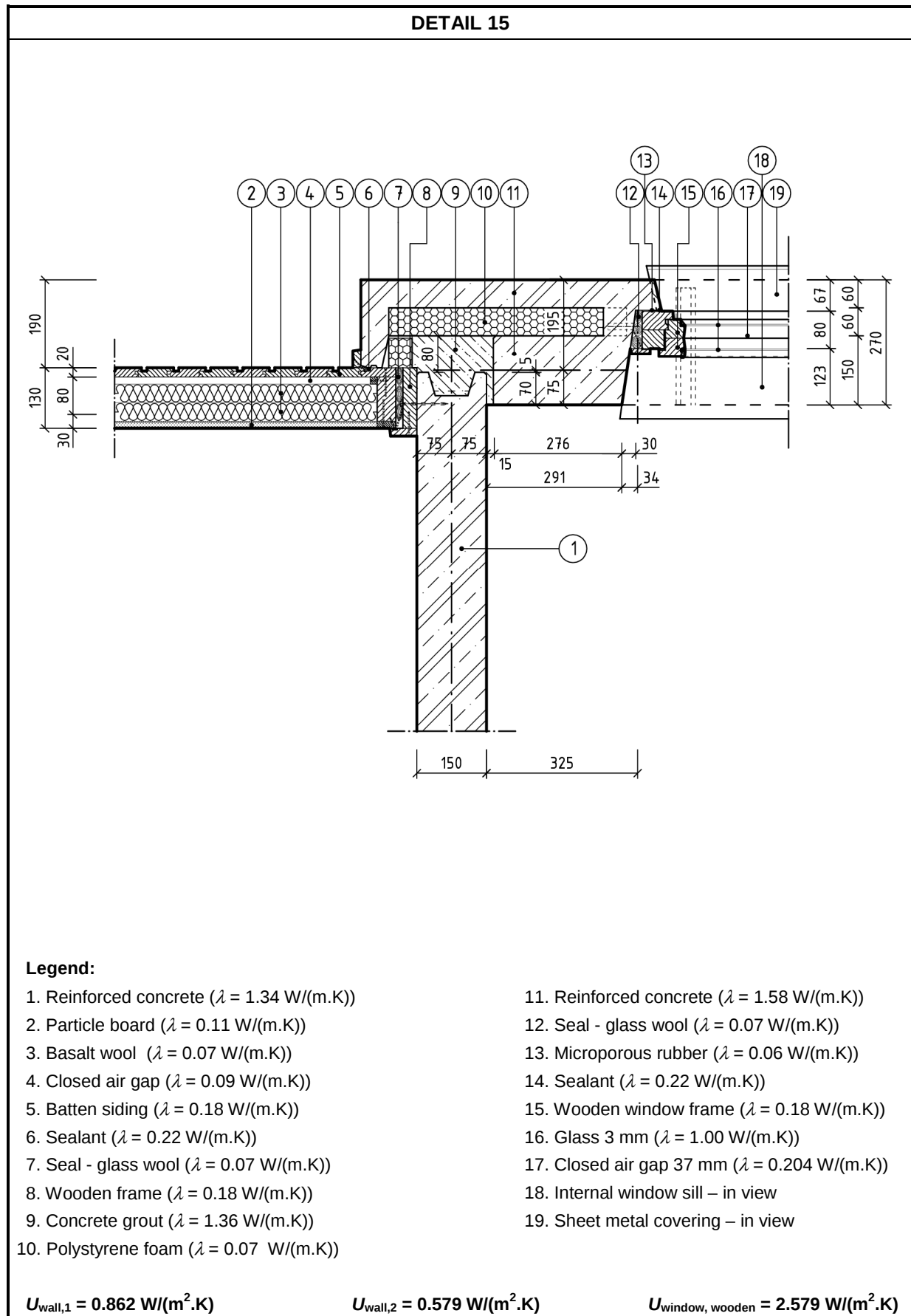


Table 4.15.3 – Boundary conditions for a calculation of detail 15

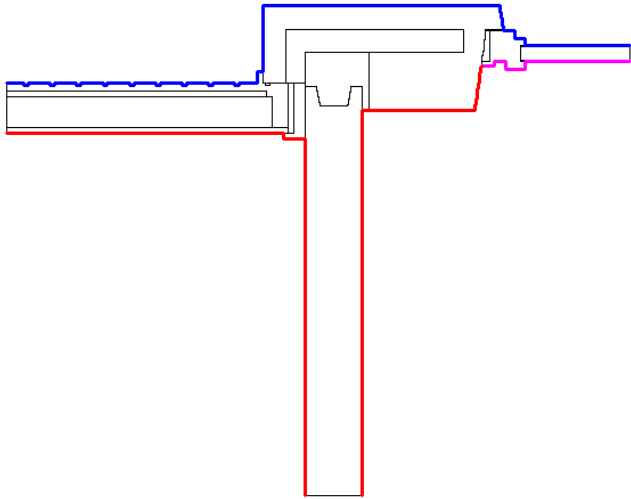
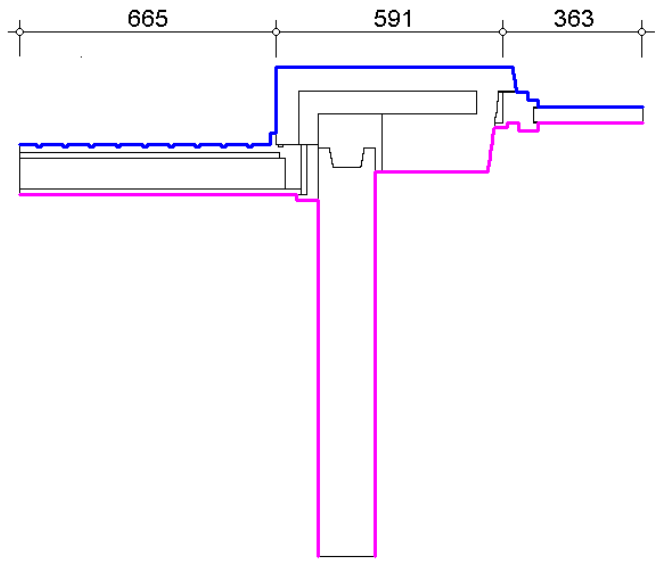
DETAIL 15	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.15.4 – Thermal-technical evaluation of detail 15

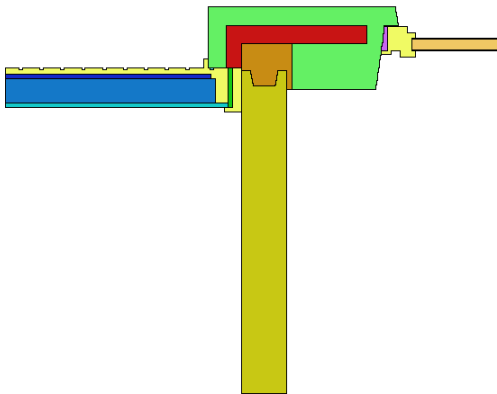
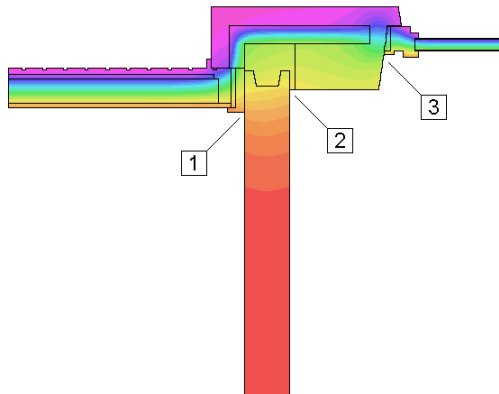
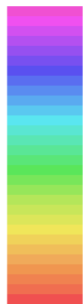
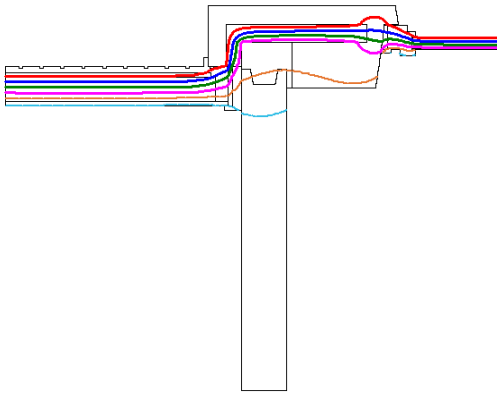
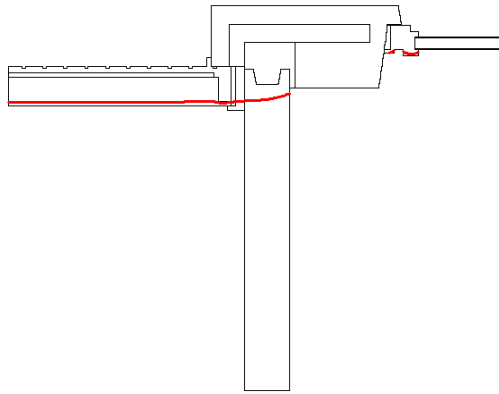
DETAIL 15																																																				
Modeled detail with marking the materials		Temperature field with marked critical temperatures																																																		
																																																				
Legend: <table><tr><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.110 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.090 \text{ W/(m.K)}$</td></tr></table>			$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.110 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.090 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>			-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																																	
	$\lambda = 0.204 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$																																																	
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16.5 °C	... 20.0 °C																																																			
Representation of characteristic isotherms		Representation of the critical isotherm																																																		
																																																				
<table><tr><td></td><td>-10 °C</td><td></td><td>5 °C</td></tr><tr><td></td><td>-5 °C</td><td></td><td>10 °C</td></tr><tr><td></td><td>0 °C</td><td></td><td>15 °C</td></tr></table>			-10 °C		5 °C		-5 °C		10 °C		0 °C		15 °C	13.12 °C																																						
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	0 °C		15 °C																																																	
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																																
1	$\theta_{si} = 14.68 \text{ °C}$	$f_{Rsi} = 0.848$	$\theta_{si} = 5.53 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet																																																
2	$\theta_{si} = 11.96 \text{ °C}$	$f_{Rsi} = 0.770$	$\theta_{si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																																	
3	$\theta_{si} = 5.53 \text{ °C}$	$f_{Rsi} = 0.587$																																																		
Linear thermal transmittance		$\psi = 2.25982 - 0.862 \times 0.591 - 0.579 \times 0.665 - 2.579 \times 0.363 = 0.429 \text{ W/(m.K)}$																																																		

Table 4.16.1 – Marking of the position of detail in the building – detail 16

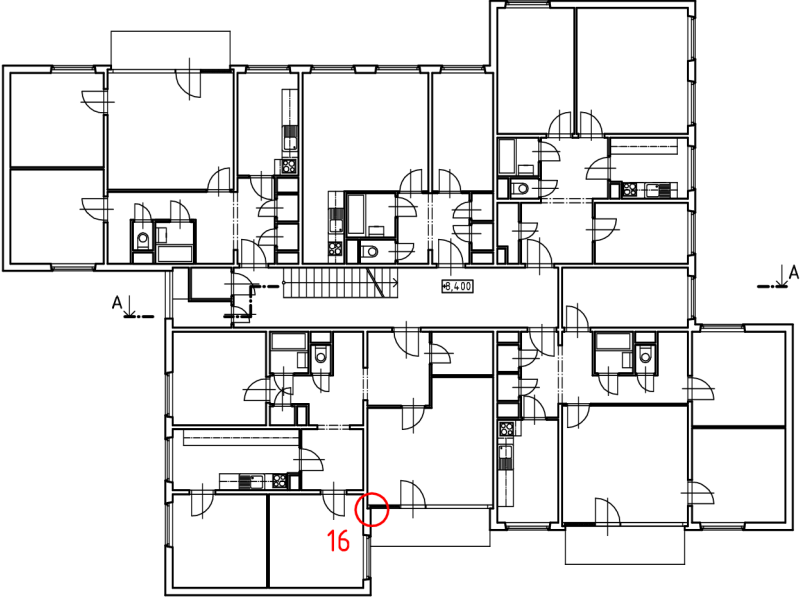
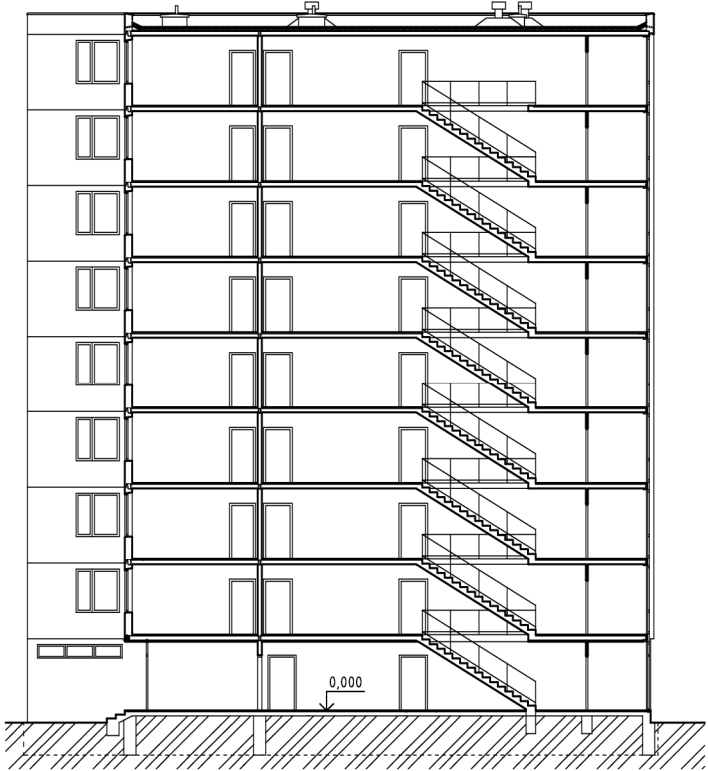
DETAIL 16
Floor plan

Section A-A


Table 4.16.2 – Structural composition of detail 16

DETAIL 16													
Legend: <table> <tbody> <tr> <td>1. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)</td><td>7. Sealant ($\lambda = 0.22 \text{ W/(m.K)}$)</td></tr> <tr> <td>2. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)</td><td>8. Batten siding ($\lambda = 0.18 \text{ W/(m.K)}$)</td></tr> <tr> <td>3. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)</td><td>9. Closed air gap ($\lambda = 0.09 \text{ W/(m.K)}$)</td></tr> <tr> <td>4. Wooden frame ($\lambda = 0.18 \text{ W/(m.K)}$)</td><td>10. Basalt wool ($\lambda = 0.07 \text{ W/(m.K)}$)</td></tr> <tr> <td>5. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)</td><td>11. Particle board ($\lambda = 0.11 \text{ W/(m.K)}$)</td></tr> <tr> <td>6. Reinforced concrete ($\lambda = 1.34 \text{ W/(m.K)}$)</td><td></td></tr> </tbody> </table>		1. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)	7. Sealant ($\lambda = 0.22 \text{ W/(m.K)}$)	2. Polystyrene foam ($\lambda = 0.07 \text{ W/(m.K)}$)	8. Batten siding ($\lambda = 0.18 \text{ W/(m.K)}$)	3. Reinforced concrete ($\lambda = 1.58 \text{ W/(m.K)}$)	9. Closed air gap ($\lambda = 0.09 \text{ W/(m.K)}$)	4. Wooden frame ($\lambda = 0.18 \text{ W/(m.K)}$)	10. Basalt wool ($\lambda = 0.07 \text{ W/(m.K)}$)	5. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)	11. Particle board ($\lambda = 0.11 \text{ W/(m.K)}$)	6. Reinforced concrete ($\lambda = 1.34 \text{ W/(m.K)}$)	
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6. Reinforced concrete ($\lambda = 1.34 \text{ W/(m.K)}$)													
$U_{\text{wall},1} = 0.862 \text{ W/(m}^2\text{.K)}$	$U_{\text{wall},2} = 0.579 \text{ W/(m}^2\text{.K)}$												

Table 4.16.3 – Boundary conditions for a calculation of detail 16

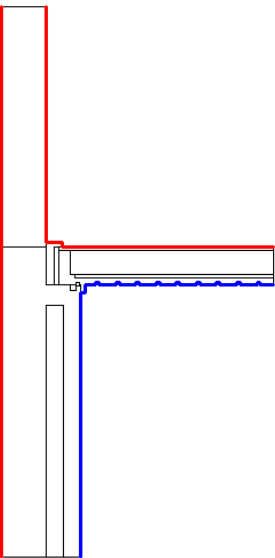
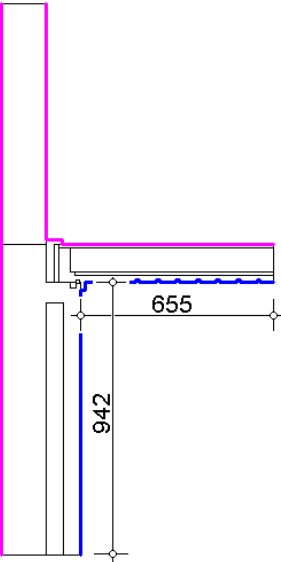
DETAIL 16	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$

Table 4.16.4 – Thermal-technical evaluation of detail 16

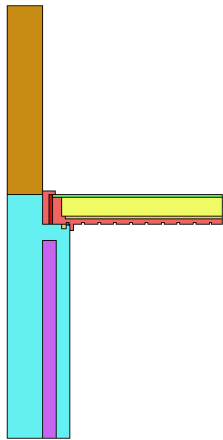
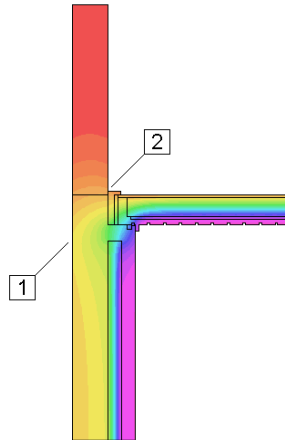
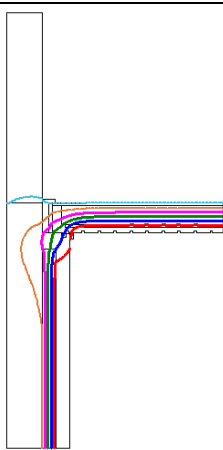
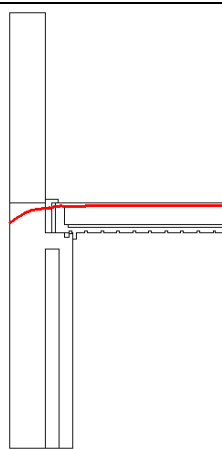
DETAIL 16				
Modeled detail with marking the materials			Temperature field with marked critical temperatures	
				
Legend: $\lambda = 0.180 \text{ W/(m.K)}$ $\lambda = 0.090 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ $\lambda = 0.110 \text{ W/(m.K)}$ $\lambda = 1.580 \text{ W/(m.K)}$ $\lambda = 0.220 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ $\lambda = 1.340 \text{ W/(m.K)}$ <td colspan="2"> -15.0 °C ... -11.5 °C -11.5 °C ... -8.0 °C -8.0 °C ... -4.5 °C -4.5 °C ... -1.0 °C -1.0 °C ... 2.5 °C 2.5 °C ... 6.0 °C 6.0 °C ... 9.5 °C 9.5 °C ... 13.0 °C 13.0 °C ... 16.5 °C 16.5 °C ... 20.0 °C </td>			-15.0 °C ... -11.5 °C -11.5 °C ... -8.0 °C -8.0 °C ... -4.5 °C -4.5 °C ... -1.0 °C -1.0 °C ... 2.5 °C 2.5 °C ... 6.0 °C 6.0 °C ... 9.5 °C 9.5 °C ... 13.0 °C 13.0 °C ... 16.5 °C 16.5 °C ... 20.0 °C	
Representation of characteristic isotherms			Representation of the critical isotherm	
				
-10 °C -5 °C 0 °C 5 °C 10 °C 15 °C			13.12 °C	
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating
1	$\theta_{si} = 11.62 \text{ °C}$	$f_{Rsi} = 0.761$	$\theta_{si} = 11.62 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet
2	$\theta_{si} = 14.92 \text{ °C}$	$f_{Rsi} = 0.855$	$\theta_{si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)	
Linear thermal transmittance			$\psi = 1.62728 - 0.862 \times 0.942 - 0.579 \times 0.655 = 0.436 \text{ W/(m.K)}$	

Table 4.17.1 – Marking of the position of detail in the building – detail 17

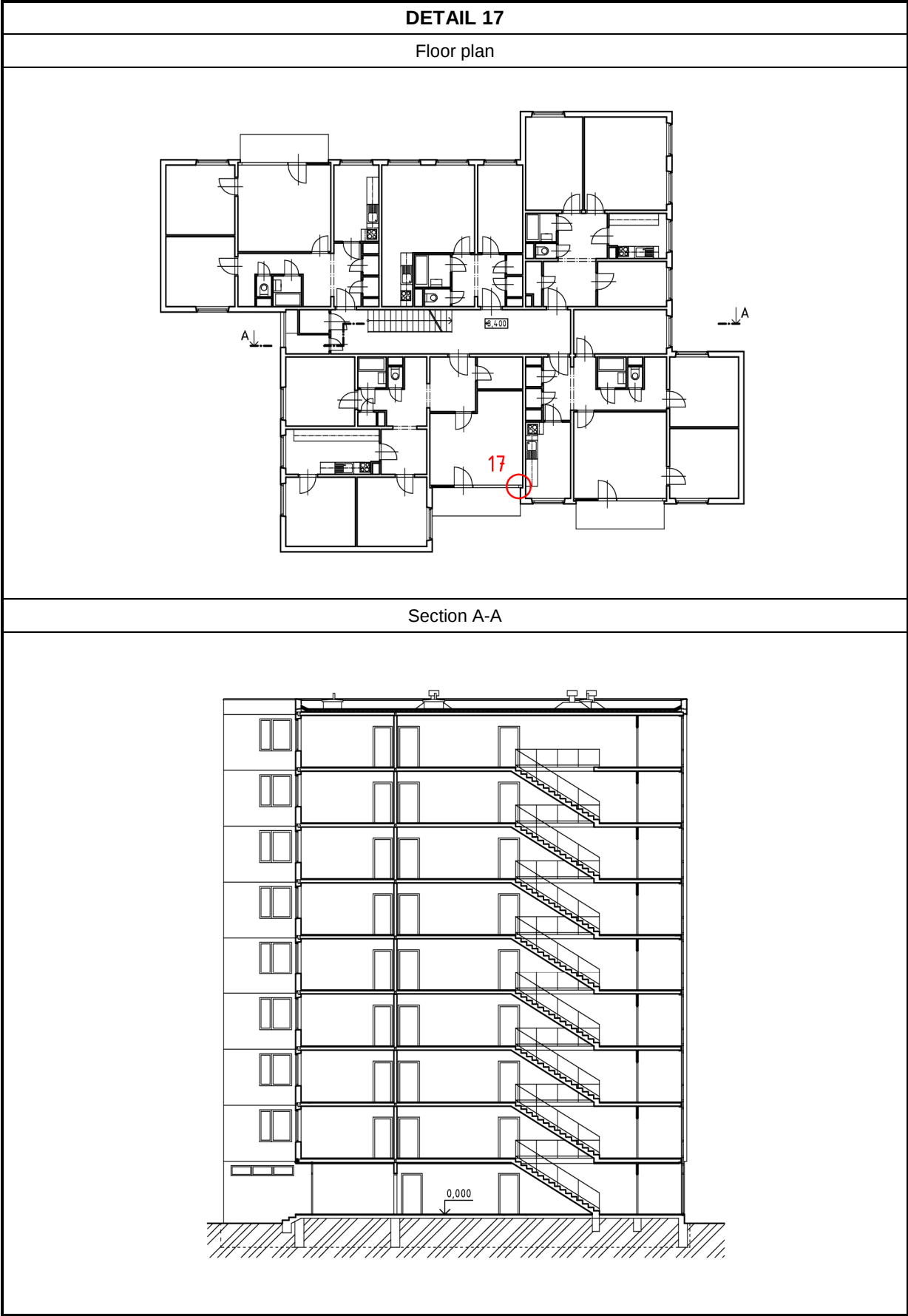


Table 4.17.2 – Structural composition of detail 17

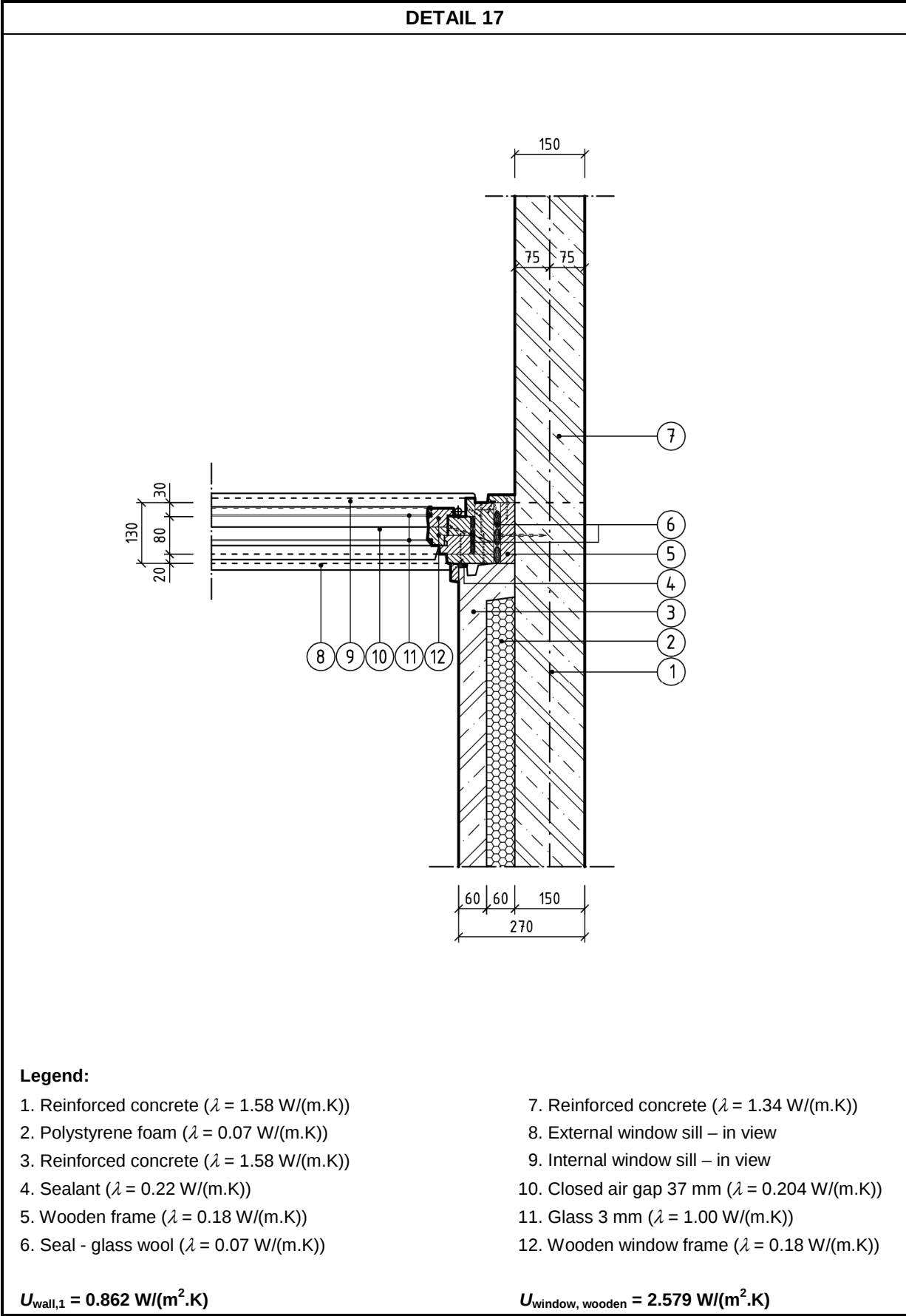


Table 4.17.3 – Boundary conditions for a calculation of detail 17

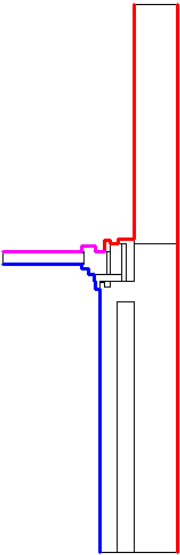
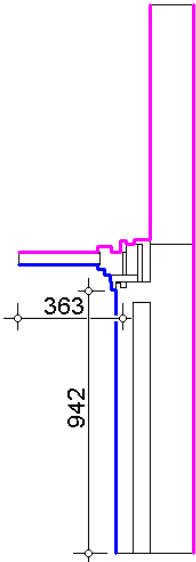
DETAIL 17	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.17.4 – Thermal-technical evaluation of detail 17

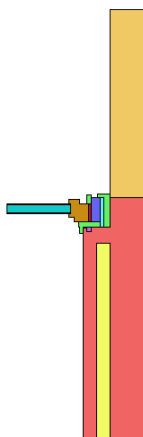
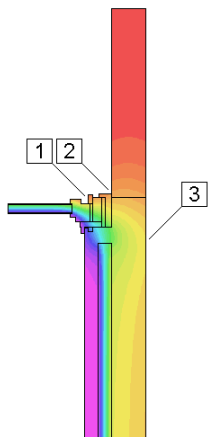
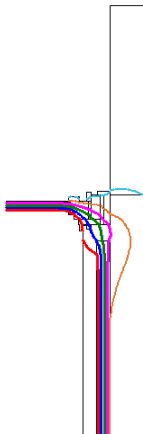
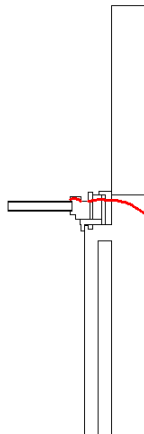
DETAIL 17																																																
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																													
																																																
Legend: <table><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.090 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.090 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.090 \text{ W/(m.K)}$																																													
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	-10 °C		5 °C																																													
	-5 °C		10 °C																																													
	0 °C		15 °C																																													
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																												
1	$\theta_{si} = 11.59 \text{ °C}$	$f_{Rsi} = 0.760$	$\theta_{si} = 11.59 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet																																												
2	$\theta_{si} = 14.94 \text{ °C}$	$f_{Rsi} = 0.855$	$\theta_{si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																													
3	$\theta_{si} = 13.05 \text{ °C}$	$f_{Rsi} = 0.801$																																														
Linear thermal transmittance			$\psi = 2.16787 - 0.862 \times 0.942 - 2.579 \times 0.363 = 0.420 \text{ W/(m.K)}$																																													

Table 4.18.1 – Marking of the position of detail in the building – detail 18

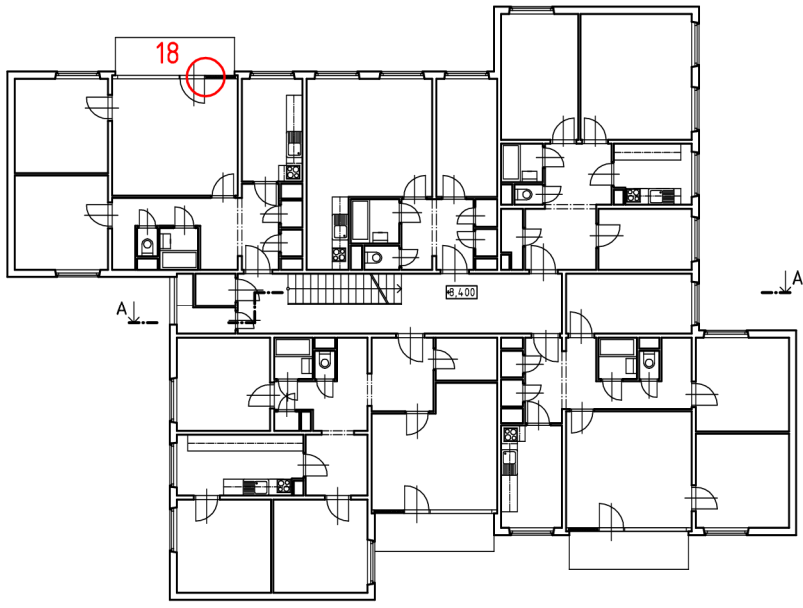
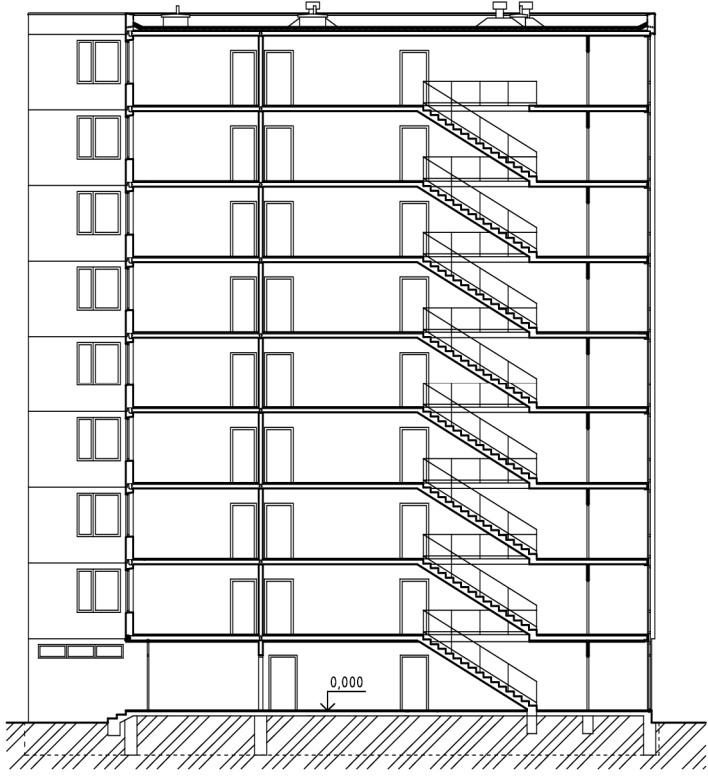
DETAIL 18
Floor plan 
Section A-A 

Table 4.18.2 – Structural composition of detail 18

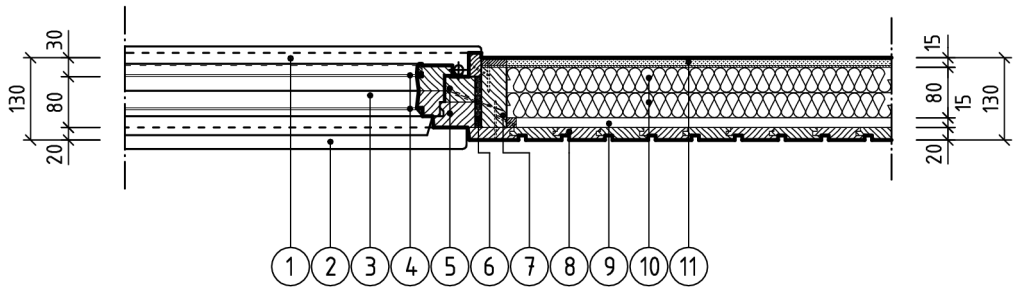
DETAIL 18													
													
Legend: <table><tbody><tr><td>1. Internal window sill – in view</td><td>7. Wooden frame ($\lambda = 0.18 \text{ W/(m.K)}$)</td></tr><tr><td>2. External window sill – in view</td><td>8. Batten siding ($\lambda = 0.18 \text{ W/(m.K)}$)</td></tr><tr><td>3. Closed air gap 37 mm ($\lambda = 0.204 \text{ W/(m.K)}$)</td><td>9. Closed air gap ($\lambda = 0.09 \text{ W/(m.K)}$)</td></tr><tr><td>4. Glass 3 mm ($\lambda = 1.00 \text{ W/(m.K)}$)</td><td>10. Basalt wool ($\lambda = 0.07 \text{ W/(m.K)}$)</td></tr><tr><td>5. Wooden window frame ($\lambda = 0.18 \text{ W/(m.K)}$)</td><td>11. Particle board ($\lambda = 0.11 \text{ W/(m.K)}$)</td></tr><tr><td>6. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)</td><td></td></tr></tbody></table>		1. Internal window sill – in view	7. Wooden frame ($\lambda = 0.18 \text{ W/(m.K)}$)	2. External window sill – in view	8. Batten siding ($\lambda = 0.18 \text{ W/(m.K)}$)	3. Closed air gap 37 mm ($\lambda = 0.204 \text{ W/(m.K)}$)	9. Closed air gap ($\lambda = 0.09 \text{ W/(m.K)}$)	4. Glass 3 mm ($\lambda = 1.00 \text{ W/(m.K)}$)	10. Basalt wool ($\lambda = 0.07 \text{ W/(m.K)}$)	5. Wooden window frame ($\lambda = 0.18 \text{ W/(m.K)}$)	11. Particle board ($\lambda = 0.11 \text{ W/(m.K)}$)	6. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)	
1. Internal window sill – in view	7. Wooden frame ($\lambda = 0.18 \text{ W/(m.K)}$)												
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6. Seal - glass wool ($\lambda = 0.07 \text{ W/(m.K)}$)													
$U_{\text{wall},2} = 0.579 \text{ W/(m}^2\text{.K)}$	$U_{\text{window, wooden}} = 2.579 \text{ W/(m}^2\text{.K)}$												

Table 4.18.3 – Boundary conditions for a calculation of detail 18

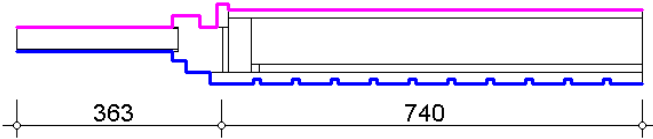
DETAIL 18	
Boundary conditions for calculation of surface temperatures	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance	
	
Boundary conditions for interior	Boundary conditions for exterior
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$

Table 4.18.4 – Thermal-technical evaluation of detail 18

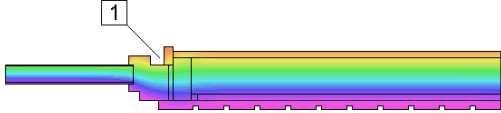
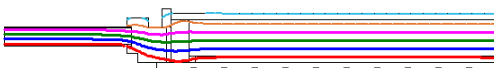
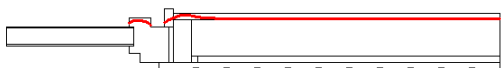
DETAIL 18																																												
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																									
																																												
Legend: <table><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.090 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.110 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.180 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.204 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.090 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.110 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.204 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 0.180 \text{ W/(m.K)}$		$\lambda = 0.180 \text{ W/(m.K)}$																																									
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-11.5 °C	... -8.0 °C																																											
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Representation of characteristic isotherms			Representation of the critical isotherm																																									
																																												
<table><tr><td></td><td>-10 °C</td><td></td><td>5 °C</td></tr><tr><td></td><td>-5 °C</td><td></td><td>10 °C</td></tr><tr><td></td><td>0 °C</td><td></td><td>15 °C</td></tr></table>				-10 °C		5 °C		-5 °C		10 °C		0 °C		15 °C	 13.12 °C																													
	-10 °C		5 °C																																									
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Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																								
1	$\theta_{Si} = 10.91 \text{ °C}$	$f_{Rsi} = 0.740$	$\theta_{Si} = 10.91 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																								
			$\theta_{Si} = f_{Rsi} \cdot (\theta_i - \theta_e) + \theta_e$ (Considered $\theta_i = 20 \text{ °C}$; $\theta_e = -15 \text{ °C}$)																																									
Linear thermal transmittance			$\psi = 1.39660 - 0.579 \times 0.740 - 2.579 \times 0.363 = 0.032 \text{ W/(m.K)}$																																									

Table 4.19.1 – Marking of the position of detail in the building – detail 19

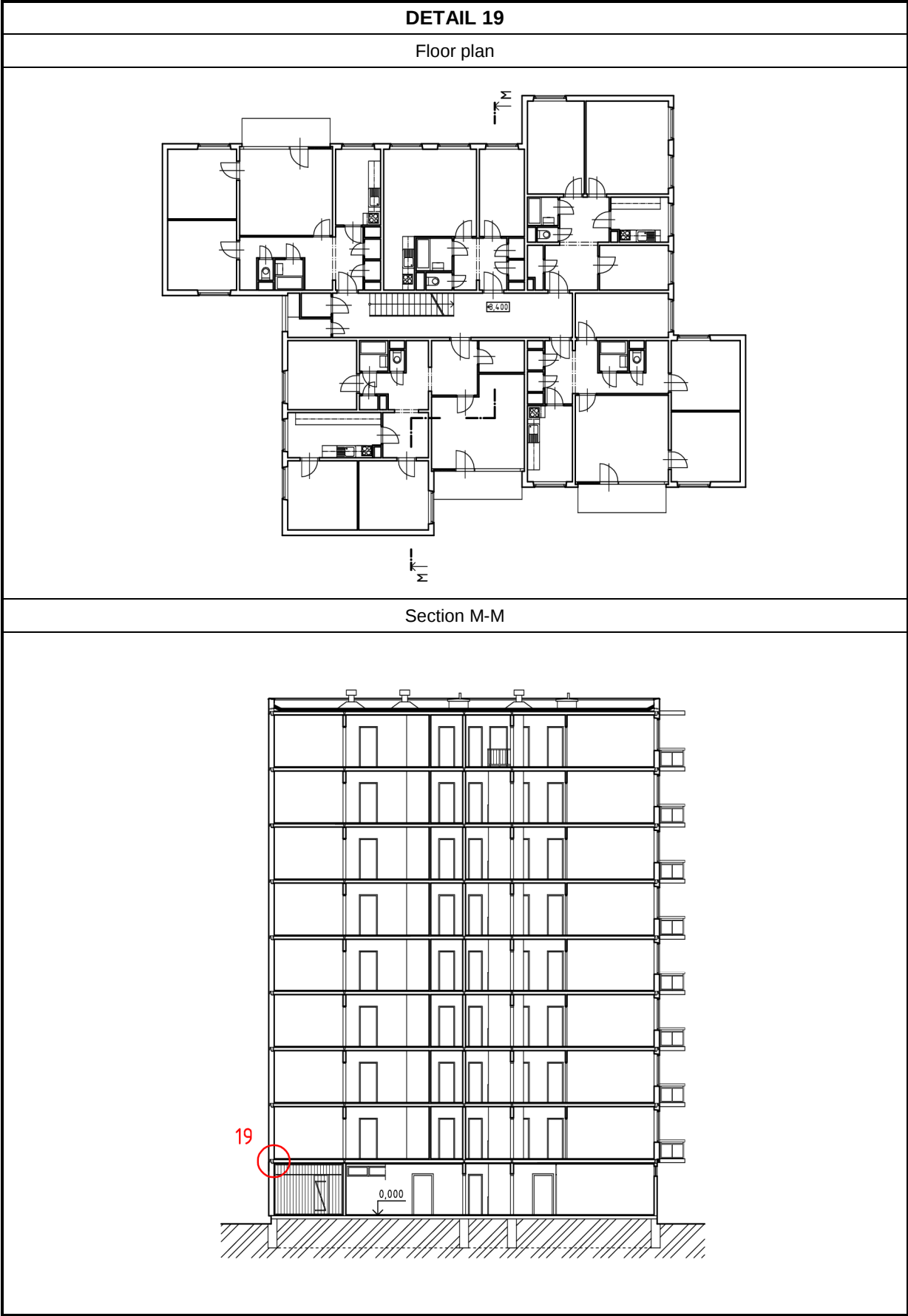


Table 4.19.2 – Structural composition of detail 19

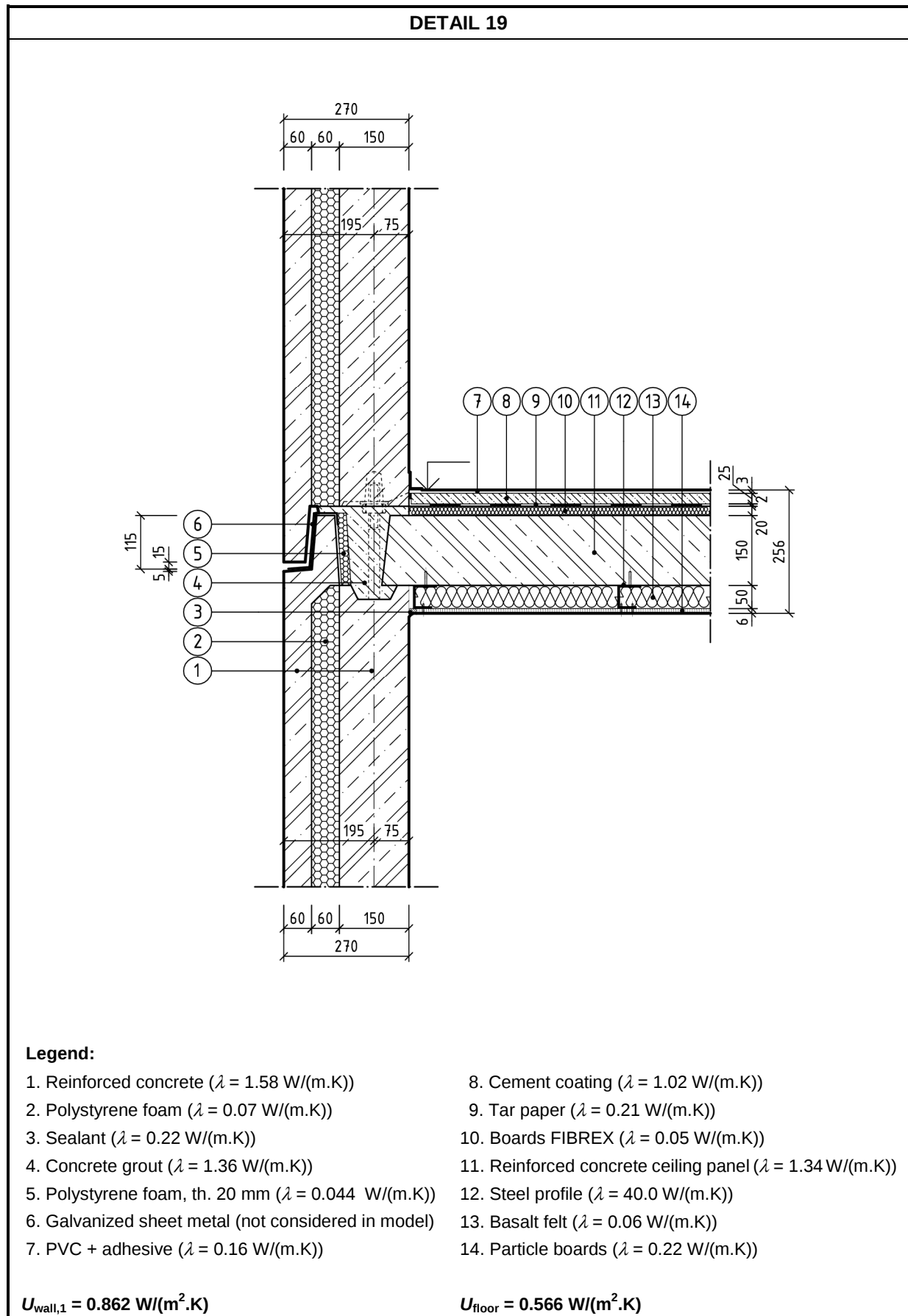


Table 4.19.3 – Boundary conditions for a calculation of detail 19

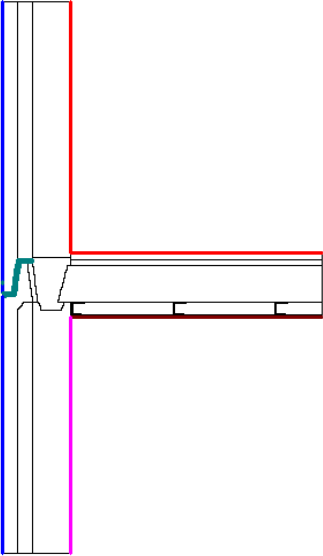
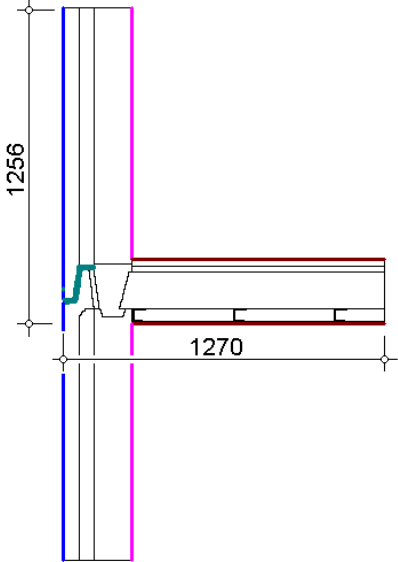
DETAIL 19		
Boundary conditions for calculation of surface temperatures		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.08\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.17\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.08\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$

Table 4.19.4 – Thermal-technical evaluation of detail 19

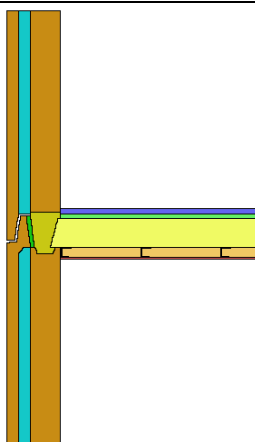
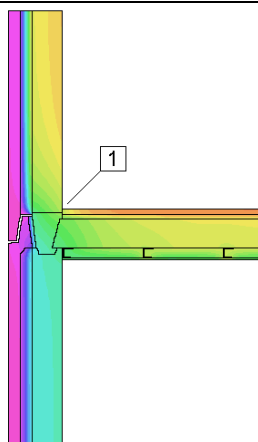
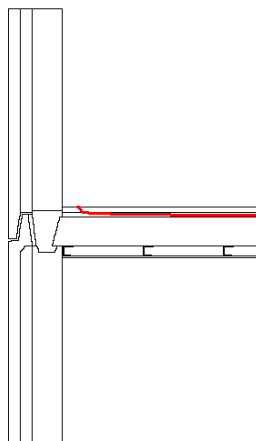
DETAIL 19																																																
Modeled detail with marking the materials		Temperature field with marked critical temperatures																																														
																																																
Legend: <table><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.160 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 40.00 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.210 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.020 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr></table>			$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.160 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 40.00 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.210 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$		$\lambda = 1.020 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>			-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.160 \text{ W/(m.K)}$																																													
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	$\lambda = 1.020 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$																																													
-15.0 °C	... -11.5 °C																																															
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-8.0 °C	... -4.5 °C																																															
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	0 °C		15 °C																																													
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1	$\theta_{Si} = 7.88 \text{ °C}$	-	$\theta_{Si} = 7.88 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																												
			NOTE: For more than two boundary conditions it is not possible to use the temperature factor. In calculation of ψ the value b_x is used.																																													
Linear thermal transmittance			$\psi = 1.57588 - 0.862 \times 1.256 - 0.566 \times 1.270 \times 0.5 = 0.134 \text{ W/(m.K)}$																																													

Table 4.20.1 – Marking of the position of detail in the building – detail 20

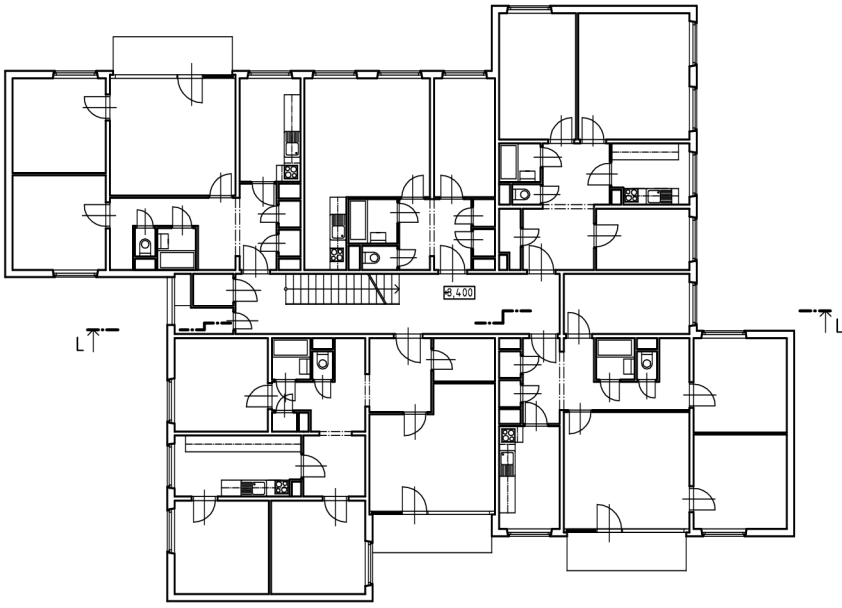
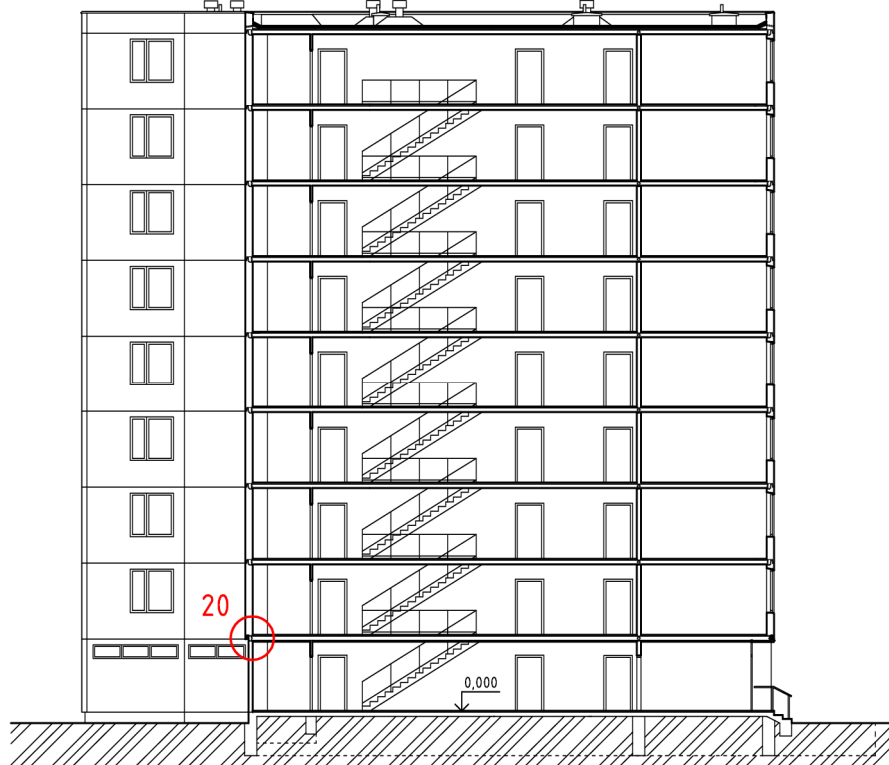
DETAIL 20
Floor plan

Section L-L


Table 4.20.2 – Structural composition of detail 20

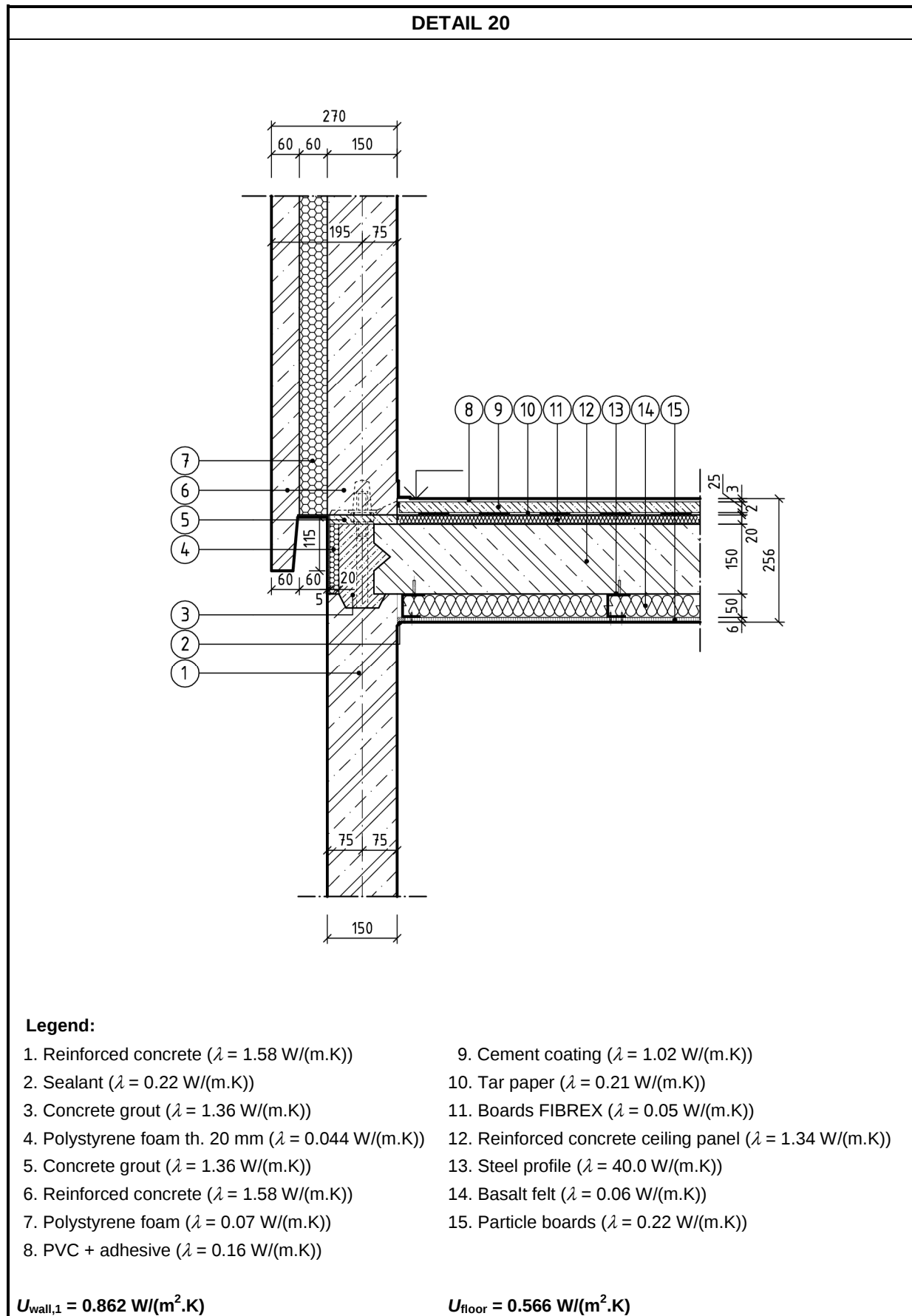


Table 4.20.3 – Boundary conditions for a calculation detail 20

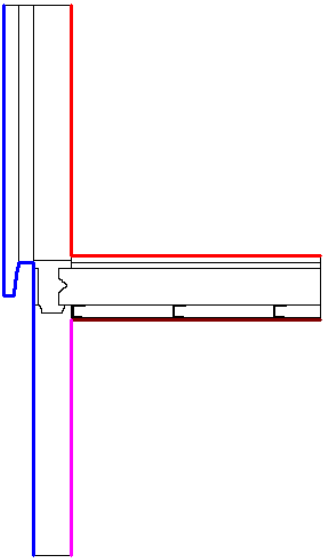
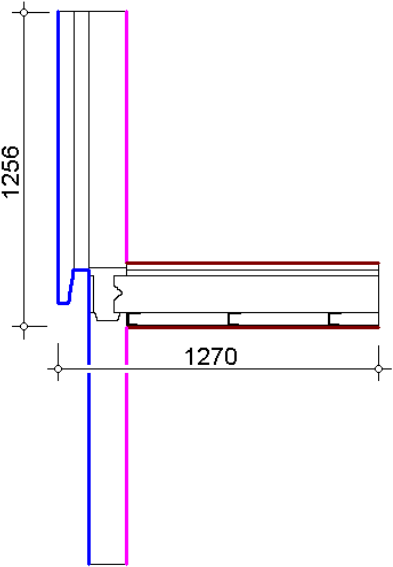
DETAIL 20		
Boundary conditions for calculation of surface temperatures		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.17\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$

Table 4.20.4 – Thermal-technical evaluation of detail 20

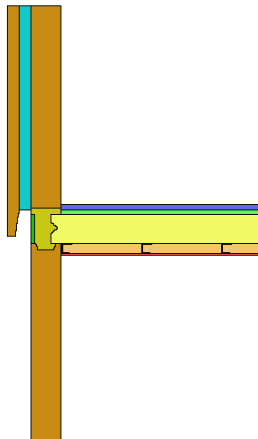
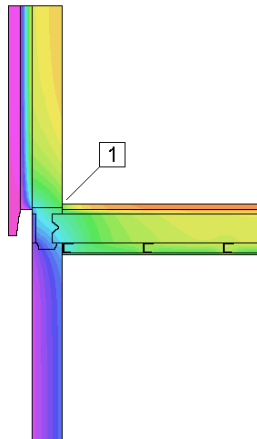
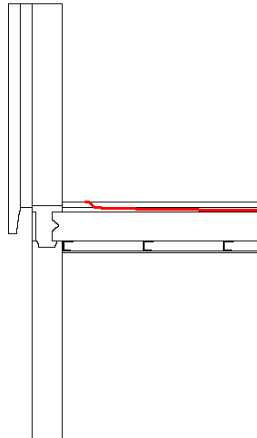
DETAIL 20																																																
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																													
																																																
Legend: <table><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.160 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 40.00 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.210 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.020 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.160 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 40.00 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.210 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$		$\lambda = 1.020 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.160 \text{ W/(m.K)}$																																													
	$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 40.00 \text{ W/(m.K)}$																																													
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-15.0 °C	... -11.5 °C																																															
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Representation of characteristic isotherms			Representation of the critical isotherm																																													
																																																
<table><tr><td></td><td>-10 °C</td><td></td><td>5 °C</td></tr><tr><td></td><td>-5 °C</td><td></td><td>10 °C</td></tr><tr><td></td><td>0 °C</td><td></td><td>15 °C</td></tr></table>				-10 °C		5 °C		-5 °C		10 °C		0 °C		15 °C	 13.12 °C																																	
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Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																												
1	$\theta_{si} = 5.05 \text{ °C}$	-	$\theta_{si} = 5.05 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet																																												
			NOTE: For more than two boundary conditions it is not possible to use the temperature factor. In calculation of ψ the value b_x is used.																																													
Linear thermal transmittance			$\psi = 1.74443 - 0.862 \times 1.256 - 0.566 \times 1.270 \times 0.5 = 0.302 \text{ W/(m.K)}$																																													

Table 4.21.1 – Marking of the position of detail in the building – detail 21

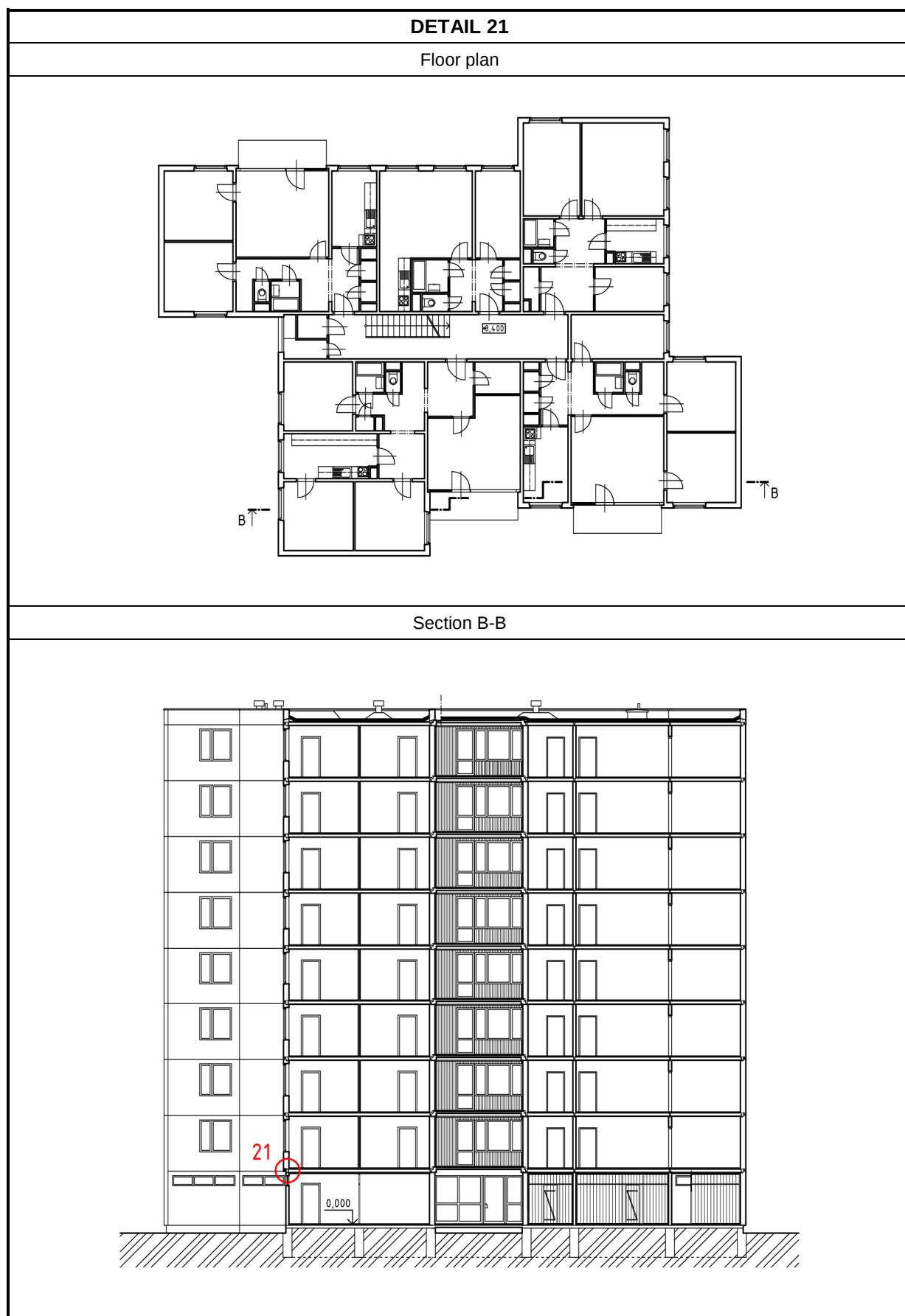


Table 4.21.2 – Structural composition of detail 21

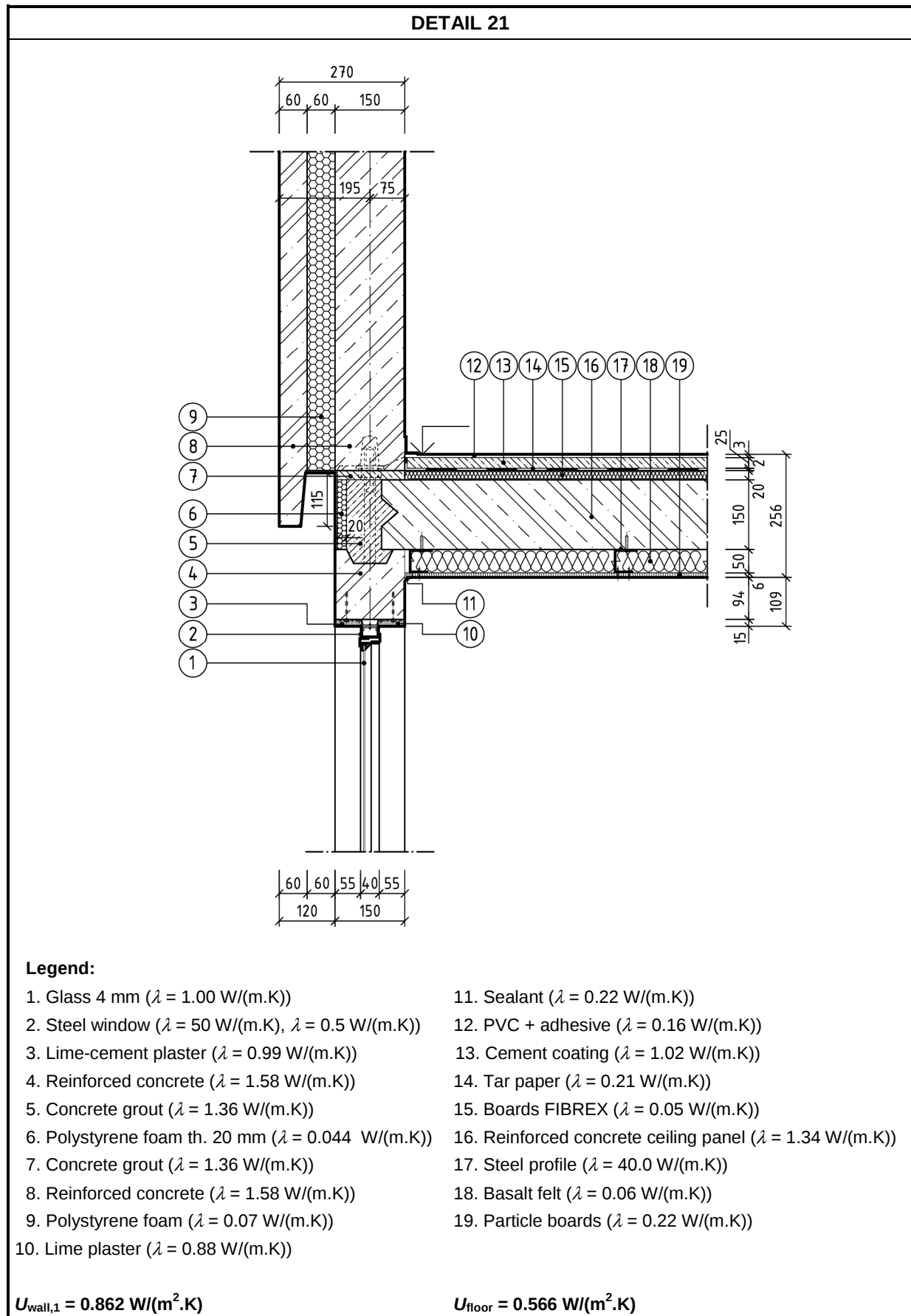


Table 4.21.3 – Boundary conditions for a calculation detail 21

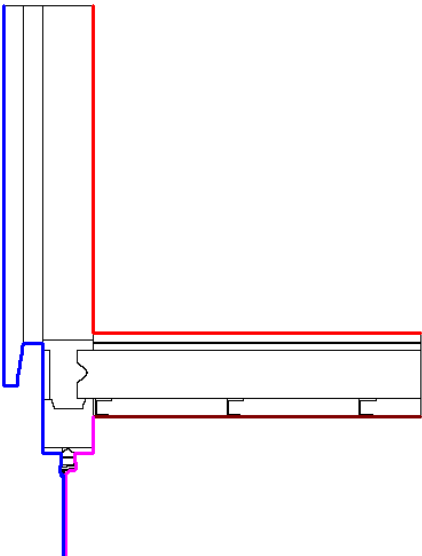
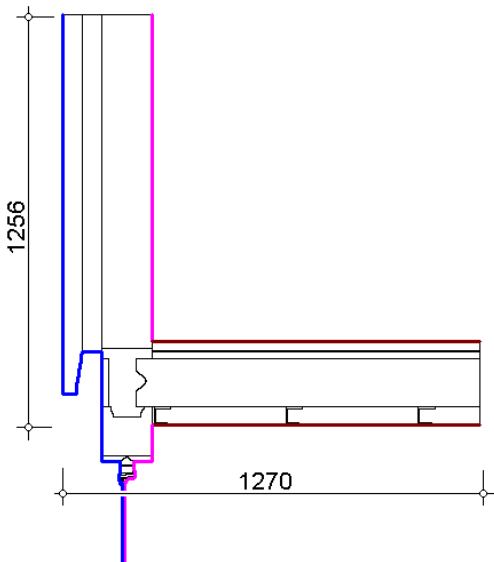
DETAIL 21		
Boundary conditions for calculation of surface temperatures		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ }^{\circ}\text{C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.17\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ }^{\circ}\text{C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$

Table 4.21.4 – Thermal-technical evaluation of detail 21

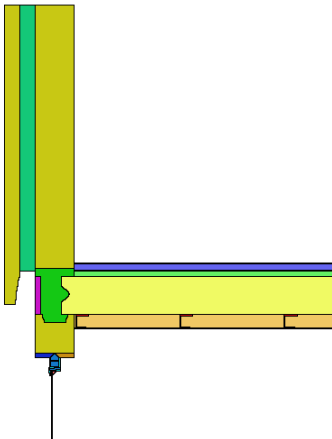
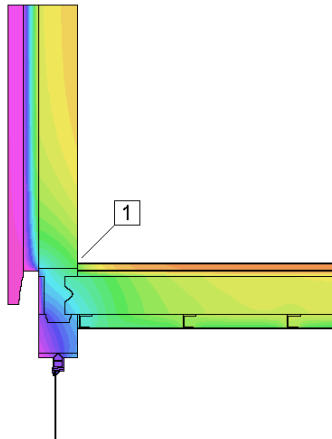
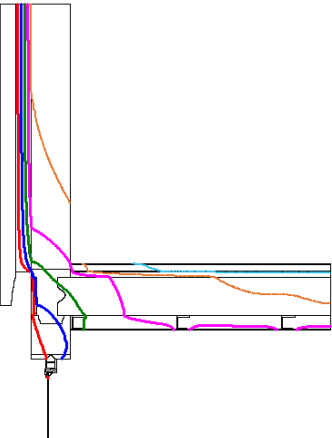
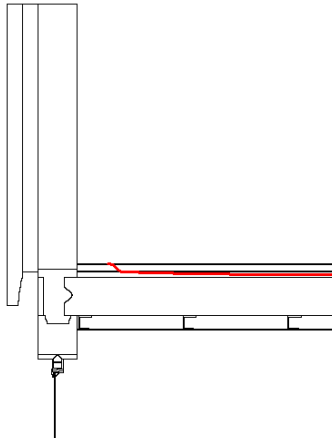
DETAIL 21																																																												
Modeled detail with marking the materials		Temperature field with marked critical temperatures																																																										
																																																												
Legend: <table><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 50.00 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.500 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.210 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.990 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.020 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.160 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 40.00 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.880 \text{ W/(m.K)}$</td><td></td><td></td></tr></table>			$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 50.00 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.500 \text{ W/(m.K)}$		$\lambda = 0.210 \text{ W/(m.K)}$		$\lambda = 0.990 \text{ W/(m.K)}$		$\lambda = 1.020 \text{ W/(m.K)}$		$\lambda = 1.000 \text{ W/(m.K)}$		$\lambda = 0.160 \text{ W/(m.K)}$		$\lambda = 0.044 \text{ W/(m.K)}$		$\lambda = 40.00 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.880 \text{ W/(m.K)}$			 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>			-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 1.580 \text{ W/(m.K)}$																																																									
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-1.0 °C	... 2.5 °C																																																											
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13.0 °C	... 16.5 °C																																																											
16.5 °C	... 20.0 °C																																																											
Representation of characteristic isotherms		Representation of the critical isotherm																																																										
																																																												
<table><tr><td> -10 °C</td><td> 5 °C</td></tr><tr><td> -5 °C</td><td> 10 °C</td></tr><tr><td> 0 °C</td><td> 15 °C</td></tr></table>		-10 °C	5 °C	-5 °C	10 °C	0 °C	15 °C	 13.12 °C																																																				
-10 °C	5 °C																																																											
-5 °C	10 °C																																																											
0 °C	15 °C																																																											
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																																								
1	$\theta_{\text{Si}} = 5.04 \text{ °C}$	-	$\theta_{\text{Si}} = 5.04 \text{ °C} < \theta_{\text{Si},80} + \Delta\theta_{\text{Si}} = 13.12 \text{ °C}$	not meet																																																								
			NOTE: For more than two boundary conditions it is not possible to use the temperature factor. In calculation of ψ the value b_x is used.																																																									
Linear thermal transmittance			$\psi = 1.74528 - 0.862 \times 1.256 - 0.566 \times 1.270 \times 0.5 = 0.303 \text{ W/(m.K)}$																																																									

Table 4.22.1 – Marking of the position of detail in the building – detail 22

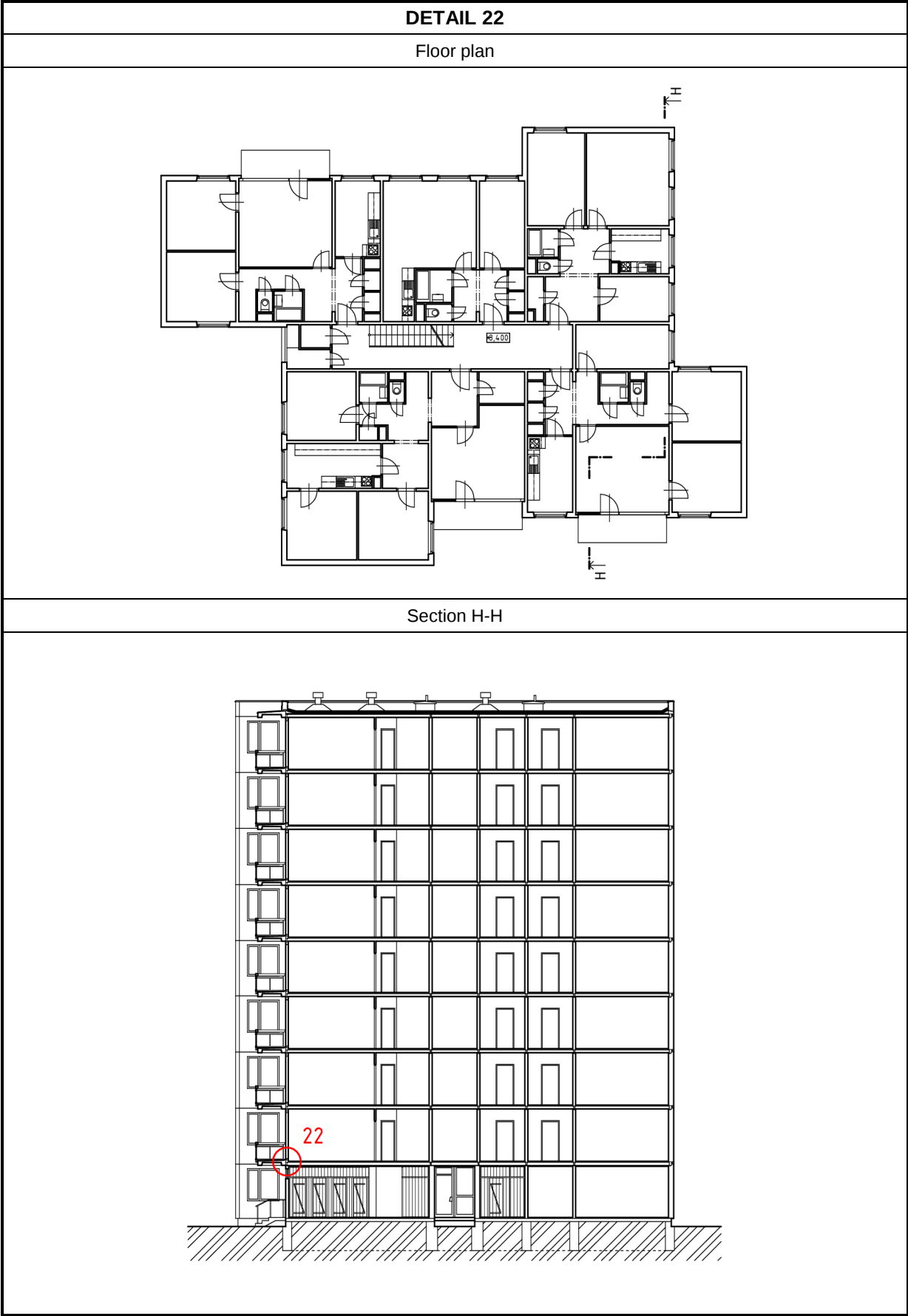


Table 4.22.2 – Structural composition of detail 22

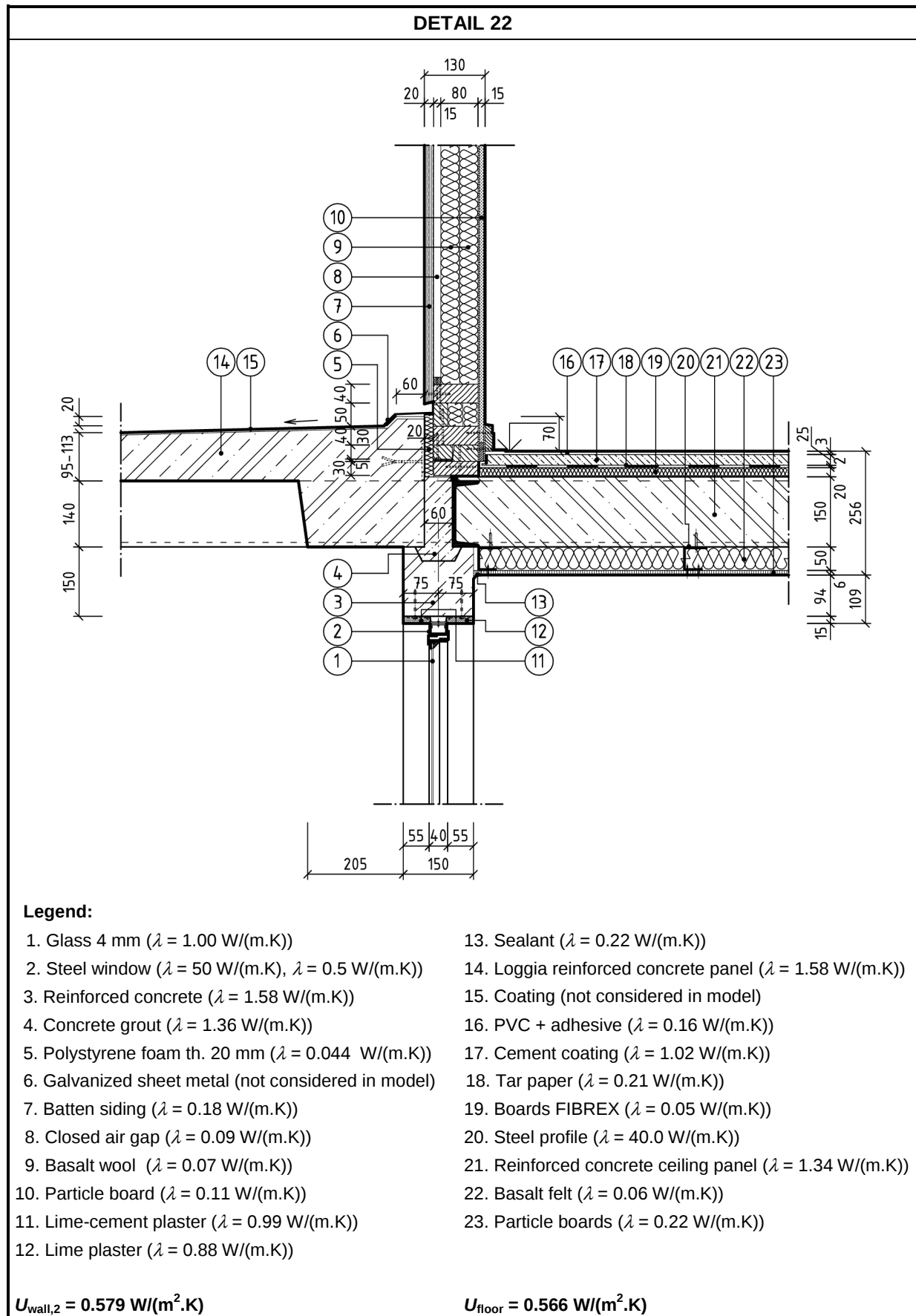


Table 4.22.3 – Boundary conditions for a calculation detail 22

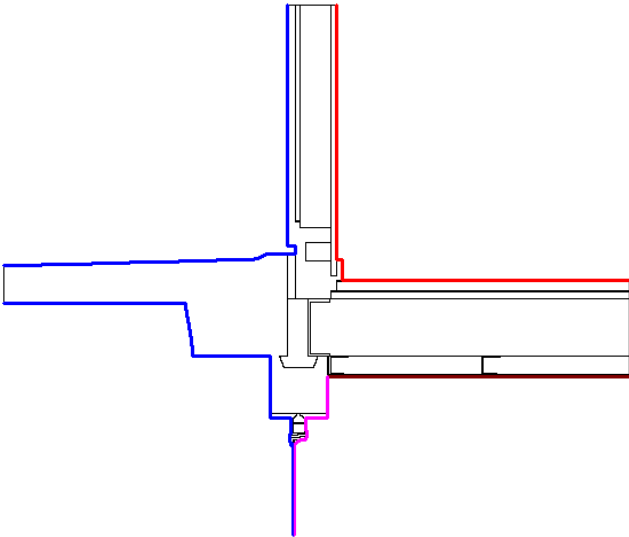
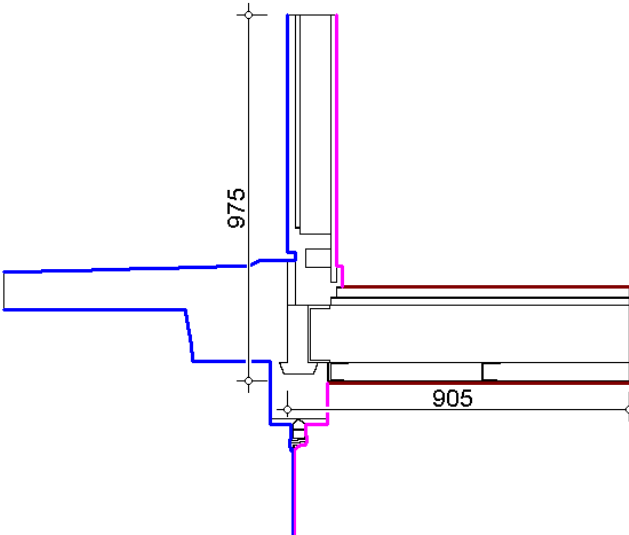
DETAIL 22		
Boundary conditions for calculation of surface temperatures		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ }^{\circ}\text{C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ }^{\circ}\text{C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.17\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ }^{\circ}\text{C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ }^{\circ}\text{C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$

Table 4.22.4 – Thermal-technical evaluation of detail 22

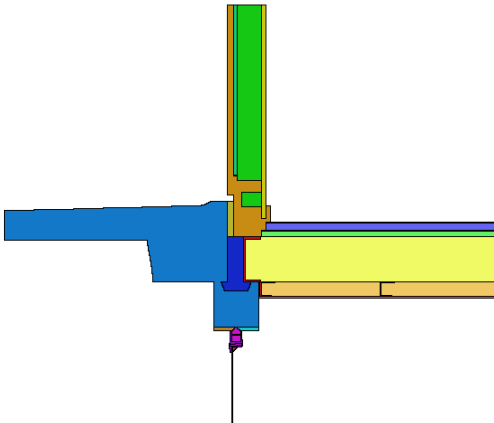
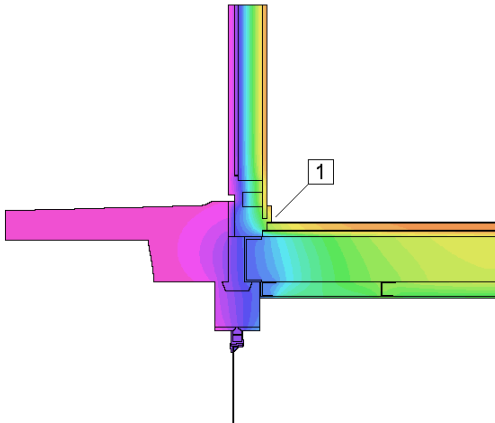
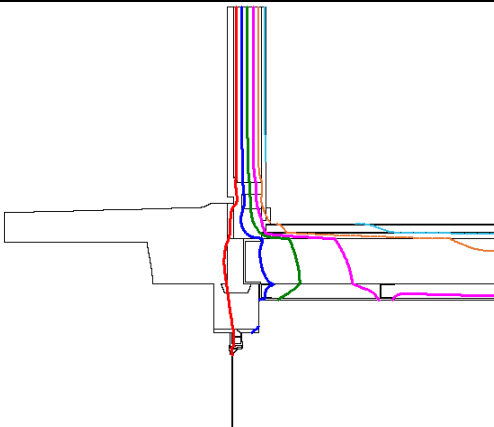
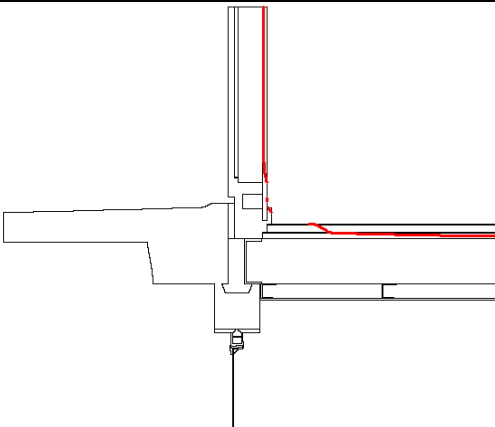
DETAIL 22				
Modeled detail with marking the materials		Temperature field with marked critical temperatures		
				
Legend:				
$\lambda = 0.220 \text{ W/(m.K)}$ $\lambda = 0.060 \text{ W/(m.K)}$ $\lambda = 1.340 \text{ W/(m.K)}$ $\lambda = 0.050 \text{ W/(m.K)}$ $\lambda = 0.210 \text{ W/(m.K)}$ $\lambda = 1.020 \text{ W/(m.K)}$ $\lambda = 0.160 \text{ W/(m.K)}$ $\lambda = 40.00 \text{ W/(m.K)}$ $\lambda = 0.180 \text{ W/(m.K)}$ $\lambda = 0.110 \text{ W/(m.K)}$ $\lambda = 0.070 \text{ W/(m.K)}$ $\lambda = 0.880 \text{ W/(m.K)}$ $\lambda = 1.580 \text{ W/(m.K)}$ $\lambda = 1.360 \text{ W/(m.K)}$ $\lambda = 50.00 \text{ W/(m.K)}$ $\lambda = 0.500 \text{ W/(m.K)}$ $\lambda = 0.090 \text{ W/(m.K)}$ $\lambda = 0.220 \text{ W/(m.K)}$ $\lambda = 0.990 \text{ W/(m.K)}$ $\lambda = 0.044 \text{ W/(m.K)}$ $\lambda = 1.000 \text{ W/(m.K)}$		-15.0 °C ... -11.5 °C ... -8.0 °C ... -4.5 °C ... -1.0 °C ... 2.5 °C ... 6.0 °C ... 9.5 °C ... 13.0 °C ... 16.5 °C ... 20.0 °C		
Representation of characteristic isotherms		Representation of the critical isotherm		
				
-10 °C -5 °C 0 °C 5 °C 10 °C 15 °C		13.12 °C		
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating
1	$\theta_{si} = 9.14 \text{ °C}$	-	$\theta_{si} = 9.14 \text{ °C} < \theta_{si,80} + \Delta\theta_{si} = 13.12 \text{ °C}$	not meet
			NOTE: For more than two boundary conditions it is not possible to use the temperature factor. In calculation of ψ the value b_x is used.	
Linear thermal transmittance			$\psi = 0.97074 - 0.579 \times 0.975 - 0.566 \times 0.905 \times 0.5 = 0.150 \text{ W/(m.K)}$	

Table 4.23.1 – Marking of the position of detail in the building – detail 23

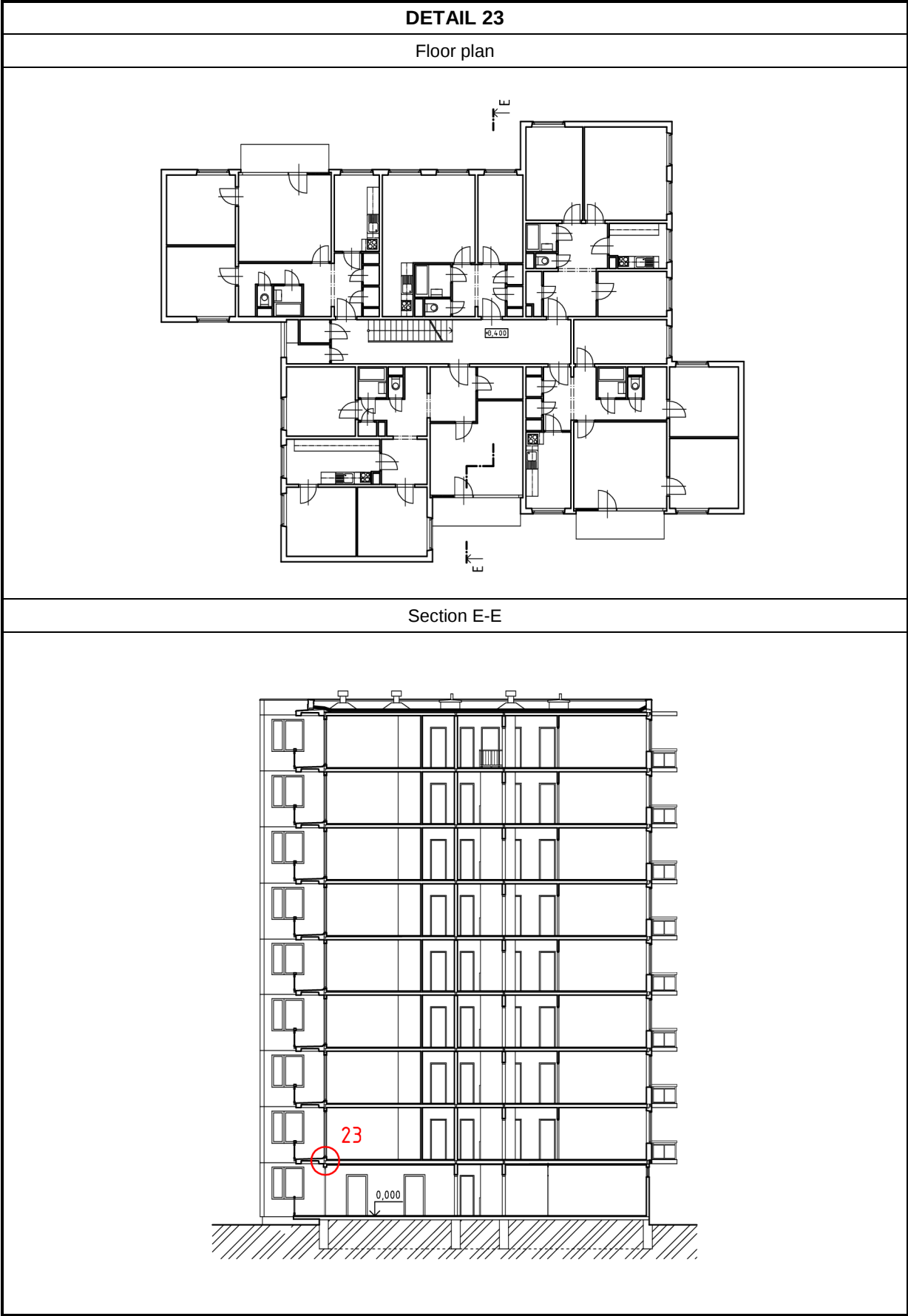


Table 4.23.2 – Structural composition of detail 23

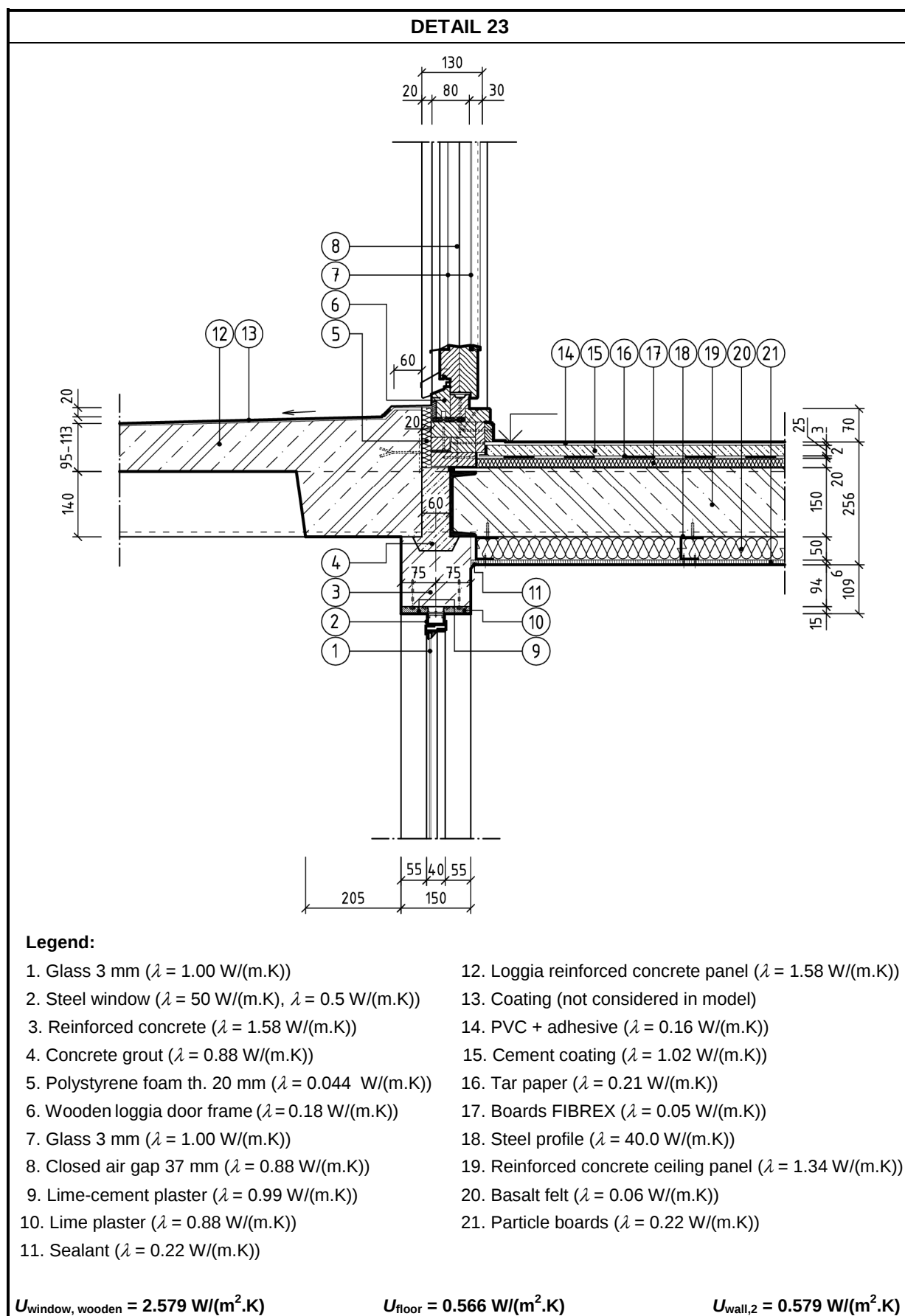


Table 4.23.3 – Boundary conditions for a calculation detail 23

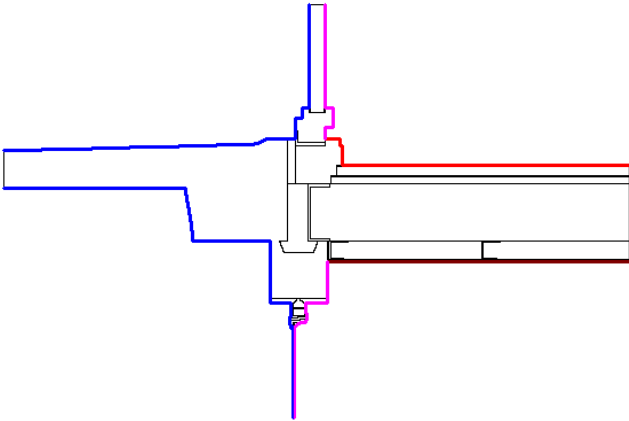
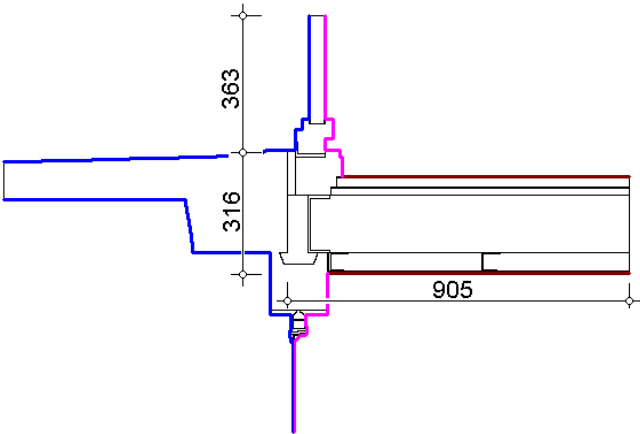
DETAIL 23		
Boundary conditions for calculation of surface temperatures		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2.\text{K/W}$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2.\text{K/W}$ — $R_{se} = 0.13\text{ m}^2.\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2.\text{K/W}$ — $R_{si} = 0.17\text{ m}^2.\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2.\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2.\text{K/W}$ — $R_{se} = 0.13\text{ m}^2.\text{K/W}$

Table 4.23.4 – Thermal-technical evaluation of detail 23

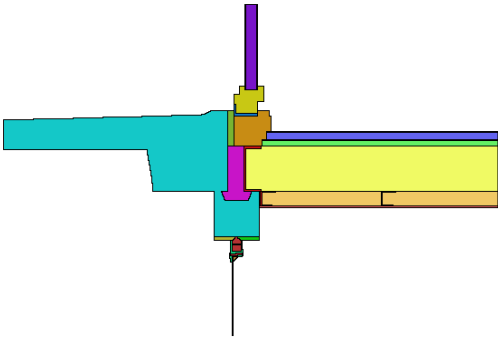
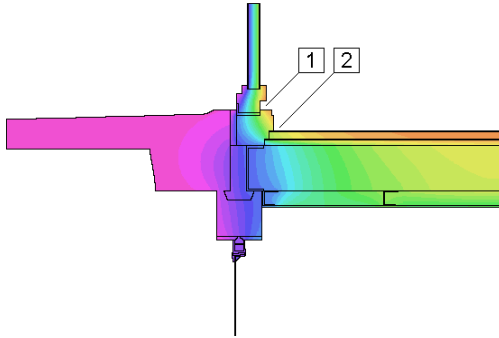
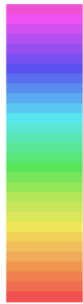
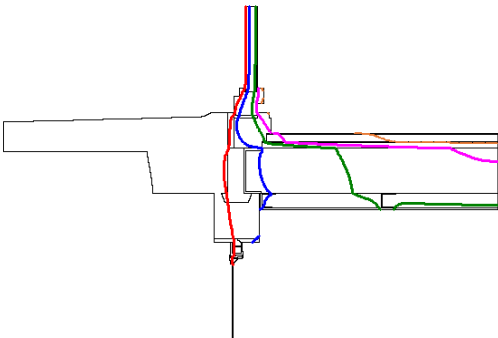
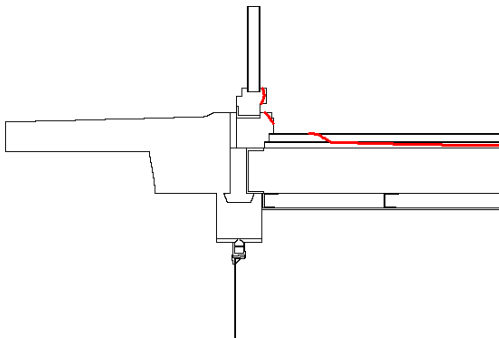
DETAIL 23																																														
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																											
																																														
Legend: <table><tr><td> $\lambda = 0.220 \text{ W/(m.K)}$</td><td> $\lambda = 1.580 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.060 \text{ W/(m.K)}$</td><td> $\lambda = 0.070 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 1.340 \text{ W/(m.K)}$</td><td> $\lambda = 1.000 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.050 \text{ W/(m.K)}$</td><td> $\lambda = 0.204 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.210 \text{ W/(m.K)}$</td><td> $\lambda = 1.360 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 1.020 \text{ W/(m.K)}$</td><td> $\lambda = 50.00 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.160 \text{ W/(m.K)}$</td><td> $\lambda = 0.500 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 40.00 \text{ W/(m.K)}$</td><td> $\lambda = 0.220 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.180 \text{ W/(m.K)}$</td><td> $\lambda = 0.990 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.180 \text{ W/(m.K)}$</td><td> $\lambda = 0.044 \text{ W/(m.K)}$</td></tr><tr><td> $\lambda = 0.880 \text{ W/(m.K)}$</td><td></td></tr></table>			$\lambda = 0.220 \text{ W/(m.K)}$	$\lambda = 1.580 \text{ W/(m.K)}$	$\lambda = 0.060 \text{ W/(m.K)}$	$\lambda = 0.070 \text{ W/(m.K)}$	$\lambda = 1.340 \text{ W/(m.K)}$	$\lambda = 1.000 \text{ W/(m.K)}$	$\lambda = 0.050 \text{ W/(m.K)}$	$\lambda = 0.204 \text{ W/(m.K)}$	$\lambda = 0.210 \text{ W/(m.K)}$	$\lambda = 1.360 \text{ W/(m.K)}$	$\lambda = 1.020 \text{ W/(m.K)}$	$\lambda = 50.00 \text{ W/(m.K)}$	$\lambda = 0.160 \text{ W/(m.K)}$	$\lambda = 0.500 \text{ W/(m.K)}$	$\lambda = 40.00 \text{ W/(m.K)}$	$\lambda = 0.220 \text{ W/(m.K)}$	$\lambda = 0.180 \text{ W/(m.K)}$	$\lambda = 0.990 \text{ W/(m.K)}$	$\lambda = 0.180 \text{ W/(m.K)}$	$\lambda = 0.044 \text{ W/(m.K)}$	$\lambda = 0.880 \text{ W/(m.K)}$		 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
$\lambda = 0.220 \text{ W/(m.K)}$	$\lambda = 1.580 \text{ W/(m.K)}$																																													
$\lambda = 0.060 \text{ W/(m.K)}$	$\lambda = 0.070 \text{ W/(m.K)}$																																													
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16.5 °C	... 20.0 °C																																													
Representation of characteristic isotherms			Representation of the critical isotherm																																											
																																														
<table><tr><td> -10 °C</td><td> 5 °C</td></tr><tr><td> -5 °C</td><td> 10 °C</td></tr><tr><td> 0 °C</td><td> 15 °C</td></tr></table>			-10 °C	5 °C	-5 °C	10 °C	0 °C	15 °C	13.12 °C																																					
-10 °C	5 °C																																													
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0 °C	15 °C																																													
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																										
1	$\theta_{\text{Si}} = 10.34 \text{ °C}$	-	$\theta_{\text{Si}} = 9.56 \text{ °C} < \theta_{\text{Si},80} + \Delta\theta_{\text{Si}} = 13.12 \text{ °C}$	not meet																																										
2	$\theta_{\text{Si}} = 9.56 \text{ °C}$	-	NOTE: For more than two boundary conditions it is not possible to use the temperature factor. In calculation of ψ the value b_x is used.																																											
Linear thermal transmittance			$\psi = 1.49608 - 2.579 \times 0.363 - 0.579 \times 0.316 - 0.566 \times 0.905 \times 0.5$ $\psi = 0.121 \text{ W/(m.K)}$																																											

Table 4.24.1 – Marking of the position of detail in the building – detail 24

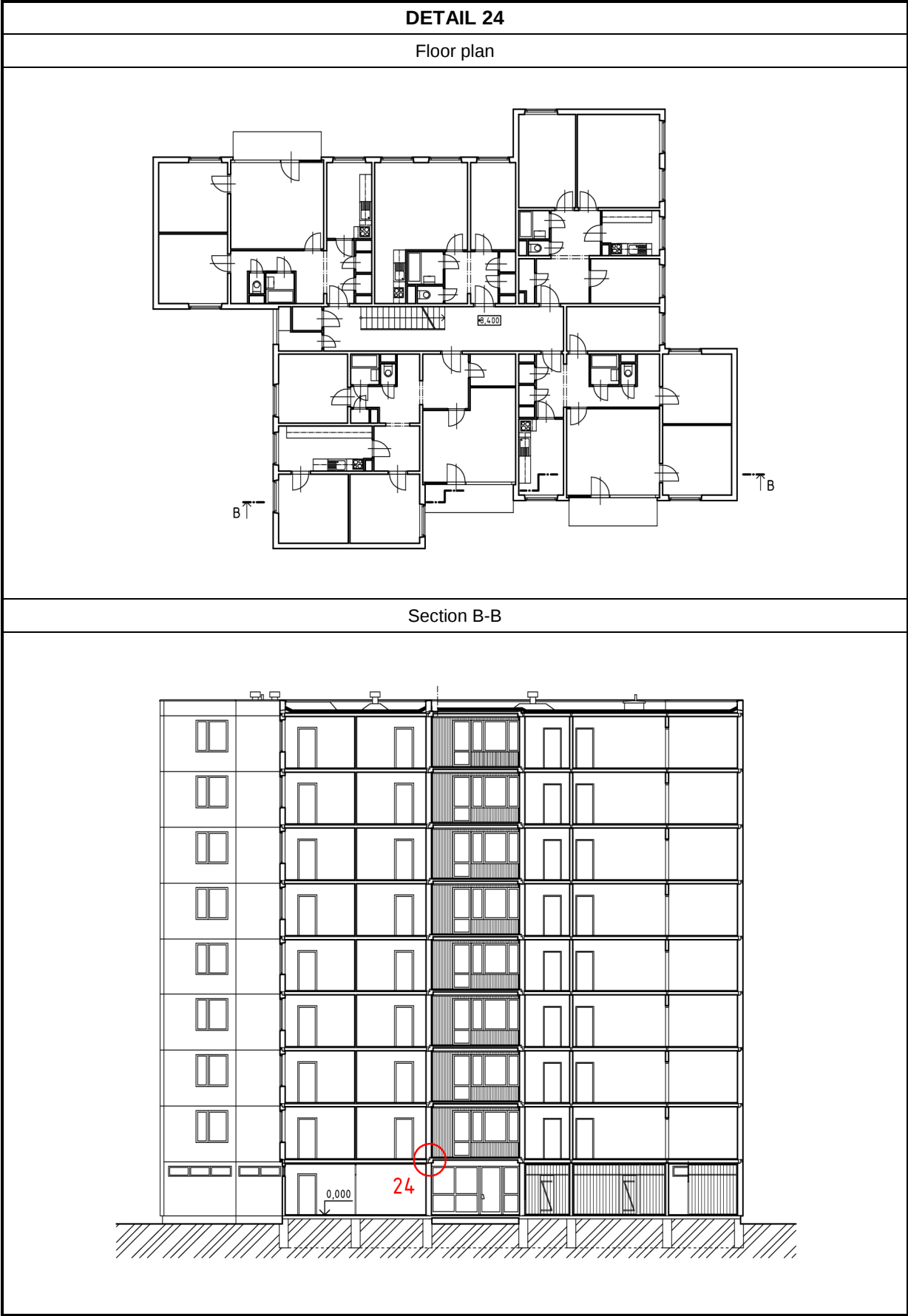


Table 4.24.2 – Structural composition of detail 24

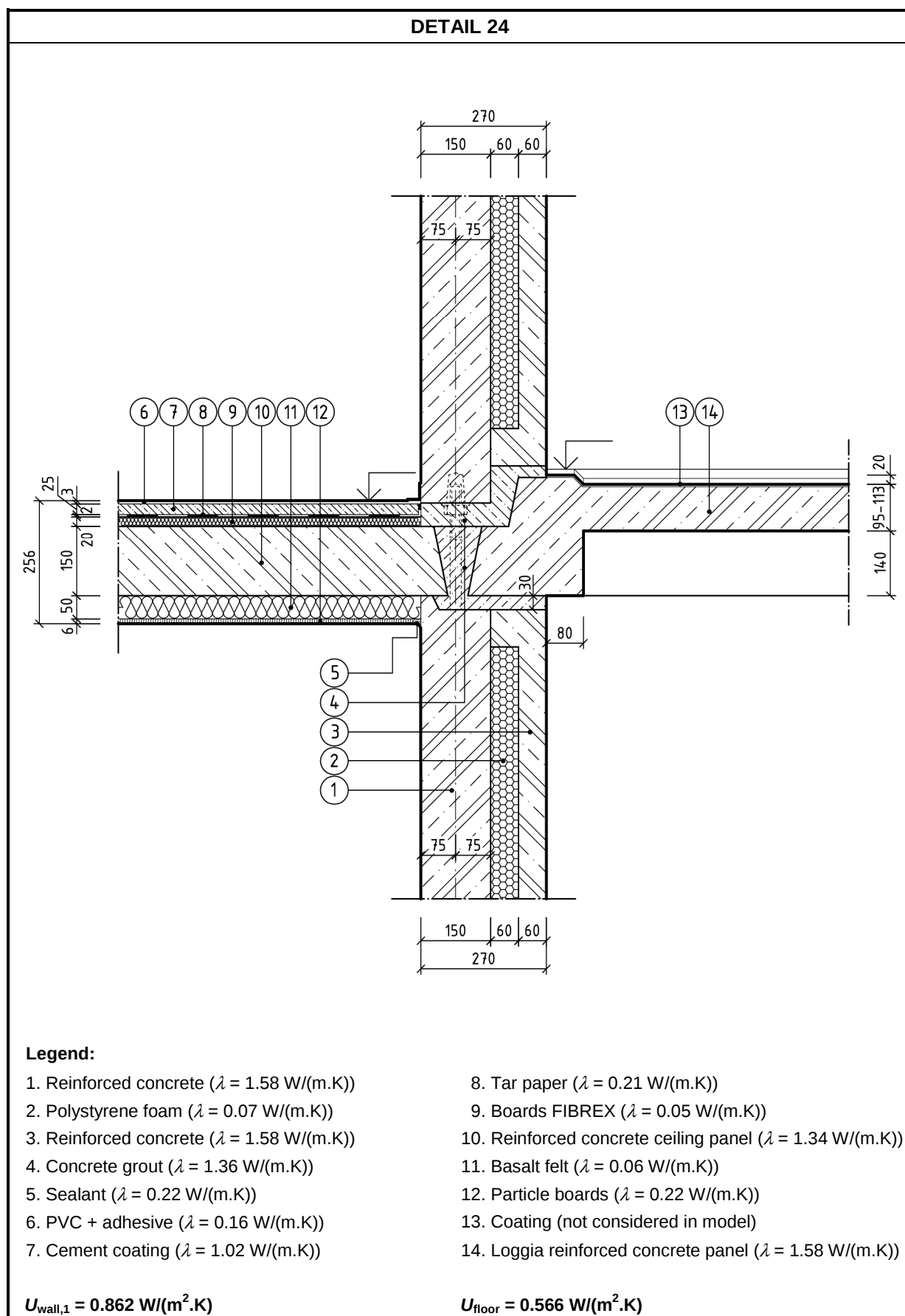


Table 4.24.3 – Boundary conditions for a calculation detail 24

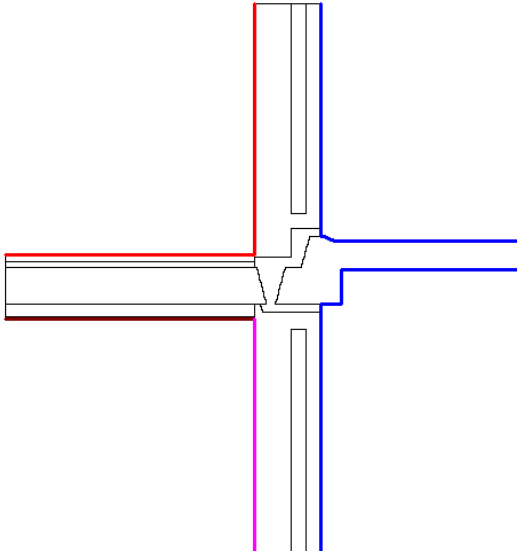
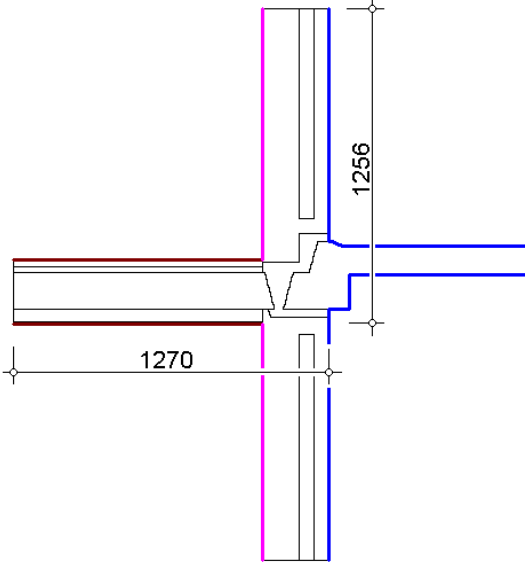
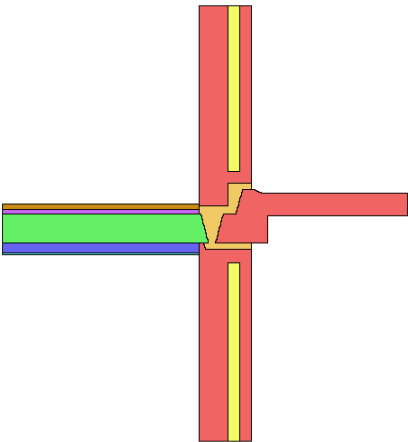
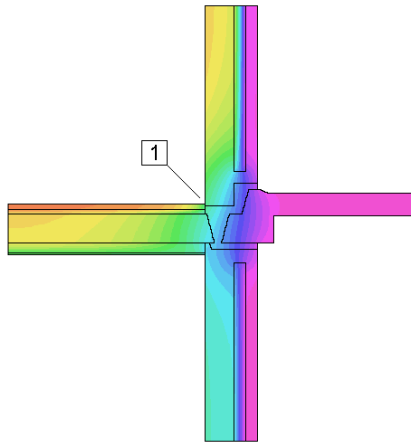
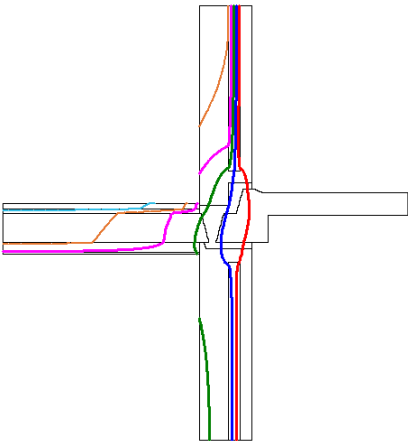
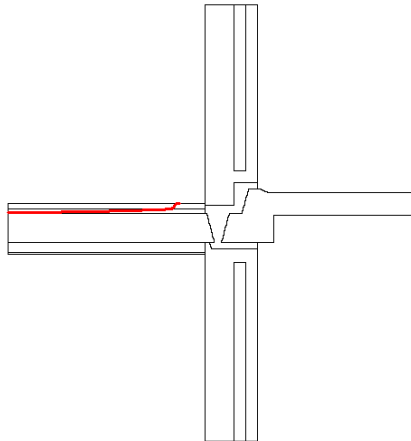
DETAIL 24		
Boundary conditions for calculation of surface temperatures		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.25\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$
Boundary conditions and corresponding lengths for a calculation of the linear thermal transmittance		
		
Boundary conditions for interior	Boundary conditions for exterior	Bound. condit. for unheated space
$\theta_i = 20\text{ °C}$ $\varphi_i = 50\%$ — $R_{si} = 0.13\text{ m}^2\cdot\text{K/W}$ — $R_{si} = 0.17\text{ m}^2\cdot\text{K/W}$	$\theta_e = -15\text{ °C}$ $\varphi_e = 84\%$ — $R_{se} = 0.04\text{ m}^2\cdot\text{K/W}$	$\theta_e = 2.5\text{ °C}$ $\varphi_e = 60\%$ — $R_{se} = 0.17\text{ m}^2\cdot\text{K/W}$ — $R_{se} = 0.13\text{ m}^2\cdot\text{K/W}$

Table 4.24.4 – Thermal-technical evaluation of detail 24

DETAIL 24																																												
Modeled detail with marking the materials			Temperature field with marked critical temperatures																																									
																																												
Legend: <table><tr><td></td><td>$\lambda = 1.580 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.060 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.360 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.050 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.070 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.210 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 1.340 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 1.020 \text{ W/(m.K)}$</td></tr><tr><td></td><td>$\lambda = 0.220 \text{ W/(m.K)}$</td><td></td><td>$\lambda = 0.160 \text{ W/(m.K)}$</td></tr></table>				$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$		$\lambda = 1.360 \text{ W/(m.K)}$		$\lambda = 0.050 \text{ W/(m.K)}$		$\lambda = 0.070 \text{ W/(m.K)}$		$\lambda = 0.210 \text{ W/(m.K)}$		$\lambda = 1.340 \text{ W/(m.K)}$		$\lambda = 1.020 \text{ W/(m.K)}$		$\lambda = 0.220 \text{ W/(m.K)}$		$\lambda = 0.160 \text{ W/(m.K)}$	 <table><tr><td>-15.0 °C</td><td>... -11.5 °C</td></tr><tr><td>-11.5 °C</td><td>... -8.0 °C</td></tr><tr><td>-8.0 °C</td><td>... -4.5 °C</td></tr><tr><td>-4.5 °C</td><td>... -1.0 °C</td></tr><tr><td>-1.0 °C</td><td>... 2.5 °C</td></tr><tr><td>2.5 °C</td><td>... 6.0 °C</td></tr><tr><td>6.0 °C</td><td>... 9.5 °C</td></tr><tr><td>9.5 °C</td><td>... 13.0 °C</td></tr><tr><td>13.0 °C</td><td>... 16.5 °C</td></tr><tr><td>16.5 °C</td><td>... 20.0 °C</td></tr></table>		-15.0 °C	... -11.5 °C	-11.5 °C	... -8.0 °C	-8.0 °C	... -4.5 °C	-4.5 °C	... -1.0 °C	-1.0 °C	... 2.5 °C	2.5 °C	... 6.0 °C	6.0 °C	... 9.5 °C	9.5 °C	... 13.0 °C	13.0 °C	... 16.5 °C	16.5 °C	... 20.0 °C
	$\lambda = 1.580 \text{ W/(m.K)}$		$\lambda = 0.060 \text{ W/(m.K)}$																																									
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Representation of characteristic isotherms			Representation of the critical isotherm																																									
																																												
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	-10 °C		5 °C																																									
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	0 °C		15 °C																																									
Point	Temperature	Temperat. factor	Evaluation of hygienic criterion	Rating																																								
1	$\theta_{Si} = 2.79 \text{ °C}$	-	$\theta_{Si} = 2.79 \text{ °C} < \theta_{Si,80} + \Delta\theta_{Si} = 13.12 \text{ °C}$	not meet																																								
			NOTE: For more than two boundary conditions it is not possible to use the temperature factor. In calculation of ψ the value b_x is used.																																									
Linear thermal transmittance			$\psi = 1.95855 - 0.862 \times 1.256 - 0.566 \times 1.270 \times 0.5 = 0.516 \text{ W/(m.K)}$																																									

5 Conclusion

This part of the publication solved problems of thermal-technical calculation, analysis and evaluation of envelope constructions, windows, and selected details of detached panel apartment house, built in structural system B 70, in its original state. The analysis of the results in chapter 2 showed that none of the envelope constructions meet the required standard values. It follows that, all envelope constructions must be renovated by additional thermal insulation and windows must be replaced. In chapter 4, were evaluated 24 details of the building from the point of view of the hygienic criterion. The linear thermal transmittance was calculated, as well. The results showed that only three details meet the requirement of the standard on hygienic criterion.

The evaluation of another details and their thermal-technical parameters is in the second part of the publication titled Complex Thermal-Technical Analysis of the Detached Panel Apartment House of Type B 70 in Original State (Part 2).

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